

TIME CRITICAL REMOVAL PLAN

FOR THE

TOLEDO TIE TREATMENT SITE

LOCATED AT

ARCO INDUSTRIAL PARK TOLEDO, OHIO

JULY 1998

Prepared For:

KERR-McGEE CHEMICAL, LLC KERR-McGEE CENTER OKLAHOMA CITY, OKLAHOMA 73125

Prepared By:



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July 10, 1998

Mr. Ralph Dollhopf, On-Scene Coordinator United States Environmental Protection Agency 9311 Groh Road, Room 316 Grosse Isle, Michigan 48138-1697

Ms Deborah Orr, Remedial Project Manager United States Environmental Protection-Agency 77 W. Jackson Boulevard (SE-4J) Chicago, Illinois 60606-3950

RE: Toledo Tie Treatment Site, Time Critical Removal Plan PWM001.100.0064

Dear Mr. Dollhopf and Ms. Orr:

Enclosed is a plan set and supporting document, Time Critical Removal Plan, which is being submitted pursuant to our discussions in June, 1998. These documents describe Kerr-McGee Chemical's, LLC, (KMC) approach to address the migration of creosote related contamination to Williams Ditch and the surface of Frenchmens Road at the Toledo Tie Treatment Site in Toledo, Ohio. We trust that the enclosed information is consistent with our discussions.

Please feel free to contact Peter Goetz, KMC project coordinator or me with questions or if you require additional information.

Sincerely,

Scott Lockhart, P.E.

SFI/jlj

Enclosure

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1.0 INTRODUCTION

Kerr-McGee Chemical Corporation, now known as Kerr-McGee Chemical, LLC (KMC), was

issued a Unilateral Administrative Order (UAO), on December 24, 1997, pursuant to Section

106(a) of the Comprehensive Environmental Response, Compensation, and Liability Act

(CERCLA). The UAO pertains to the Toledo Tie Treatment Site (Site) located in and near the

Arco Industrial Park in Toledo, Ohio. Section V, Item 3.5) and Item 3.7) of the UAO dictate that

KMC:

Remove the immediate source areas of hazardous substances or implement

engineering controls to prevent the contamination in the source areas from

migrating to Williams Ditch and to the surface of Frenchmens Road, and

Remove coal tar creosote contamination from Williams Ditch sediments and/or implement additional engineering controls to prevent continued release of

contaminants to Williams Ditch.

KMC has entered into contract negotiations with OHM Corporation (OHM) to complete these time

critical activities at the Site. A qualified backup contractor has been identified should KMC not

reach agreement with OHM. Pending the approval of a work plan, the final scope of work with

the contractor will be negotiated. This work plan has been prepared by Hull & Associates, Inc.

(HAI) on behalf of KMC to describe KMC's proposed approach to comply with the UAO.

1.1 Report Organization

This Work Plan is organized into four sections. Section 1.0 presents an overview of the project

history and the status of removal activities at the site. Section 2.0 includes a summary of the field

investigations conducted at the Site in accordance with the approved Removal Action Work Plan

(HAI, April 1998). Section 3.0 provides the rationale for the selected remedy. Section 4.0

addresses the implementation of the remedy and provides a framework for finalizing a contract

with the selected remedial contractor.

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1.2 Site Description

The Site encompasses over 50 acres and is located in the City of Toledo, Lucas County, Ohio, as

shown on Figure 1. The Site was a railroad tie treating facility owned and operated by Federal

Creosoting Company (FCC) from approximately 1923 to 1959, and the American Creosoting

Corporation (ACC) from 1959 to 1962. Operations ceased in 1962 when the Site was sold to the

City of Toledo. In 1969, the Site was sold to Arco Realty, Inc., who subdivided the Site into a

number of parcels and developed the area into a business and industrial park.

While operated by FCC and ACC, wooden railroad ties were treated with coal tar creosote at the

Site. A site map of the general wood treating operations is shown on Plate 1 in Appendix A. Based

on a review of aerial photographs from years 1950, 1957, 1963 and 1969, it appears that untreated

lumber was stored on the eastern section of the Site, and treated wood was stored on the western

section of the Site. An above ground tank farm was located in the central southern section of the

Site, south of the old access road formerly known as Creosote Road. The Ohio Environmental

Protection Agency (OEPA) reported in the Site Inspection report (SI, 1993) that the tank farm

consisted of two 500,000 gallon, three 30,000 gallon, and four 150,000 gallon creosote tanks, and

one 150,000 gallon zinc chloride tank. Suspected waste lagoons are located in the central section of

the Site, north of the access road. The suspected lagoons are located east of Arco Drive. One is

directly under and two are south of the current location of Frenchmens Road. Based on a review of

aerial photographs, it appears that the suspected lagoons were filled between 1969 and 1972. A

currently unoccupied distribution warehouse is currently situated over a portion of one of the

suspected lagoons.

Williams Ditch serves as the natural drainage in the area. When the Site operated as a wood treating

facility, the ditch ran southwest to northeast along the western section of the Site. The ditch

generally intersected what are now known as Arco Drive and Frenchmens Road, at approximately a

45-degree angle. A review of aerial photos indicates the impacted portion of the ditch was rerouted

to its current location during the redevelopment of the area.

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The Site (see Figure 1) is located on a relatively level piece of property approximately 4,500 feet

north of Swan Creek and 8,000 feet south of the Ottawa River. The Site gently slopes toward

Williams Ditch, which crosses the Site from southwest to northeast. Elevations across the site range

from 620 to 625 mean sea level (msl). Elevations are referenced to the Lucas County Datum.

The Site lies within the Eastern Lake Plains of the Central Lowland physiographic province of North

America. This glaciolacustrine landscape typically possesses low relief and low elevation. This flat

surface was created due to several widely spaced periods of continental glaciation that supplied the

largely unsorted, unstratified surficial drift deposits that cover the land in this area of the state.

During the most recent stages of ice retreat, released water became trapped between the retreating ice

mass to the north and the glacial deposits to the south and proglacial lakes formed. These lakes

produced a thin veneer of lacustrine deposits over the glacial tills.

More specifically, the surficial lacustrine deposits consist of two distinct types: silt and clay deposits

representing quiet water deposition; and sand deposits representing higher energy environments (i.e.

near shore). The lacustrine deposits are approximately 12 to 14 feet thick at the Site and range from

silt to clay to sand.

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The Ohio Department of Natural Resource (ODNR), Division of Geological Survey, Drift Thickness

Map of Lucas County, Ohio (ODNR, 1985) indicates that the Site sits on the southern slope of a

buried valley where the drift thickness is approximately 125 feet. The buried valley trace is from the

southwest to the northeast and reaches a maximum depth of approximately 150 feet north of the Site.

The glacial drift overlies Devonian limestone or dolomite bedrock.

The ODNR Ground-Water Resources Map of Lucas County indicates that the principal aquifer

beneath the Site is a thin, discontinuous sand and gravel lenses interbedded in the clay till filling the

preglacial valley. Yields of approximately 10 to 20 gallons per minute (gpm) are encountered at

depths of 120 feet or less.

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Higher yields may be obtained from the underlying carbonate aquifer. The area in the vicinity of the

Site is served by a municipal water supply system, and local use of ground water for potable

consumption is expected to be minimal or non-existent.

1.3 Status of Site Removal Activites

1.7

A number of environmental investigations were conducted at the Site from 1987 to 1995. Key

documents describing site conditions include the "Initial Investigation and Preliminary Risk

Assessment" report dated June 27, 1990, by Midwest Environmental Consultants, "The

Hydrogeology and Creosote Contamination of an Abandoned Wood Preserving Plant Site at Toledo,

Ohio," report dated December 1995, by Greg Victor Lesniak of the University of Toledo, and the

1993 Ohio EPA Site Inspection Report (SI). Results of soil, groundwater, and surface water samples

collected from the Site during these investigations indicated contamination from creosote compounds

existed near the suspected lagoons, former process area, and Williams Ditch. Some of the major

individual polynuclear hydrocarbons (PAHs) detected were naphthalene, benzo(a)pyrene,

phenanthrene, chrysene, fluoranthene, acenaphthalene, pyrene, and dibenzo(a,h)anthracene.

Concentrations were detected in the range of 100s to 1,000s of parts per million (ppm) in the soil,

sediment, and surface water. Investigations conducted by Ohio EPA in 1993, and the Ohio

Department of Health in 1995, determined that sediments in some areas of Williams Ditch were

saturated with creosote.

On September 25, 1997, following a significant rain event in Toledo, Ohio, the National Response

Center was notified of the presence of a sheen of an unknown oil in Williams Ditch. On October 1,

1997, representatives of the U.S. EPA Emergency Response Branch evaluated conditions in Williams

Ditch and observed an oil sheen upgradient of the National Super Service storm sewer outfall to

Williams Ditch. U.S. EPA documented that the sheen was heavy in the ditch east of Arco Drive (50

to 100 feet) and north (50 to 100 feet) of the location of the suspected creosote lagoon areas. This

area of heavy sheening is where a storm sewer apparently runs through the suspected lagoon area to

Williams Ditch.

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At the request of the U.S. EPA, KMC initiated abatement activities to preclude sheen migration in Williams Ditch on October 10, 1997, and continued these efforts until the issuance of the UAO. Pursuant to the terms of the UAO, KMC prepared work plans for conducting field investigations for the time critical phase and for the Engineering Evaluation/Cost Analysis (EE/CA). A site specific Health & Safety Plan (HASP) was also prepared, which addressed anticipated removal activities. Field investigations to collect data on surface water, soil, sediment, and air at the site were conducted between April 27, 1998 and June 1, 1998, in accordance with the Removal Action Work Plan (HAI, April 1998, approved by the U.S. EPA on April 29, 1998). These investigations are briefly described in Section 2.0. Currently, creosote related contamination that accumulates on the surface of water in Williams Ditch is recovered on a weekly basis. Two siphon dams were constructed and are functioning as intended to control the downstream migration of visible oil and oil sheen in Williams Ditch. The site has been secured with high-visibility fencing and warning signs. Support facilities and equipment, including a site trailer and a dedicated tractor to maintain the grass, have been mobilized. Site visits are conducted on a regular basis to document the site's security status and to conduct perimeter ambient air monitoring.

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2.0 SUMMARY OF INITIAL FIELD INVESTIGATIONS

HAI completed the initial field investigation of the project area from April to June 1998 in

accordance with the Field Sampling and Analysis Plan (FSAP) (HAI April, 1998). The objective

of the initial field investigation was to determine the distribution of creosote related contamination

in the suspected former lagoon area and to identify the immediate source of creosote related

contamination migrating to Williams Ditch. Activities completed during the initial field

investigation included:

Installation of sixty-five borings in the project area by Fugro Geosciences (Fugro) under the 1.

observation of an HAI representative. Borings CPT-1 through CPT-64 and BG-1 were

installed using a cone penetrometer testing (CPT) probe and a laser-induced fluorescence

(LIF) probe (see Plate 2 for CPT locations).

2. Installation of ten geoprobe borings (SB-1 through SB-10) and six test pits (TP-1 through

TP-6) to allow for visual characterization of subsurface conditions in the project area, as

well as to facilitate the collection of selected soil samples for chemical and geotechnical

analysis (see Figure 2 for soil sampling locations).

3. Collection of five surface water samples (SW1 through SW4 and BG1) and fourteen

sediment samples (SED-001 through SED-013 and SED-BG) to evaluate the quality of

water and sediment within Williams Ditch, respectively (see Figure 3 for sediment and

surface water sampling locations).

A map, showing the overall site, with environmental sampling locations, is provided as Plate 1 in

Appendix A. A summary of each task is listed below, including a review of data collected:

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2.1 Collection of Surface Water Samples

Five surface water samples were collected from Williams Ditch (BG1 and SW1 through SW4) by

HAI representatives on May 12, 1998. Each of the surface water samples were collected as close

as practical to the proposed locations presented in the FSAP, the locations of which are shown on

Figure 3. Each sample was collected consistent with the procedures presented in the FSAP and

submitted to Lancaster Laboratories, Inc. for chemical analysis. Environmental Standards, Inc. is

performing data validatation. Results are pending. Provided on Table 1 is a summary of surface

water sample collection activities, including time of collection, field parameters, and general notes

associated with sample collection. Results of the chemical analysis of surface water samples are

provided on Table 2.

A review of the chemical data indicates the highest parameter concentrations for surface water

samples to be reported for surface water sample SW-2. As shown on Figure 3, surface water

sample SW-2 was collected in close proximity to the former lagoon areas, and as discussed in

Section 2.2, is located within the approximate extent of impacted shallow soils that have been

determined to be potentially affecting the quality of surface water and/or sediment in Williams

Ditch using the CPT/LIF data. Parameter concentrations reported for surface water samples

collected both upstream and downstream of SW-2 were less than those reported for surface water

sample SW-2.

2.2 Installation of CPT/LIF Borings

Sixty-five borings were installed by Fugro from April 27 through April 30, 1998 under the

observation of an HAI representative consistent with the FSAP. Borings CPT-1 through CPT-64

and BG-1 were installed in the project area to evaluate shallow stratigraphic conditions and to

identify the approximate extent of impacted shallow soils. The CPT/LIF borings were also

installed to determine if impacted shallow soils were affecting the quality of water and/or sediment

in Williams Ditch. Each of the borings were installed using direct push technology to advance

CPT and LIF probes until the underlying silt- and clay-rich lacustrine deposits blanketing the

project area were encountered and the full thickness of LIF response above background within the

shallow soils was identified. Locations of the CPT/LIF borings were selected to allow for

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evaluation of the extent of impacted soils and are shown on Plate 1. Boring BG-1 was installed to

allow for consideration of background conditions while interpreting the CPT/LIF data. CPT/LIF

logs developed by Fugro are provided in Appendix B. Plate 2 documents the LIF signature

thickness based on the CPT/LIF logs.

Cross-sections A-A', B-B', C-C' and D-D', which are shown on Plates 3, 4, and 5, provide an

interpretation of shallow stratigraphic conditions encountered in the project area based on data

obtained via installation of the CPT/LIF borings. Included on the cross-sections are the

approximate limits of the former lagoon areas, Williams Ditch and the LIF response above

background (as appropriate). Also provided on the cross-sections are the approximate locations of

utilities in the project area and a cross-section profile line location map. As shown on the cross-

sections, the project area is characterized by an upper zone of primarily sand/silt/clay deposits

most likely associated with reworking of the surficial soils as part of filling operations. Some of

the sand/silt zones identified by the CPT/LIF borings in the upper zone may be associated with in-

situ deposits that have been documented to be present in the vicinity of the project area. Beneath

the sand/silt/clay deposits is a laterally continuous silt/clay deposit that has been identified to

represent the lacustrine deposits that blanket the project area. Within the silt/clay deposits are

silt/sand/clay zones that most likely correspond to thin granular seams/lenses typically encountered

in the lacustrine deposits in the region.

A review of the LIF data presented on the CPT/LIF borings was completed to identify depth

intervals representing the LIF response above background. The thickness of LIF signature above

background (measured in feet below ground surface) was identified for each CPT/LIF boring to

determine the thickness of LIF signature above background across the project area. As shown on

Plate 2, the thickest intervals of LIF signature above background were, in general, encountered in

the vicinity of the former lagoon areas. Minimum LIF responses above background ranged from

zero at several locations, to a maximum thickness of approximately eleven feet at boring CPT-46

near the approximate northeast corner of the former lagoon overlain by Frenchmens Road. Cross-

sections A-A' through D-D' also provide an illustration of the LIF signature above background

within shallow soils in the project area. As shown, LIF signatures above background are mostly

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encountered in the upper sand/silt/clay deposits, and occasionally extend to greater depths within

the underlying lacustrine silt/clay deposits where sand/silt/clay seams and/or utilities may serve as

preferential pathways.

A review of the CPT/LIF logs contained in Appendix B, cross-sections A-A' through D-D', and

the LIF signature thickness map provided as Plate 2 indicates that the CPT/LIF borings were

successful in providing an understanding of shallow stratigraphic conditions in the project area,

as well as identifying the approximate extent of impacted shallow soils affecting the quality of

water and/or sediment in Williams Ditch. As shown on Plate 2, the approximate extent of

impacted shallow soils has been defined using the LIF data. As shown, the quality of sediment

and/or water within Williams Ditch may be affected by impacted shallow soils in the vicinity of

borings CPT-17/17A, CPT-18, CPT-19 and CPT-33 installed directly adjacent to the south/east

bank of Williams Ditch. The approximate western extent of impacted soils as identified using

the CPT/LIF borings has been determined to be between borings CPT-19 and CPT-20, while the

approximate eastern/northern extent has been determined to be between borings CPT-33 and

CPT-35.

2.3 Installation of Geoprobe Borings and Test Pits

Ten geoprobe borings designated SB-1 through SB-10 were installed by Terra Probe on May 6,

1998 under the observation of an HAI representative. The geoprobe borings were installed in the

project area to allow for a visual description of subsurface conditions, as well as to facilitate the

collection of soil samples for chemical and geotechnical analysis. Each of the geoprobe borings

was installed immediately adjacent to a previously installed CPT/LIF boring, as summarized on

Table 3, to allow for a comparison of CPT/LIF data to data obtained via installation of the

geoprobe borings. Locations of the geoprobe borings are shown on Figure 2. Logs are found in

Appendix C.

One soil sample from each geoprobe boring (i.e., total of ten samples) was submitted to Lancaster

Laboratories, Inc. for chemical analysis to demonstrate compliance with the 10% confirmatory

sampling requirement specified in the FSAP. The locations of samples submitted for chemical

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analysis were selected based on a review of LIF data, with each sample depth selected from the

interval representing the LIF response above background. In general, samples were collected from

shallow soils immediately above the silt- and clay-rich lacustrine deposits blanketing the project

area, as a review of the CPT/LIF data indicated that, in general, the LIF signature above

background appeared to be limited to shallow soils above the silt- and clay-rich lacustrine deposits

(excluding locations where no LIF signature above background was identified). Results of the

chemical analysis completed by Lancaster Laboratories, Inc. are provided on Table 4.

A review of the chemical data indicates the highest parameter concentrations to be reported for soil

samples collected from within the approximate former lagoon areas. Soil samples collected from

geoprobe borings SB-8 (CPT-48), SB-9 (CPT-16) and SB-10 (CPT-58) exhibited the highest

parameter concentrations (in general) and are located within the approximate former lagoon areas.

Elevated parameter concentrations were also reported for samples collected at geoprobe borings

SB-4 (CPT-57) and SB-7 (CPT-56) located immediately adjacent to the former lagoon areas. The

soil sample collected from geoprobe boring SB-5 (CPT-4) exhibited lower parameter

concentrations than those reported for samples collected from nearby borings SB-8 (CPT-48) and

SB-9 (CPT-16) installed within the former lagoon areas, which lends support to soil boring SB-5

(CPT-4) being located between two separate former lagoon areas.

Consistent with the FSAP, test pits TP-1 through TP-6 were installed by Heritage Environmental

Services, Inc. (Heritage) on May 7, 1998 under the observation of an HAI representative. As

shown on Figure 4, the test pits were installed in close proximity to previously installed CPT/LIF

borings to allow for visual characterization of subsurface conditions. Data obtained via installation

of the test pits were used in addition to the geoprobe borings to further evaluate the CPT/LIF data.

Test pit logs are contained in Appendix C, and a summary of installation data associated with the

test pits is provided on Table 5.

As previously stated, the geoprobe borings and test pits were installed to allow for an evaluation of

the validity of data obtained via installation of the CPT/LIF borings. Soils encountered during the

completion of geoprobe and test pit installation activities were visually characterized by an HAI

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hydrogeologist. A review of data collected during the initial field investigation indicates that good

correlation exists between the CPT/LIF borings, geoprobe borings and test pits. As part of this

evaluation, each of the geoprobe logs were reviewed by Fugro, with the overall conclusion being

that, in general, good correlation between the geoprobe borings and CPT/LIF borings exists.

2.4 Collection of Sediment Samples

Fourteen sediment samples were collected from Williams Ditch (SED-BG and SED-001 through

SED-013) by HAI representatives from May 12 to May 15, 1998. Each of the sediment samples

were collected at the proposed locations presented in the FSAP. Sediment sample locations are

shown on Figure 3. Each sample was collected consistent with the procedures presented in the

FSAP and submitted to Lancaster Laboratories, Inc. for chemical analysis. Table 6 is a summary

of sediment sample collection activities, including date/time of collection and general notes

associated with sample collection. Results of the chemical analysis of sediment samples are

provided on Table 7.

A review of the chemical data indicates the highest parameter concentrations for sediment samples

to be reported was for sediment sample SED-005. Sediment sample SED-005 was collected in

close proximity to the former lagoon areas and surface water sample SW2, and as discussed in

Section 2.2, is located within the approximate extent of impacted shallow soils that have been

determined to be potentially affecting the quality of surface water and/or sediment in Williams

Ditch. Sediment samples SED-004 and SED-006 collected upstream and downstream of sediment

sample SED-005, respectively, indicate decreasing parameter concentrations. Sediment sample

SED-004 was collected from the approximate western (i.e., upstream) extent of impacted shallow

soils as determined using the CPT/LIF borings, with decreasing parameter concentrations reported

for sediment samples collected further upstream. Similarly, sediment sample SED-6 was collected

downstream from the approximate extent of impacted shallow soils, with sediments samples

collected further downstream exhibiting parameter concentrations significantly less than those

reported for sediment sample SED-005.

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3.0 RATIONALE FOR TECHNICAL APPROACH

Section IV, Item 6 of the Unilateral Administrative Order (UAO) identifies the primary factors,

pursuant to Section 300.415(b)(2) of the National Oil and Hazardous Substances Pollution

Contingency Plan (NCP), driving the implementation of time critical removal activities at the

Toledo Tie Treatment Site. The proposed remedy addresses these driving forces by mitigating

potential migration and exposure pathways through source removal and engineering controls.

Components of the time critical removal activities include:

1. Excavation of sediment to remove the most immediate source of contamination to the waters of

Williams Ditch.

2. Excavation of immediate source areas and migration pathway(s).

3. Modifications to the infrastructure to mitigate impacts caused by source removal and to

eliminate the primary migration pathway to Williams Ditch.

4. Installation of a subsurface barrier system with a french drain to control future migration to

Williams Ditch and to address areas of residual contamination.

The proposed remedy was selected because:

1. Creosote related contamination in the sediments accumulated in Williams Ditch was confirmed

by sampling and geochemical data. Removal of this source of contamination to the water in

Williams Ditch was considered the most effective option in preventing continued

contamination.

2. The immediate source of the creosote contamination to the sediments and waters of Williams

Ditch is identified as the two, westernmost lagoons. Creosote related contamination was

confirmed in the soil in these areas and a direct migration pathway from these areas to the ditch

was identified.

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3. Removal of the storm sewer and construction of the french drain will significantly reduce the potential for creosote migration to Williams Ditch and provide a mechanism for capturing residual creosote that remains after the immediate source has been removed.

Excavition of additional area should be considered

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4.0 IMPLEMENTATION OF THE REMEDY

During the time critical removal process, the immediate source areas will be excavated,

infrastructure will be removed and replaced as needed, sediment in Williams Ditch will be

excavated, and a subsurface barrier system will be constructed. The following is a brief

description of the activities required to implement these tasks.

4.1 Lagoon Excavation and Infrastructure Removal

KMC's expectation is that if transportation and disposal of excavated materials is chosen, Peoria

Disposal Company, (PDC) in Peoria, Illinois will be the preferred off-site disposal facility. If

thermal desporption is reasonably achievable, available, and is competitive, thermal treatment

could be an option. PDC has been used by KMC for previous projects involving wood treatment

sites and is in compliance with §300.440 of the National Contingency Plan. KMC will contract

directly with PDC for disposal of contaminated material. Excavated soils/sediments will be

classified as F034 under 40 CFR, Subpart D §261.31. The selected contractor will provide a full

time on-site waste management coordinator to track transportation and disposal activities.

4.1.1 Excavation, Backfill, and Site Grading

The area indicated on Sheet 2 of the plan set will be excavated to the subsurface lacustrine clay

layer which is at an average depth of approximately eight feet. There are several underground

utilities located within the excavation area. Please see the plan set and Section 4.1.2 for details

regarding excavating near these utilities and the removal and replacement of some of the utilities

present.

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An effort will be made to segregate the excavated soil by its level of visual contamination, if

possible. The data show creosote related contamination resides within an upper sand/silt stratum

and rests upon a lower confining layer of lacustrine silts/clays, typical of a dense, non-aqueous

phase liquid (DNAPL) plume. Observations during test pit excavation were that the DNAPL was

present in thin bands or seams within the sand/silt layer and was not distributed homogeneously

through the stratum. The data support limiting the excavation to the limits shown on the drawings,

considering the other controls that will be in place. The area will be backfilled in accordance with

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the final grade indicated in the plan set. Where possible, native soils from the upper few feet,

which are not visually contaminated with creosote, will be used to the degree practicable as

backfill. This will be done in conjunction with the construction of the subsurface barrier system,

the removal of the utilities as listed below, and the reconstruction of Frenchmens Road.

4.1.2 Utility Removal and Replacement

Refer to Sheet 3 of the plan set for all utility removal work. Storm sewer pipes #1 - #11 and all

associated fixtures will be removed. Additional storm water controls will be installed, subject to

City of Toledo concurrence with the proposed modifications, to insure the proper management of

storm water in this area.

Columbia Gas's 4" low pressure gas line may be temporarily removed or isolated if needed to

facilitate the excavation. It is currently anticipated that the underground Ameritech lines, water

main, and sanitary sewers will not be removed. Sanitary, water and electric service must be

maintained to the unoccupied distribution warehouse during and after removal activities.

Coordination with Ameritech, Toledo Edison, and Columbia Gas will be necessary during the

construction of the french drain. Toledo Edison will provide support during excavation activities

to maintain the integrity of the existing above ground electrical service.

Potential migration pathways along subsurface utility corridors will be addressed by sealing around

the pipes/trenches with a geosynthetic material or bentonite seal across the utility trench. This seal

applies to the Columbia Gas service line (if applicable), the sanitary tap, the water tap and the

below ground electrical conduit servicing the former Spartan building.

The utilities have been contacted and the project discussed with them. Any excavation, backfill,

site grading, and construction activities performed near these utilities will need to be coordinated

with the appropriate organizations.

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4.1.3 Road Replacement and Removal

For a delineation of the portion of Frenchmens Road to be removed and replaced, refer to Sheet 3

of the plan set. Sheets 5 and 6 provide detailed information on the replacement road.

The removal of the storm sewer in this area necessitates the removal and replacement of this

portion of Frenchmens Road to insure proper management of the surface water in the area. A

drainage swale along the south side of Frenchmens Road is required to insure proper drainage of

the area south of Frenchmens Road.

4.2 Sediment Removal

4.2.1 Sediment Excavation and Backfill

Two feet of sediment will be excavated from the portion of Williams Ditch that is delineated in the

plan set. The terminus point will be halfway between SED-009 and SED-010. The area between

SED-007 and SED-008 may require excavation upto 3.5 feet below existing ditch grade.

Confirmation of excavation depth will be made using field flourescence techniques. Excavated

areas will be backfilled with either general soil fill or lined with a flexible membrane liner and

filled with gravel to the design grade prescribed in the City of Toledo's Comprehensive Ditch Plan.

Field conditions at the time of excavation/backfill will dictate which method is selected.

4.2.2 Williams Ditch Rerouting

The contractor has proposed to isolate the ditch in sections to reroute the water around the

sediment removal area. Alternately, placement of a sheet pile coffer west of Arco Drive and

diverting flow past the terminus point may be used. The siphon dams will remain in place until it

has been demonstrated by visual observation that the water in Williams Ditch is free of visible oil

or oil sheen. Water will need to be rerouted during the sediment excavation, and soil backfill

activities.

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4.3 Subsurface Barrier (French Drain)

A french drain will be constructed to address the residual contamination that is not removed during

the excavation portion of the time critical removal action and to provide a mechanism to protect

sediment and surface water in Williams Ditch.

4.3.1 Excavation

The subsurface barrier will be installed once the storm sewer and associated backfill near Williams

Ditch has been removed. Placing the subsurface barrier in the initial stages of the project provides

the benefit of isolating the immediate source from Williams Ditch. See Sheet 4 in the plan set for

construction details.

4.3.2 Construction

Sheet piling will be driven on both sides of the french drain. Then the area between the sheet

piling will be excavated to the depth and grade indicated in the plan set. The geocomposite

consisting of geonet surrounded by geotextile fabric will be attached to the permanent sheet piling

and the geotextile fabric wrap, gravel, and pipe will be laid in place. The sump will be constructed

and each leg of the french drain will be connected to the sump. Then, the excavation will be

backfilled with clean soil to the final grade indicated in the plan set. Once the excavation has been

backfilled, the temporary sheet piling will be removed.

4.3.3 Operation

Liquids entering the french drain pipes will drain to the sump. DNAPL which accumulates in the

sump will be removed and water, once treated, is planned to be discharged to the City of Toledo

sewer system. A Warren-Rupp, double diaphragm pump or similar, using a footer valve or similar

set up will be used. The operational concept is to maximize the collection of creosote product and

minimize water production. A float system, with a dial up alarm system to alert KMC of system in

operation or excessive liquid level, will be incorporated. Alternately, a timer mechanism may be

used if it proves more effective in drawing free product to the french drain. A timer mechanism

may be preferable to a float system as maintenance could be become problematic due to product

build up on the float(s).

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4.4 Required Contractor Submittals

4.4.1 Site Specific Health and Safety Plan (HASP)

HAI has prepared a HASP addressing the requirements for the anticipated activities at the former Toledo Tie Treatment Site. This document is located in Appendix B of the Removal Action Work Plan. The minimum provisions of this plan are mandatory for all project personnel entering the site as well as site visitors. It should be acknowledged that the employees of other consulting and/or contracted companies may work in accordance with their own independent HASP's if it is more or as stringent as the one submitted by HAI. At a minimum, this document should be submitted to KMC for review prior to initiating any intrusive on-site activities.

The selected contractor is responsible for developing and implementing a HASP that addresses anticipated site health and safety concerns and specifically focuses on project tasks scheduled to be performed. The plan should also present required information including, but not limited to: identification of key personnel and lines of communication, training, medical surveillance, site hazards, work zones, personal safety, ambient and personal air monitoring, respiratory clearance, equipment cleaning and material safety data sheets, heat stress monitoring for permeable and non-permeable clothing, respirable contaminant action levels, levels of PPE, and emergency contingencies (i.e., injury, chemical release, etc.). Frequency and location should also be taken into consideration. As applicable, these criteria should be in document form and reviewed by KMC. Copies of training(s) should be tabulated and submitted as one bound document. Note all persons entering the site must show proof of OSHA 40-hr training, 8-hr refresher training, medical surveillance, and respirator clearance before they will be permitted to enter the site.

4.4.2 Stormwater Management Plan

The selected contractor will be responsible for ensuring that all stormwater is properly managed and segregated. Portable water holding tanks may be used to contain stormwater from excavations and, if needed, to serve as a holding mechanism for decontamination water.

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4.4.3 Dust/Odor Control Plan

Visible dust emissions will be addressed by periodically applying misted water or using an

equivalent approach. OHM has proposed to use a chemical deodorizer to control odors if need. A

detailed plan describing engineering controls, traffic control measures, etc will be required.

4.4.4 Air Monitoring Plan

The contractor will be responsible for conducting ambient and personal air monitoring throughout

the duration of all intrusive construction activities. Action levels, based upon site specific chemical

data are being developed and will be incorporated as an amendment to the site HASP.

4.4.5 Dewatering/Stabilization Plan

The selected contractor will be required to submit a detailed plan for handling and management of

contaminated sediments/soils. This plan must also include a liquids management program

incorporating at a minimum, details for the recovery, management, treatment (if any), and disposal

of potentially contaminated water. Anticipated sources of potentially contaminated water include,

but are not limited, to decontamination water, water entering excavations or draining from

excavated soils or sediments. The City of Toledo WWTP is the preferred receptor of potentially

contaminated water from the site and negotiations are ongoing to provide this capacity.

4.4.6 Contingency Plan

The site contingency plan will be amended as needed to address such things as on-site or off-site

spills of materials leaving the site, traffic emergencies, etc. The amended plan will be distributed to

the parties previously contacted and prior to initiating construction, reviewed with them.

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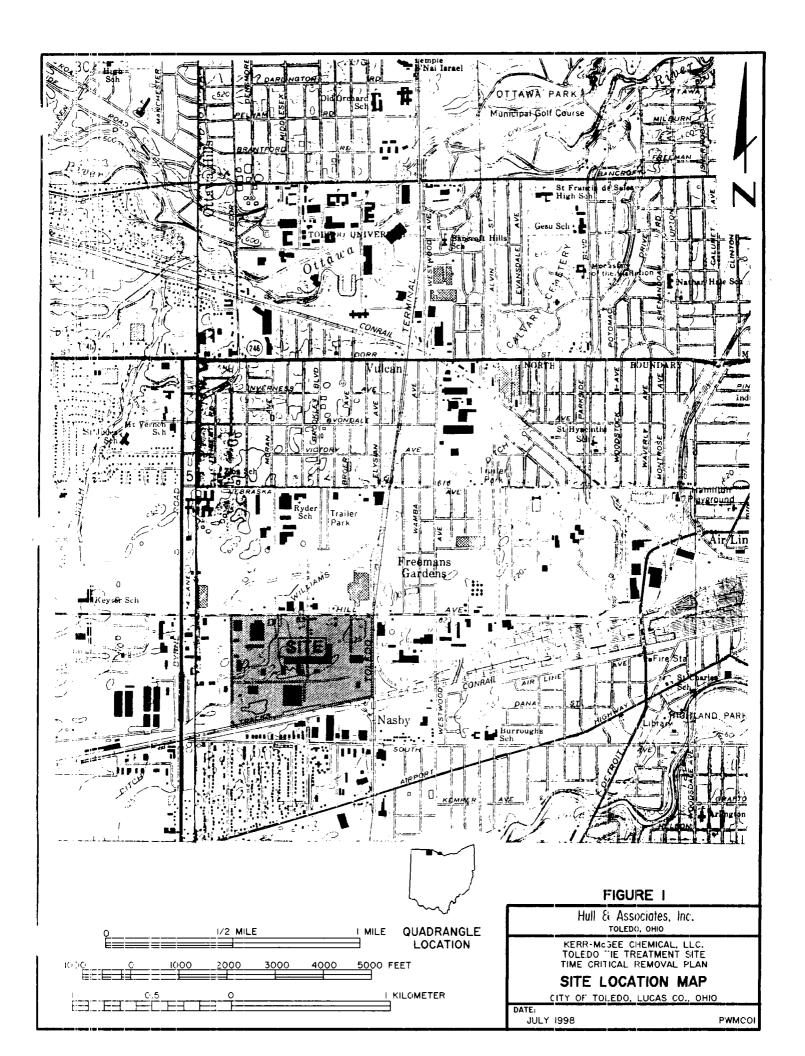
5.0 REFERENCES

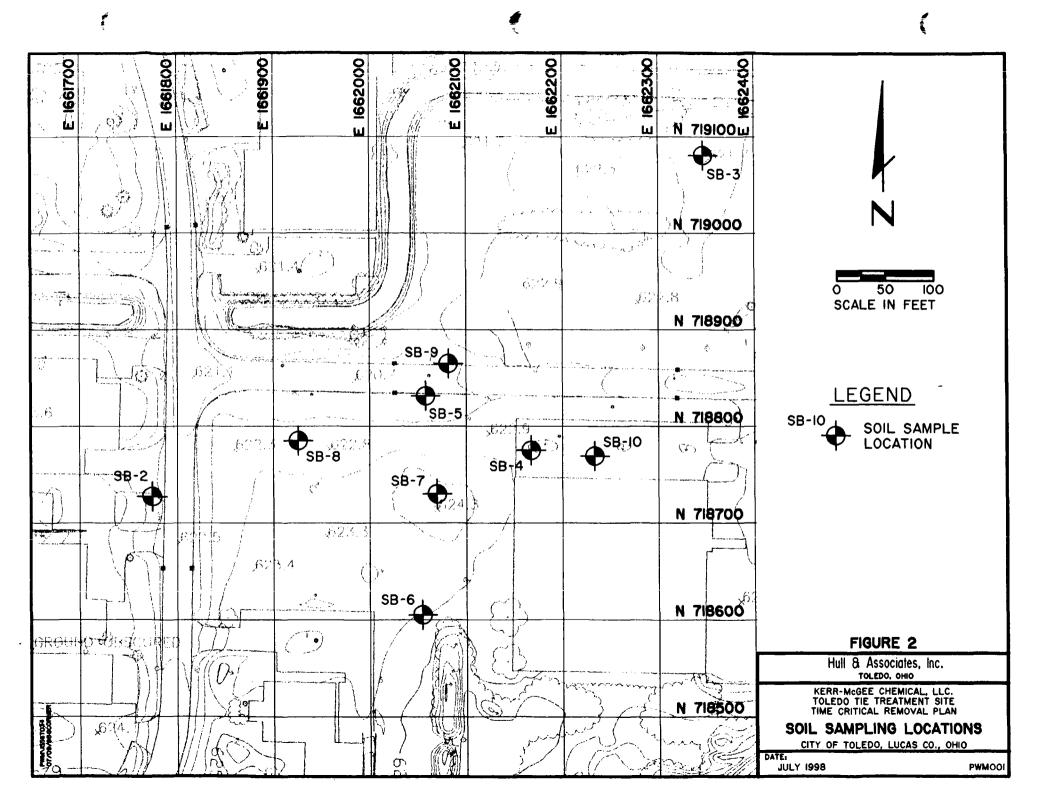
A variety of technical documents, administrative documents, and publications were referred to during the preparation of this document. Some of the references consulted are presented below.

- HAI. Removal Action Work Plan for the Toledo Tie Treatment Site, Hull & Associates, Inc. April 1998.
- U.S.EPA. <u>Interim Guidelines and Specifications for Preparing Quality Assurance Project Plans</u>. United States Environmental Protection Agency. 1983.
- U.S. EPA. <u>A Compendium of Superfund Field Operations Methods</u>, United States Environmental Protection Agency. 1987.
- American Society of Testing and Materials. "ASTM Standards Relating to Environmental Site Characterization", ASTM Publication Code Number: 03-418297-38, 1410 pp. 1997.
- U.S EPA. <u>Test Methods for Evaluating Solid Waste, Physical/Chemical Methods</u>, SW-846, 3rd Edition. United States Environmental Protection Agency. 1986.
- U.S. EPA. Methods for Chemical Analysis of Water and Wastes, EPA 600/4-79-020. United States Environmental Protection Agency. 1983.
- HAI. Appendix A. Field Sampling and Analysis Plan, Toledo Tie Treatment Site, Hull & Associates, Inc. April 1998.
- HAI. Appedix C. Quality Assurance Project Plan, Toledo Tie Treatment Site, Hull & Associates, Inc. April 1998.
- U.S. EPA. <u>Approaches for Remdiation of Uncontrolled Wood Processing Sites</u>, Office of Research and Development, United States Environmental Protection Agency, EPA/625/7-90/011, November 1990.

- U.S. EPA. <u>Presumptive Remedies, Technology Selection Guide for Wood Treatment Sites</u>, Office of Solid Waste and Emergency Response, United States Environmental Protection Agency. EPA540-F-93-020, April 1993.
- U.S. EPA. <u>Contaminats and Remedial Options at Wood Processing Sites</u>, Office of Research and Development, Risk Reduction Engineering Laboratory, EPA/600/R-92/182, October 1992.

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ш 720000 WICKER CONT. SCALE IN FEET LEGEND SED-009 SED-OIO SEDIMENT SAMPLE LOCATION SURFACE WATER SW-3 ● فينتط LOCATION SED-002 N 718500 FIGURE 3 Hull & Associates, Inc. TOLEDO, OHIO KERR-McGEE CHEMICAL, LLC.
TOLEDO TIE TREATMENT SITE
TIME CRITICAL REMOVAL PLAN
SEDIMENT AND SURFACE
WATER SAPPLING LOCATIONS CITY OF TOLEDO, LUCAS CO., OHIO JULY 1998

E-1661900 166200d 1662200 1662400 **1662300** ш 11.... N 719100 TP#2 N 719000 TP#I 50 SCALE IN FEET TP#4 N 718900 **LEGEND** TP#3 TEST PIT LOCATION N 718800 \boxtimes 3 2% 10 T_{3} TP#5 TP#6 N 718700 192 £24.91 12/3/4 11/21 N 718600 FIGURE 4 Hull & Associates, Inc. \$22 KERR-McGEE CHEMICAL, LLC. TOLEDO TIE TREATMENT SITE TIME CRITICAL REMOVAL PLAN **TEST PIT LOCATIONS** CITY OF TOLEDO, LUCAS CO., OHIO DATE **PWM**00I JULY 1998



TABLE 1 SURFACE WATER SAMPLING NOTES KERR-McGEE CHEMICAL, LLC TOLEDO TIE TREATMENT SITE

Sample Point	Sample Time	Temperature (degrees F)	pH (S.U)	Conductance (uohms/cm)	Notes
BG1	1120	68	7.1	894	Water sample collected from ditch at a location prior to where it enters the piped (underground) section of Williams Ditch. This locality is adjacent to cultivated land directly behind a machine shop.
SW1	1430	66.9	6.79	1352	Water sample collected at resurgence of Williams Ditch, adjacent to the concrete outfall, on the downstream side of the boom dam.
SW2	1330	68.7	7.83	1920	Water sample collected at resurgence of Williams Ditch, after flowing under Arco Drive, adjacent to the concrete outfall, on the downstream side of the boom dam. The water surface at this locality has areas of strong sheen. The field blank was taken following collection of this sample and decontamination of the sampler. Field blank sampling procedures consisted of pouring lab supplied water into the dipper and then transferring the water into the sample jars.
SW3	1230	65.5	7.69	1739	Water sample was collected approximately 100 feet downstream of the last siphon dam, on the downstream side of a boom dam. Water at this location is very shallow and the sample taken was very turbid due to disturbed bottom material.
SW4	1200	67.3	7.59	1766	Water sample was collected from the ditch directly upstream of the concrete pipe that carries Williams Ditch under Hill Avenue.

NOTES

Samples were taken as close as practical to the locations shown on Figure A1 contained in Appendix A of the Removal Action Work Plan.

Decontamination procedures for the "dipper" consisted of an initial alconox and potable water wash, followed by a DI water brush and rinse, and completed with a DI water spray rinse. Decontamination fluids were containerized and emptied into the waste water tank at the end of the sampling event.

TABLE 2 SUMMARY OF ANALYTICAL RESULTS SURFACE WATER SAMPLES KERR-McGEE CHEMICAL, LLC TOLEDO TIE TREATMENT SITE

	Analytical Results									
Parameter	SW-B1	SW-1	SW-2	SW-3	SW-4					
VOLATILES (ug/l)										
Tetrachloroethene	<1	2J	1J	<1	<1					
	SEMI-VOLATILES (ug/l)									
Phenanthrene	<1	<0.9	18	2 J	<0.9					
Anthracene	<1	<0.9	1J	<0.9	<0.9					
Fluoranthene	<1	<0.9	34	10	1J					
Pyrene	<1	<0.9	24	8J	<0.9					
Benzo(a)anthracene	<1	<0.9	5J	3J	<0.9					
Bis(2-ethylhexyl)phthalate	<2	<0.9	<2	3J	<0.9					
Chrysene	<1	<0.9	11	4.J	<0.9					
Benzo(b)fluoranthene	<1	<0.9	10	6J	<0.9					
Benzo(k)fluoranthene	<1	<0.9	4.J	2J	<0.9					
Benzo(a)pyrene	<1	<0.9	5J	4J	<0.9					
Indeno(1,2,3-cd)pyrene	<1	<0.9	4J	3J	<0.9					
Benzo(ghi)perylene	<1	<0.9	3 J	2J	<0.9					
	CHLORINA	TED HERBIC	IDES (ug/l)							
2,4,5-T	<0.0096	0.0236J	0.0381J	NA	NA					
2,4,5-TP	<0.0096	<0.095	0.0182J	NA	NA					
ORGA	NOCHLORIN	E PESTICIDE	S AND PCBs	(ug/l)						
PCB-1260	<0.095	<0.095	0.316J	<0.095	<0.095					
	N	IETALS (mg/	i)							
Arsenic	<0.005	<0.005	<0.005	0.017	<0.005					
Barium	0.0497J	0.0893J	0.0918J	0.32	0.0843J					
Chromium	<0.0066	<0.0045	<0.0066	0.0283J	<0.0066					
Copper	0.0047J	<0.0045	0.0054J	0.083	0.0052J					
Lead	<0.021	<0.021	<0.021	0.093J	<0.021					
Zinc	<0.009	0.0103J	0.0150J	0.537	0.0198J					
Mercury	0.000099J	0.000096J	<0.000023	0.000163J	0.000088J					

NA - Not Analyzed

J denotes that the concentration found is below the method detection limit and therefore can not be precisely quantified. The value indicated is a laboratory estimate.

Dinoseb was detected at concentration of 0.065J ug/l and Barium was detected at a concentration of 0.0061J mg/l in the equipment blank.

TABLE 3 **SOIL SAMPLING NOTES** KERR-McGEE CHEMICAL, LLC **TOLEDO TIE TREATMENT SITE**

Boring Number	CPT Equivalent	Sample Number	Depth of Sample (feet bgs)	Time Sampled	Sample Description
SB-1	BG-1	PWM001-SB1-SS3-D385	9.0-11.0	900	Sample collected @ 9 to 11 feet bgs from a saturated, loose, Brn fine SAND containing shell fragments. This unit overlies a Dk gray lacustrine clay.
SB-2	CPT-27	PWM001-SB2-SS2-D385	2.0-3.5	935	Sample collected @ 2 to 3.5 feet bgs from a slightly cohesive, Brn fine clayey SAND. This unit overlies a Digray lacustrine clay that contains small fine sand lenses.
SB-3	CPT-39	PWM001-SB3-SS2-D385	3.5-5.5	1025	Sample collected @ 3.5 to 5.5 feet bgs from alternating seams of Dk gray loose silt & Dk gray lacustrine clay.
SB-4	CPT-57	PWM001-SB4-SS2-D385	4.0-6.0	1105	Sample collected @ 4 to 6 feet bgs from Blk stained fine to med. SAND (4-5.5 feet) and Dk gray SILT (5.5-6.0 feet). These units demonstrated strong sheen and possessed creosote type odor and overlie a Dk gray lacustrine clay.
SB-5	CPT-4	PWM001-SB5-SS2-D385	5.0-7.0	1148	Sample collected @ 5 to 7 feet bgs from a Dk gray to Blk stained fine silty SAND that possessed a strong creosote type odor and sheen. This unit overlies a Dk gray lacustrine clay. Silt seams within the upper part of the lacustrine unit show some sheening also.
SB-6	CPT-61	PWM001-SB6-SS1-D385	6.0-8.0	1408	Sample collected @ 6 to 7.5 feet bgs from a saturated, loose, Gray fine SAND that possesses a strong creosote type odor and sheen. This unit overlies a Dk gray lacustrine clay.
SB-7	CPT-56	PWM001-SB7-SS3-D385	7.0-9.5	1536	Sample collected @ 7 to 9.5 feet bgs from a saturated, loose, Gray fine SAND containing shell fragments and possessing a strong creosote type odor and sheen. This unit overfies a Dk gray lacustrine clay.
SB-8	CPT-48	PWM001-SB8-SS2-D385	4.0-6.5	1612	Sample collected @ 4 to 6.5 feet bgs from a Blk stained Gray fine to med SAND that demonstrates a strong sheen and possesses a creosote type odor. This sand unit overlies a Dk gray lacustrine clay which contains very thin sand seams.
SB-9	CPT-16	PWM001-SB9-SS2-D385	4.5-6.0	1651	Sample collected @ 4.5 to 6 feet bgs from a Dk gray to Blk stained fine SAND and a Gray lacustrine CLAY containing fine sand and silt seams. Both the fine sand and the silt and sand seams within the upper part of the lacustrine unit possess strong creosote type odor and sheen.
SB-10	CPT-58	PWM001-SB10-SS3-D385	4.0-6.0	1725	Sample collected @ 4 to 6 feet bgs from a Blk stained Gray fine SAND that demonstrates a strong sheen and possesses a creosote type odor. Sand is saturated with free product @ 6 feet. The unit overlies a Dk gray lacustrine clay

NOTES

This field blank was collected adjacent to SB-6 by passing laboratory supplied water through the decontaminated macro sampler.

TABLE 4 SUMMARY OF ANALYTICAL RESULTS SOIL SAMPLES KERR-McGEE CHEMICAL, LLC TOLEDO TIE TREATMENT SITE

	Analytical Results										
	SB1-	SB2-	SB3-	SB4-	SB5-	SB6-	SB7-	SB8-	SB9-	SB10-	
Parameter	SS3	SS2	SS2	SS2	SS2	SS-2	SS3	SS2	SS2	SS2	
sample depth (feet bgs)	9-11	2.0-3.5	3.0-5.0	4.0-6.0	5.0-7.0	6.0-8.0	7.0-9.0	4.0-6.0	4.5-6.5	4.0-6.0	
CPT number	BG-1	CPT-27	CPT-39	CPT-57	CPT-4	CPT-61	CPT-56	CPT-48	CPT-16	CPT-58	
VOLATILES (mg/kg wet weight as received)											
Acetone	<0.007	<0.006	<0.006	<3.2	<3.1	0.007J	<3.3	<32	<3.4	<6.5	
Berizene	<0.001	<0.0009	<0.0009	7.4	1.4J	0.072	26	12	9.4	8.9	
Toluene	<0.001	<0.0009	<0.0009	7.3	1.4J	0.035	110	28	16	35	
Enhylbenzene	<0.001	<0.0009	<0.0009	24	4.6	0,45	100	32	9.5	21	
X _' /lene (total)	<0.001	<0.0009	<0.0009	48	9	0.3	210	76	38	66	
Styrene	<0.001	<0.0009	<0.0009	<0.45	<0.45	<0.001	<0.47	<4.6	5.4	6	
					ng/kg dry v						
2-picoline	<0.082	<0.79	<0.085	2.9J	<0.86	<0.081	<2	<2	2.2J	<2	
Phenol	<0.082	<0.79	<0.085	<1.6	<0.86	<0.081	<2	<2	26	<2	
2-methyphenol	<0.041	<0.4	<0.043	<0.67	<0.43	<0.04	<1	<1	19	<1	
3- and 4- methylphenol	<0.082	<0.79	<0.085	4.3J	2.4J	<0.081	<2	<2	53	<2	
2,4-dimetnylphenol	<0.082	<0.79	<0.085	4.4J	<0.86	<0.081	4.6J	4.1	39	23	
Naphthalene	<0.041	0.48J	<0.043	990	140	47	2800	1600	2200	4900	
2-methylnaphthalene	<0.041	<0.4	<0.043	230	43	20	680	500	1	810J	
Acenaphthylene	<0.041	18	<0.043	29	5.1	870	79	58	110	120	
Acenaphthene	<0.041	1.3J	<0.043	260	38	12	400	400	230J	640J	
Dibenzofuran	<0.041	.65J	<0.043	200	34	11	350	340	260J	550J	
Fluorene	<0.041	2J	<0.043	250	100	14	410 1000	990	310J	440J 1800J	
Phenanthrene Anthracene	<0.041	8.8 19	<0.043	640	1				850 470	290J	
	<0.041	97	<0.043	76 350	28 57	4.1	240 470	100 490	440	940J	
Fluoranthene Pyrene	<0.041 <0.041	95	<0.043 <0.043	260	48	8.7	370	390	330J	720J	
Benzo(a)anthracene	<0.041	66	<0.043	89	19	2.6	120	130	140J	260J	
Bis(2-ethylhexyl)phthalate	<0.082	<0.79	<0.045	<1.6	<0.86	0.1J	<2	<2	<2.1	<2	
Chrysene	<0.041	60	<0.043	74	18	2.4	120	110	120J	<2	
Benzo(b)fluoranthene	<0.041	87	<0.043	68	17	2.1	98	93	120	<1	
Benzo(k)fluoranthene	<0.041	30	<0.043	22	5.9	0.72	40	34	42	62	
Benzo(a)pyrene	<0.041	67	<0.043	54	13	1.7	80	76	95	150	
Indeno(1,2,3-cd)pyrene	<0.041	46	<0.043	25	6.7	0.95	40	38	52	79	
dibenz(a,h)anthracene	<0.041	12	<0.043	6.5	1.9J	0.27J	11	11	14	20	
benzo(ghi)perylene	<0.041	36	<0.043	21	5.3	0.79	33	32	40	63	
		GANOCHI	ORINE PE			(mg/kg dr	y weight)		L	L	
Akdrin	<0.000083		<0.000086		<0.0017	0.0055J	<0.0016	<0.0016	<0.0017	<0.0016	
Beta BHC	<0.000083	0.006J	<0.000086	<0.0016	<0.0017	<0.0016	<0.0016	<0.0016	<0.0017	<0.0016	
Delta BHC	<0.000083	0.0056J	<0.000086	0.0032J	0.0055J	0.0027J	0.0027J	0.0023J	0.0067J	<0.0016	
רנוס.	<0.00016	0.032	<0.00017	0.061	0.037	<0.0016	<0.0031	<0.0032	0.056	0.144	
DDE	<0.00016	<0.0031	<0.00017	<0.0031	0.0129J	<0.0031	<0.0031	<0.0032	<0.0032	<0.0031	
Eridosulfan I	<0.00016	<0.0016	<0.00017	<0.0016	<0.0017	<0.0016	0.0116	<0.0016	0.0096	0.0155	
Eridosulfan II	<0.000083	0.0042J	<0.00017	0.0051J	<0.0033	<0.0031	0.0124J	0.0043J	<0.0032	0.0076J	
Eridosulfan Sulfate	<0.00016	0.083	<0.00017	0.074	0.047	0.0076J	0.297	0.128	0.265	0.193	
Eridan	<0.00016	0.02	<0.00017	0.0041J	0.0064J	<0.0031	0.0079J	0.0047J	0.0095J	0.0154	
Eridrin Aldehyde	<0.00016	0.02	<0.00017	<0.0031	<0.0033	<0.0031	<0.0031	<0.0031	<0.0032	<0.0031	
Heptachlor	<0.000083		<0.000086		<0.0017	<0.0016	0.03	0.0074J	0.0261	0.0236	
Heptachlor epoxide	<0.000083		<0.000086		<0.0017	<0.0016	<0.0016	0.0027J	<0.0017	<0.0016	
Kepone	<0.00083	<0.016	<0.00086	<0.016	<0.017	<0.016	<0.016	0.04J	<0.017	0.144	
Methoxychlor	<0.00083	<0.016	<0.00086	0.093	0.075J	<0.016	0.339	0.239	0.35	0.679	
A	0.0047.1	0.00751			dry weigh		0.0000.1	0.0441	0.25	0.0252	
Mercury	0.0047J	0.0375J	0.0219J	0.0072J	0.0734J	0.0085J	0.0060J	0.011J 18	0.25 62	0.0253J 22	
Barrum	10.2J	48	81 1.04J	14 <0.23	46 0.64J	9.86J <0.23	11.5J <0.023	0.31J	0.88J	<0.23	
Cadmium	0.24J	0.51J	22.6	5.3	32.2	3.8J	6.5	7	16.5	9	
Chromium	5.4	11 12	16.6	5.5	9.9	4.01	5.1	7.1	13.5	4.3J	
Chromium	4.12J					<3.1	3.4J	4J	31	<3.1	
Lead	<3.2	11.2J	11.2J	<3.1	53 57	15	15	19	105	14	
Zinc	20	38	54 42.6	15 3.5	57	2.4	3.6	4.4	10.8	1.3	
Arsenic	4.2	4.7	12.6	<0.44	6.9 <0.47	<0.45	<0.45	<0.45	<0.46	0.58J	
Selenium	<0.46	<0.44	<0.47	~ U.44	~0.47	~0.45	~0.4 5	70.40	~U.40	U.J0J	

TABLE 5 TEST PIT EXCAVATION NOTES KERR-McGEE CHEMICAL, LLC TOLEDO TIE TREATMENT SITE

Test Pit Number	Adjacent to	Total Depth (ft. bgs)	Depth Contaminant Encountered (ft. bgs) (1)	Notes
TP#1	CPT#40	7.6	None Observed	No staining observed or odor detected. Very little water entering the excavation. Digging terminated in gray lacustrine clay deposits.
TP#2	CPT#38	9.6	None Observed	No staining observed or odor detected. First water encountered at approximately 4 ft. bgs along an interface between two lacustrine clay deposits. A greater quantity of water encountered in a sand (?) seam at approximately 8 ft. bgs. Digging terminated in gray lacustrine clay deposits.
TP#3	CPT#35	6	None Observed	No staining observed or odor detected. First water encountered at approximately 4 ft. bgs in an approximately 6 inch thick brown fine sand seam which overlies a mottled brown/gray lacustrine clay deposit below the stained sand. Digging terminated in gray lacustrine clay deposits.
TP#4	CPT#33	5.3	2.5 to 3	Staining observed in a sand rich seam at approximately 2.5 ft. bgs. Boring terminated in lacustrine clay deposit below the stained sand.
TP#5	CPT#48	7.5	4 to 6	Water and dark colored liquid (w/strcng peacock sheen) observed in a 6 inch sand seam at approximately 4 ft. bgs. Additional staining observed to approximately 6 ft. bgs. Excavation terminated in gray lacustrine clay encountered @ appoximately 6.5 ft. bgs.
TP#6	CPT#56	7.5	7	Water encountered at approximately 4 ft. bgs in a gray fine sand. Strong staining and dark colored liquids displaying a strong peacock sheen were encountered at approximately 7 ft. bgs in zones where the sand coarsened. The boring was terminated at this point due to the quantity of water entering the excavation and the amount of contaminants observed.

NOTES

bgs

Below ground surface

(1)

Based on olfactory and visual observations

TABLE 6 SEDIMENT SAMPLING NOTES KERR-McGEE CHEMICAL, LLC TOLEDO TIE TREATMENT SITE

Sediment Sample Number	Depth of Sample (feet bgs)	Date Sampled	Time Sampled	Sample Description
SED-BG	0-1.2	5/15/98	1355	Drove sampler and recovered 1.2 feet
SED-001	1.5-2.0	5/15/98		Drove sampler and recovered approximately 2.5 feet. Sed Profile: 0 to 1.5 organic material; 1.5 to 2.0 silt, 2.0 to 2.5 clay/silt. No flourescence detected.
SED-002	1-1.5	5/15/98		Drove sampler and recovered approximately 2.5 feet. Sed Profile: 0 to 1 organic material; 1.0 to 1.5 sand and silt; 1.5 to 2.5 clay/silt No flourescence detected.
SED-003	1-1.75	5/15/98		Drove sampler and recovered approximately 2.0 feet. Sed Profile: organic rich zone followed by sand followed by clay. Sand zone sampled. No flourescence detected.
SED-004	0-1.2	5/14/98	1835	Drove sampler and recovered 1.2 feet. Sed Profile: 1.2 feet of silt containing free product with clay in the very tip of the sampler.
SED-005	0-1.8	5/14/98	1300	Entire sample consisted of fine sand and silt held in suspension by Free Product.
SED-006	0.5-1	5/14/98	930	Base of ditch contained large gravel that required several attempts to bypass. Sed. Sample recovery approximately 1.2 ft. Sed Profile: 0 to 0.75 ft dark black organic rich loose sand and silt possessing a strong odor and sheen; 0.75 to 1.0 ft silt with strong odor and sheen (0 to 1 ft strong flourescence); 1 to 1.2 very soft gray silt and clay.
SED-007	2.5-3.5	5/14/98	825	Drove sampler approximately 3.8 feet - 3.6 feet recovered. Sed Profile: 0 to 1.5 very loose black silt and fine sand possessing a strong sheen and odor; 1.5 to 3.6 very soft gray silt and clay (strong flourescence).
SED-008	1.75-3.0	5/13/98	1820	Drove sampler approximately 4.0 feet - 3.3 feet recovered. Sed Profile: 0 to 2.5 ft dark black organic rich silt with some sand, strong sheen and some odor; 2.5 to 3.0 ft dark gray fine sand (strong flourescence); 3.0 to 3.3 ft clay.
SED-009	2.5-3.1	5/13/98	1602	Drove sampler approximately 3.9 feet - 3.5 feet recovered. Sed Profile: 0 to 2.8 ft organic rich material; 2.8 to 3.0 ft dark gray fine sand (strong flourescence); 3.0 to 3.3 ft clay.
SED-010	1.1-1.6	5/13/98	1215	Drove sampler approximately 3.5 feet - 2.1 feet recovered. Sed Profile: 0 to 1.6 ft organic rich silt; 1.6 to 2.1 ft fine sand with little silt. No flourescence detected.
SED-011	1.3-2.6	5/13 /98	950	Drove sampler approximately 3.6 feet - 2.7 feet recovered. Sed Profile: 0 to 1.3 ft organic rich silt; 1.3 to 2.6 ft fine sand with little silt containing a thin organic rich seam @ 1.6 ft.; 2.6 to 2.7 ft soft dark gray clay with black staining. No flourescence detected.
SED-012	0.8-1.6	5/13/98	830	Drove sampler approximately 3.5 feet - 1.7 feet recovered. Sed Profile: 0 to 0.6 ft organic rich silt; 0.6 to 1.5 ft laminated silt and sand; 1.5 to 1.7 ft soft gray clay. Sample collected from the laminated fine sand and silt based on flourescence.
SED-013	0.9-1.2	5/12/98	1705	Drove sampler approximately 3.8 feet - 2.8 feet recovered. Sample collected from a gray clayey sand seam dividing a dark black organic rich seam. (FID response: 61.9 ppm - no response in adjacent sediments)

NOTES

The field blank was collected adjacent to SED-004 by passing laboratory supplied water through the decontaminated sediment sampler.

TABLE 7 SUMMARY OF ANALYTICAL RESULTS SEDIMENT SAMPLES KERR-McGEE CHEMICAL, LLC TOLEDO TIE TREATMENT SITE

	Analytical Results (mg/kg) SED-001 SED-002 SED-003 SED-004 SED-008 SED-006 SED-008 SED-009 SED-010 SED-011 SED-012 SED-013													
Parameter	SED-BG	SED-001	SED-002	SED-003	8ED-004	SED-008	SED-006	SED-007	SED-008	SED-009	SED-010	SED-011	SED-012	SED-013
VOLATILES														
Xyle∩e	<0.001	<0.002	<0.002	0.007J	150	910	29	3.1	3.1	0.010J	0.016	<0 002	<0.002	0.036J
Acetone	<0.009	0.021J	<0.011	0.033J	<27	<15	<5.7	<1.4	<1.8	0.045J	0.039J	<0.011	0.013J	<0.077
Ethylbenzene	<0.001	<0.002	<0.002	<0.002	76	410	11	1.7	1.8	<0.003	<0.002	<0.002	<0.002	<0.011
Toluene	<0.001	<0.002	<0.002	<0.002	<3.8	360	1.4J	<0.19	<0.26	<0.003	<0.002	<0.002	<0.002	<0.011
Benzene	<0.001	<0.002	<0.002	<0.002	<3.8	77	<0.82	<0.19	<0.26	<0.003	<0.002	<0.002	<0.002	<0.011
Vinyl acetate	<0.004	<0.006	<0.005	<0.007	40	<6.6	<2.5	<0.58	<0.77	<0.008	<0.006	<0.005	<0.005	<0.033
						BEMI-VOLA	TILES							
3- and 4-methylphenol	<0.089	<0.14	<0.11	<0.14	<5.1	78J	<0.87	<1	<1.4	<1.7	<0.67	<0.1	<0.52	<2.9
Acetophenone	<0.044	<0.071	<0.053	<0.071	<2.5	15J	<0.44	<0.52	<0.68	<0.87	<0.34	<0.05	<0.26	<1.5
2,4-dimethylphenol	<0.089	<0.14	<0.11	<0.14	<5.1	95J	<0.87	<1	<1.4	<1.7	<0.67	<0.1	<0.52	<2.9
Naphthalene	<0.044	0.100J	0.096J	0.080J	1900	45000	800	220	820	<0.87	0.390J	0.080J	<0.26	<1.5
2-methylnaphthalene	<0.044	0.081J	0.085J	0.1	900	11000	230	52	290	0.980J	<0.34	<0.05	<0.26	<1.5
Acenaphthylene	<0.044	0.120J	0.320J	0.24J	38	850	9.4	2.9J	16	17	2.6J	0.73	2J	13J
Acenaphthene	<0.044	0.290J	0.470J	0.400J	680	8800	200	53	310	28	1.8J	0.99	2.9	28
Dibenzofuran	<0.044	0.210J	0.490J	0.330J	570	7000	150	45	240	22	1.2J	1.1	2.2J	25
Fluorene	<0.044	0.440J	1.1	0.680J	800	8900	200	70	340	52	2.3J	2.6	5.1	57
N-nitrosodiphenylamine	<0.044	0.330J	0.330J	0.400J	<2.5	<15	<0.44	<0.52	<0.68	<0.87	<0.34	<0.05	<0.26	<1.5
Phenanthrene	0.150J	3.8	5.4	4	1800	21000	460	150	860	320	9.8	9.9	25	230
Anthracene	<0.044	0.85	0.86	0.59J	220	3100	47	19	79	38	3.7	2	4.9	38
Fluoranthene	0.260J	6.7	8.3	6.2	1000	11000	250	78	570	480	33	14	61	350
Pyrene	0.240J	6.6	6.7	5.8	750	8200	190	51	430	360	28	11	46J	260
Butyl benzyl phthalate	<0.089	2.3	0.180J	0.420J	<5.1	<29	<0.87	<1	<1.4	<1.7	<0.67	<0.1	<0.58	<2.9
Benzo(a)anthracene	0.110J	2.7	2.2	1.9	250	2700	64	20	150	130	13	3.9	15	95
Bis(2-ethylhexyl) phthalate	0.110J	2.2	0.76	1.4	5.3	<29	<0.870	<1	1.4J	2.3J	1.7J	0.440J	0.640J	<2.9
Chrysene	0.140J	3.7	2.4	2.8	210	2200	43	16	130J	130	16	4.2	15	93
Di-n-octyl phthalate	<0.089	0.16	<0.11	<0.14	<5.1	<29	<0.87	<1	<1.4	<1.7	<0.67	<0.1	<0.52	<2.9
Benzo(b)fluoranthene	0.190J	4.4	2.4	3.5	190	1700	40	15	130J	130	17	4.7	14	88
Benzo(k)fluoranthene	0.071J	1.5	0.84	1.1	66	610	13	4.5J	35	41	6.2	1.7	4.7	32
Benzo(a)pyrene	0.130J	3	1.5	2.1	150	1400	32	11	71	75	11	3	9.6	59
Indeno(1,2,3-cd)pyrene	0.110J	2.7	1.1	1.9	80	690	16	5.6	38	44	7.5	2.1	5.5	33
Dibenz(a,h)anthracene	<0.044	0.55J	0.280J	0.430J	22	180	4.1J	1.6J	10	11	2J	0.54	1.5J	9.1J
Benzo(ghi)perylene	0.099J	2.3	0.91	1.7	65	570	13	4.4J	31	36	6.2	1.7	4.4	26

Concentrations of all chemicals were non-detect in equipment and trip blanks submitted with these samples.

TABLE 7 (cont.) SUMMARY OF ANALYTICAL RESULTS SEDIMENT SAMPLES KERR-McGEE CHEMICAL, LLC TOLEDO TIE TREATMENT SITE

	Analytical Results (mg/kg dry weight)													
Parameter	SED-BG	SED-001	SED-002	8ED-003	8ED-004	SED-005	SED-008	SED-007	8ED-008	SED-009	SED-010	SED-011	SED-012	SED-013
CHLORINATED HERBICIDES														
Dinoseb	<0.0023	0.199J	<0.0027	0.086J	<0.1	NA								
2,4,5-TP (Silvex)	<0.00044	0.146	<0.00053	<0.014	0.045J	NA								
2,4,5-T	<0.00044	0.071J	0.0028	0.098	0.093J	NA								
ORGANOCHLORINE PESTICIDES AND PCBs														
Aldrin	<0.00089	<0.0029	<0.0021	<0.0029	<0.041	<0.024	<0.018	0.005J	<0.0028	<0.0035	<0.0027	<0.002	<0.0021	<0.0029
Alpha BHC	<0.00089	<0.0029	<0.0021	<0.0029	<0.041	<0.024	<0.018	<0.0021	0.0087J	<0.0035	<0.0027	<0.002	<0.0021	0.0054J
Delta BHC	<0.00089	<0.0029	<0.0021	<0.0029	0.075J	0.057J	0.042J	0.0063J	0.0121J	<00035	<0.0027	<0.002	<0.0021	0.0116J
Chlordane	0.170J	<0.14	<0.11	<0.14	<2.0	<1.2	<0.86	<0.1	<0.140	<0.17	<0.13	<0.099	<0.1	<0.14
DDT	0.0758	0.22	0.037	0.099	<0.079	0.79	0.042J	0.0126J	0.112	0.126	0.089	0.0185J	0.0195J	0.101
DDE	0.271	1	0.216	0.584	0.344J	0.33	<0.034	0.0053J	0.207	0.262	0.333	0.045	0.025	0.163
DDD	0.246	1.03	0.214	0.452	0.222J	<0.046	<0.034	0.0094J	0.147	0.245	0.3	0.029	0.033	0.347
Dieldrin	0.0064J	0.08	<0.0041	<0.0057	<0.079	<0.046	<0.034	0.0094J	<0.0053	0.0078J	0.0055J	0.0082J	<0.0041	<0.0057
Endosulfan II	<0.00089	<0.0056	<0.0041	<0.0057	<0.079	0.091J	<0.034	<0.004	0.0074J	<0.0068	<0.0053	<0.0039	<0.0041	0.0059J
Endosulfan Sulfate	<0.0017	<0.0056	0.015J	<0.0057	0.5	2.84	0.28	0.038	0.153	0.071	0.0137J	<0.0039	0.0146J	0.115
Endrin	<0.0017	<0.0056	<0.0041	<0.0057	<0.079	0.124J	<0.034	<0.004	<0.0053	<0.0068	<0.0053	<0.0039	<0.0041	0.0141
Endrin Aldehyde	<0.0017	<0.0056	<0.0041	<0.0057	0.296J	<0.046	<0.034	<0.004	<0.0053	<0.0068	<0.0053	<0.0039	<0.0041	<0.0037
Methoxychlor	<0.0089	<0.029	<0.021	<0.140	<2.0	3.8	<0.180	<0.021	0.31	0.21	<0.027	<0.020	<0.021	0.19
Mercury	0.0653J	0.0931J	0.0244J	0.125J	0.127J	0.0664J	0.0155J	0.0536J	0.0836J	0.113J	0.094J	0.0441J	0.0347J	0.0983J
Barium	26	126	67	127	160	54	44	78	124	140	91	44	44	79
Cadmium	<0.25	2.89J	1.15	2.91J	3.41J	0.93J	<0.25	0.46J	1.49J	3.53J	3.2J	0.65J	0.86J	2.09J
Chromium	5.9	26.6	14.2	28.6	32	10.5	12.6	17.4	23.2	35	24.4	13.1	11	26.8
Copper	7.8	60.6	21.6	49.6	66	18.1	11.1	22.9	35.3	50	41.3	16.4	16.4	36.3
Silver	<0.59	<0.94	<0.70	<1	<1.3	<0.77	<0.58	<0.68	<0.90	<1.2	<0.89	<0.66	< 0.69	1.9
Zinc	34	297	112	264	408	102	39	65	210	405	272	89	83	207
Lead	11.1	162	65	133	165	50	10.7	16	125	202	117	52	69	183
Arsenic	1.9	13.2	6.8	13.2	15.8	10.7	4.8	7.5	15.1	22.1	15.2	7.6	7.7	14
Selenium	< 0.49	<0.79	<0.59	<0.80	<1.1	1.64J	<0.48	<0.57	<0.76	<1	<0.75	<0.56	<0.58	<0.81

NA - Not Analyzed

Concentrations of all chemicals were non-detect in equipment and trip blanks submitted with these samples.

J denotes that the concentration found is below the method detection limit and therefore can not be precisely quantified. The value indicated is a laboratory estimate.

APPENDIX A

Overall Site Map

HULL & ASSOCIATES, INC. FOLEDO. OHIO

JULY 1998 PWM001.100.0063

SDMS US EPA Region V

Imagery Insert Form

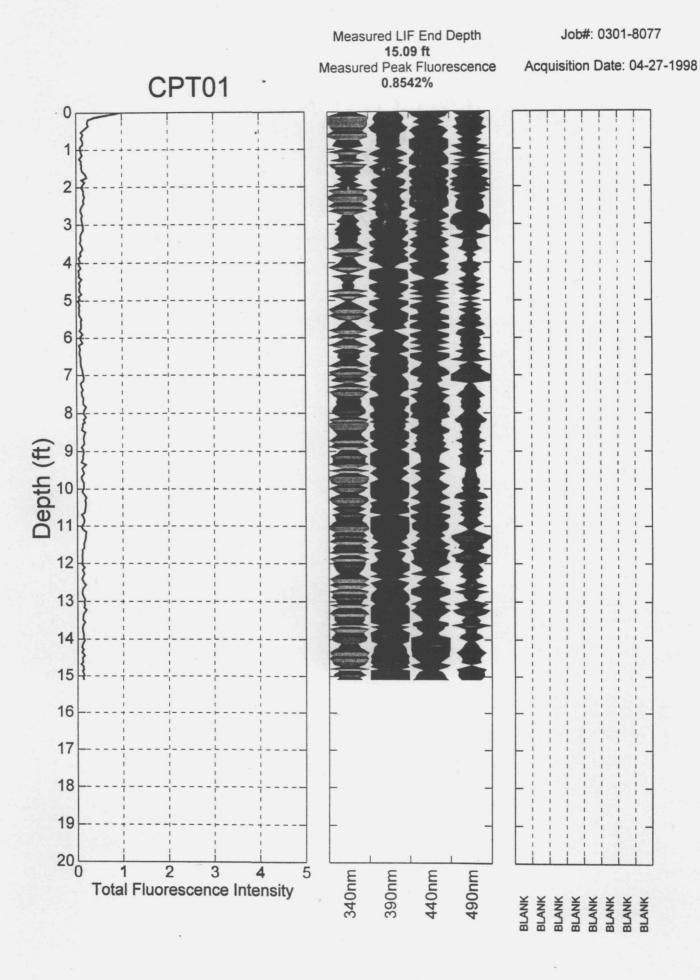
Some images in this document may be illegible or unavailable in SDMS. Please see reason(s) indicated below:

	Illegible due to bad source documents. Image(s) in SDMS is equivalent to hard copy.
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	APPENDIX A: OVERALL SITE MAP
	Other:

APPENDIX B

ROST™ Logs And LIF Signature Thickness Map

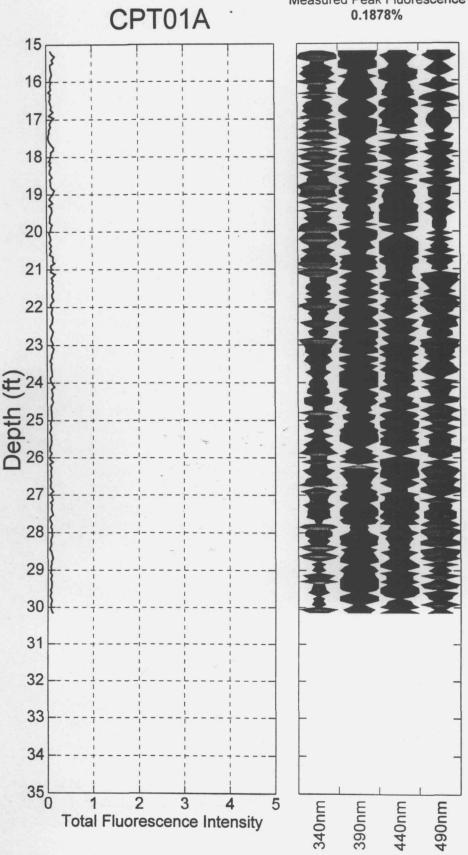
JULY 1998 PWM001.100.0063 ROST™ LOGS

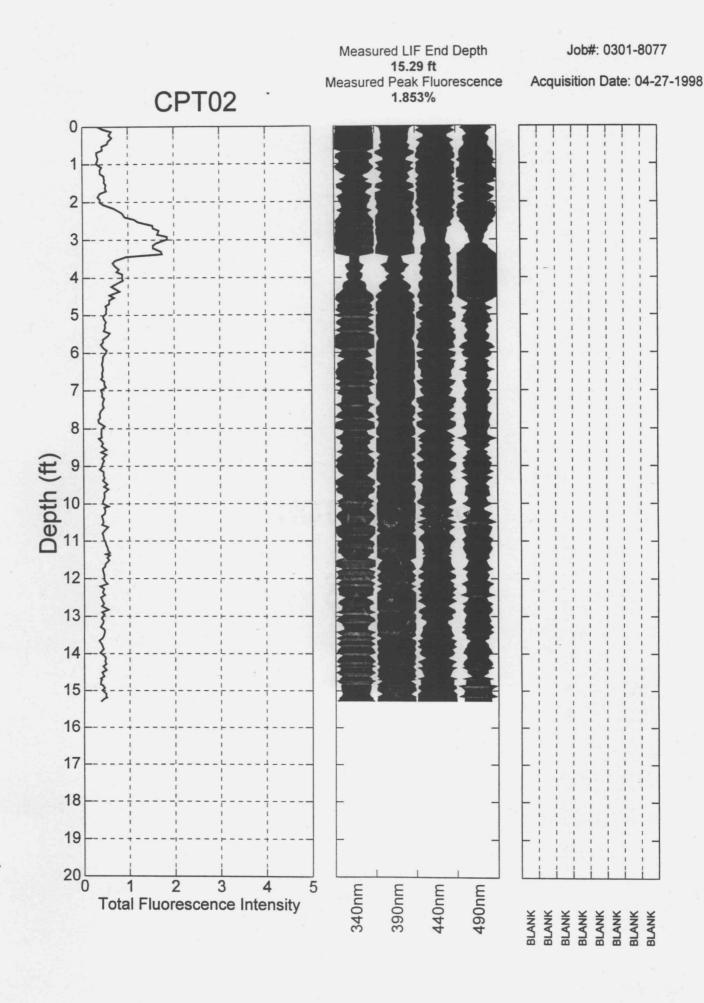


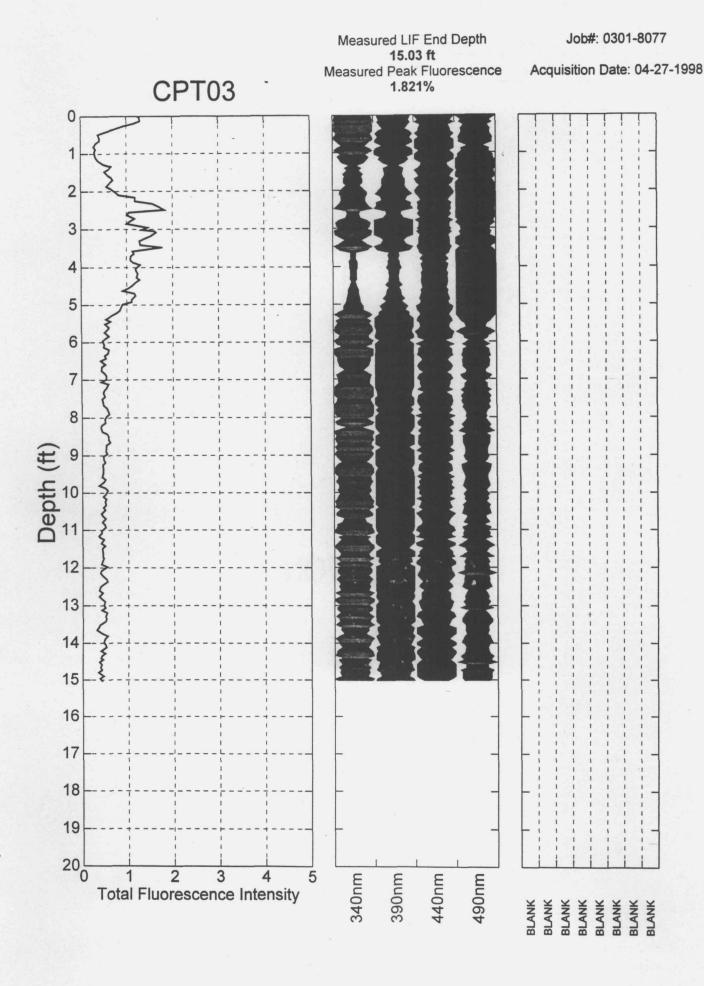
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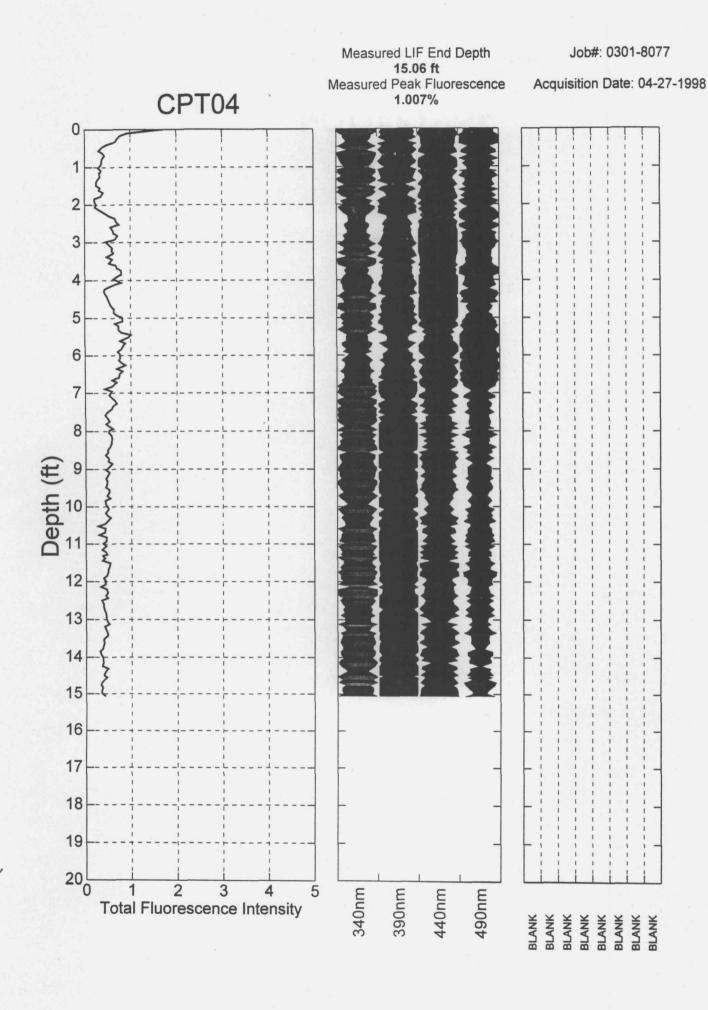
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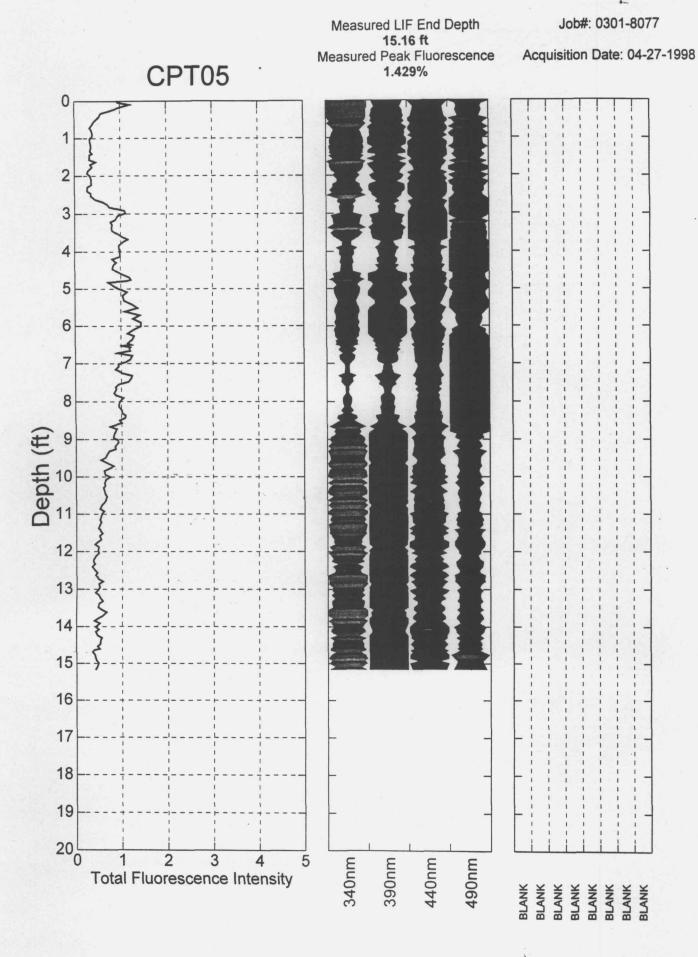
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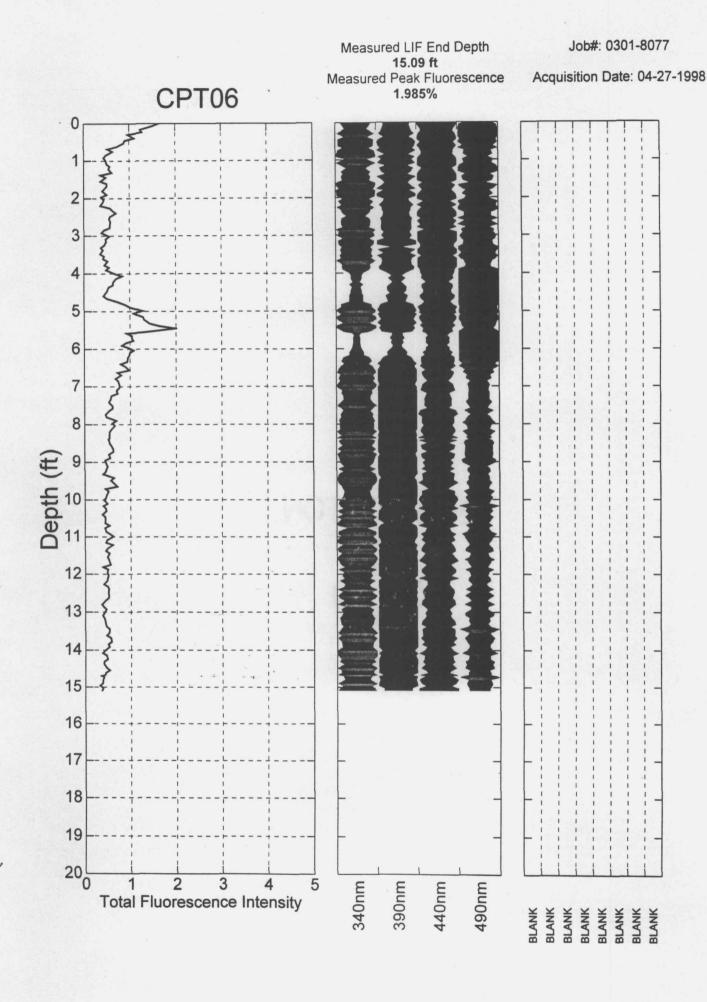


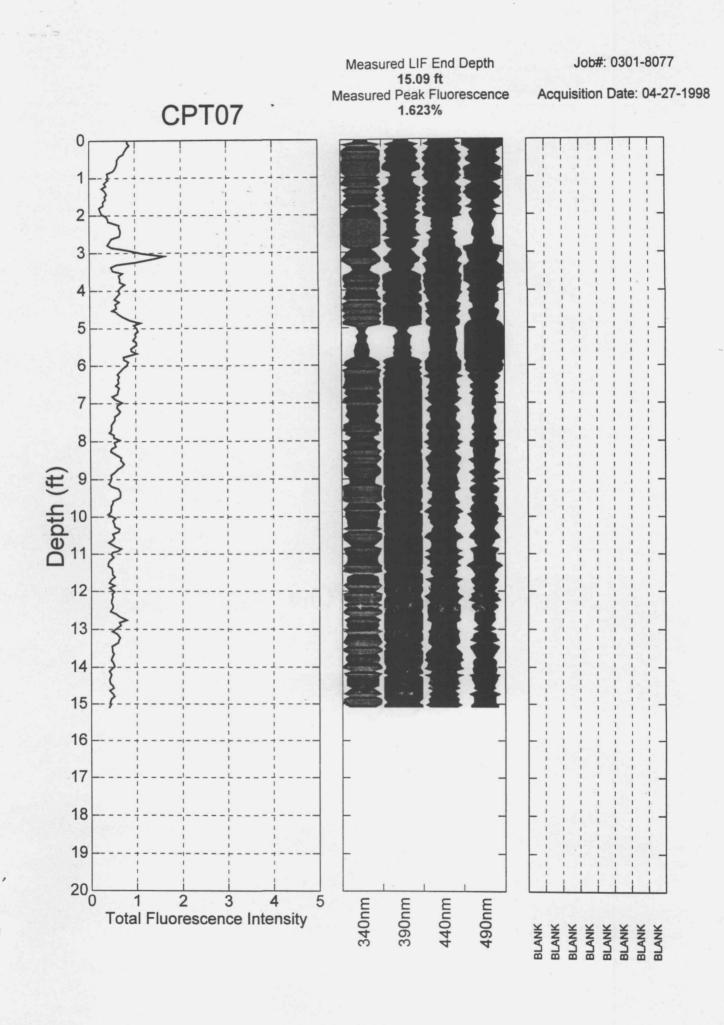


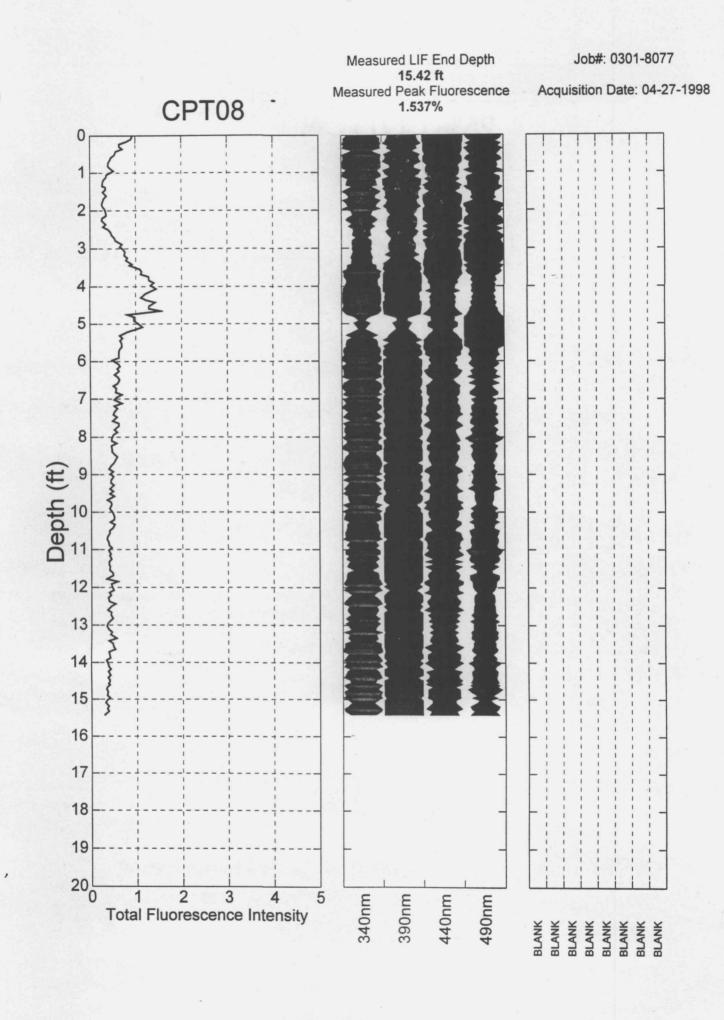


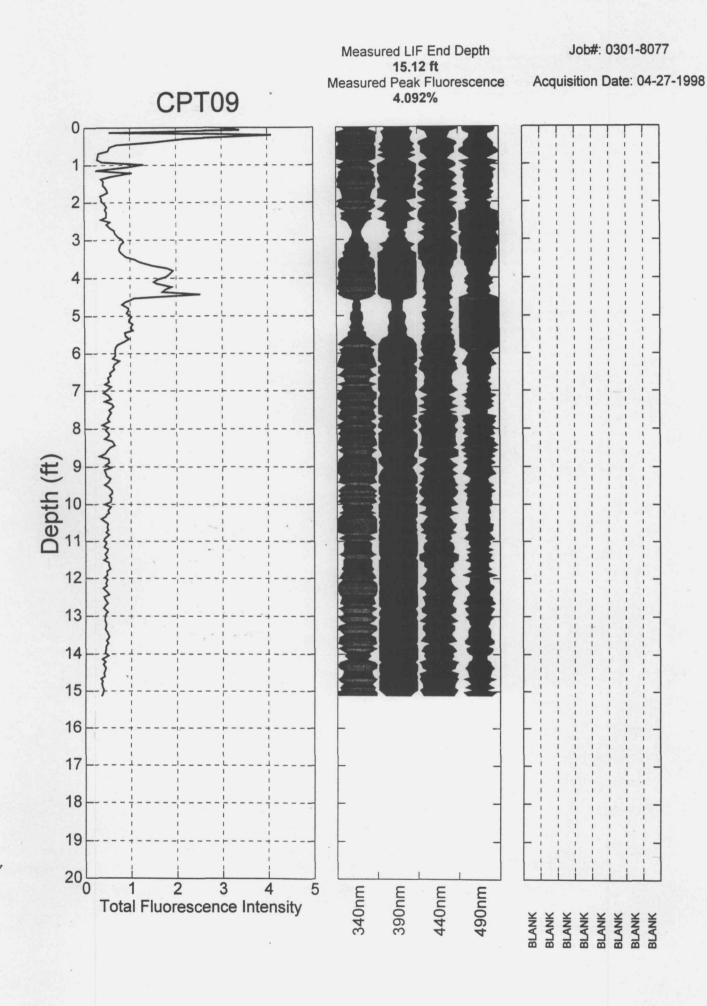


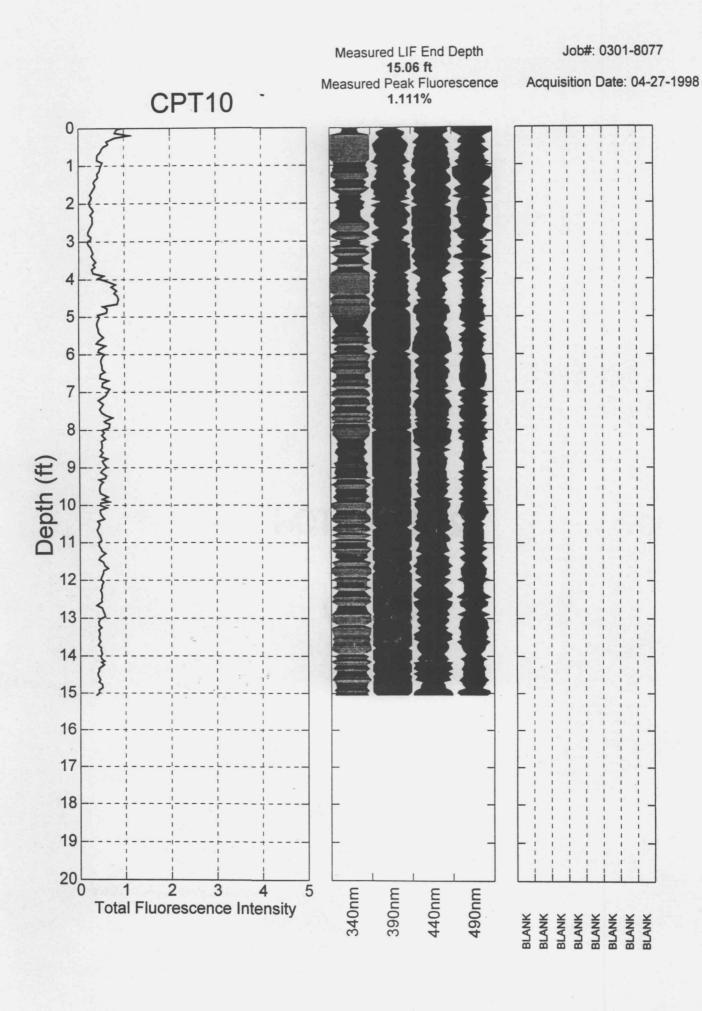


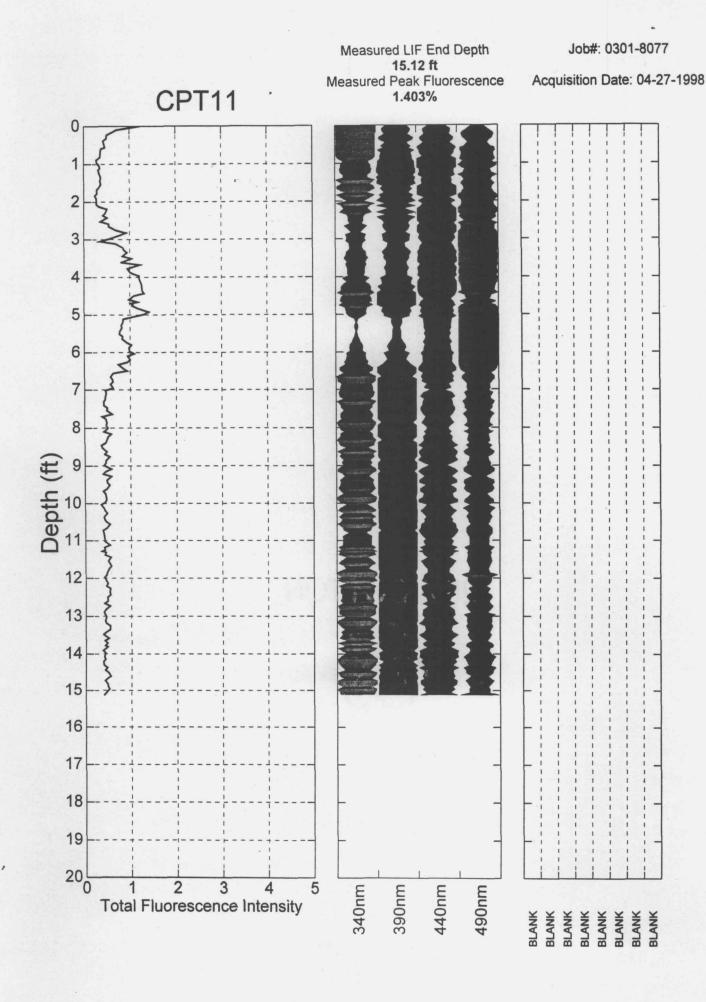


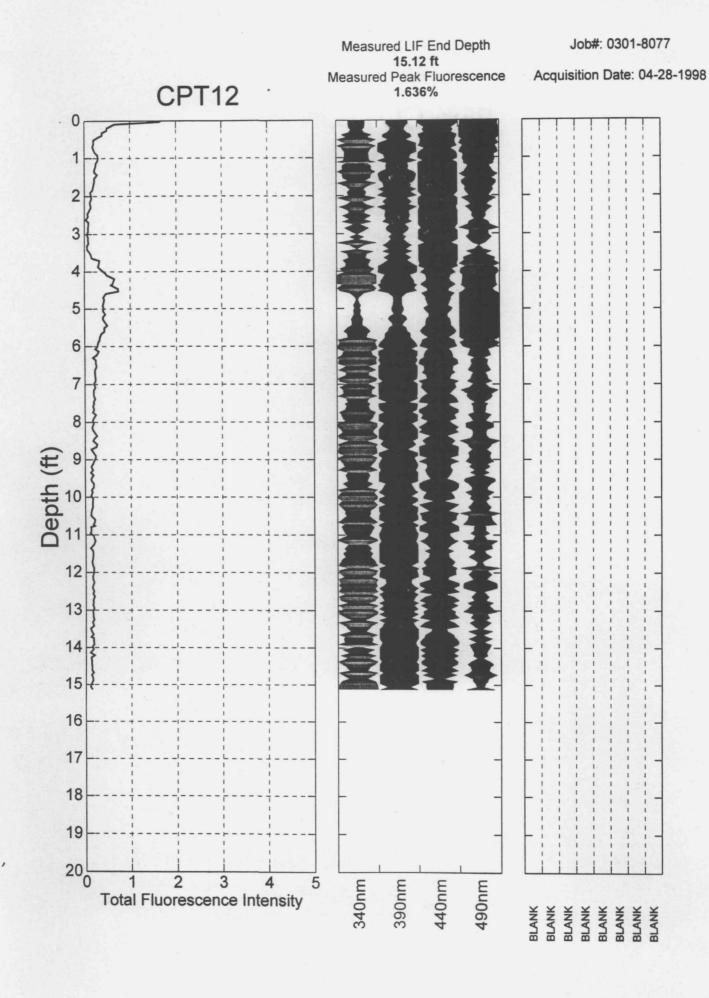


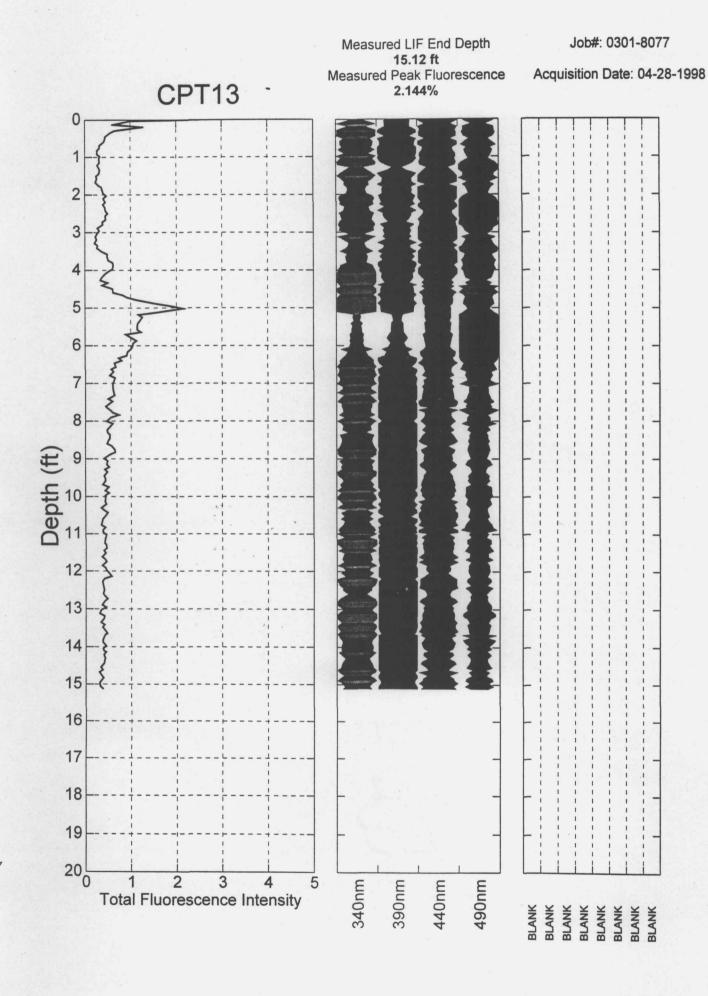


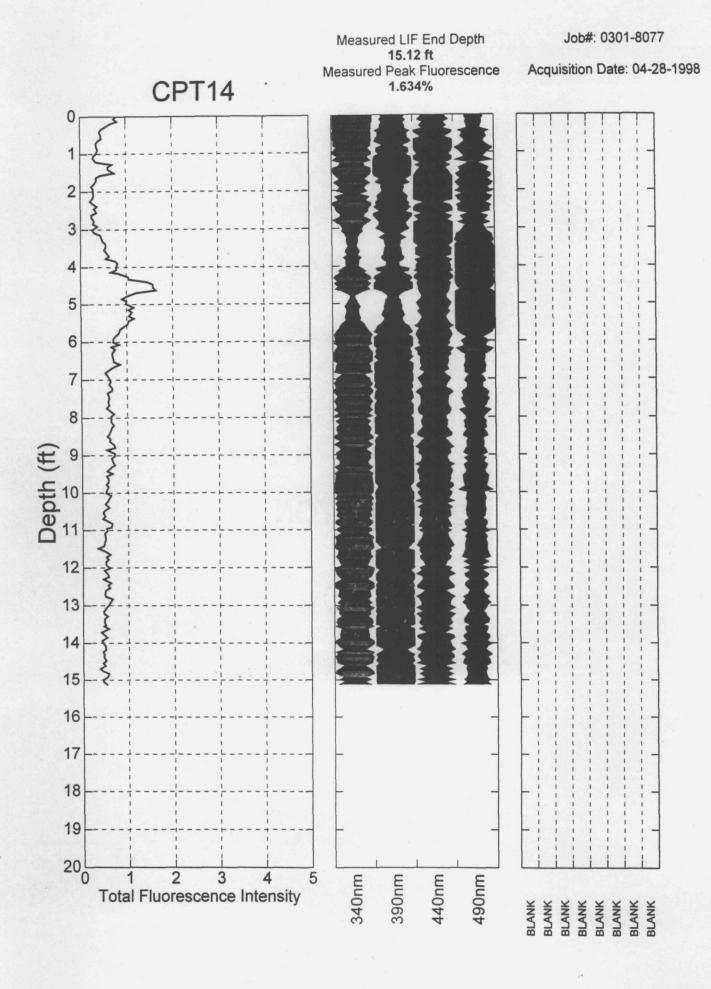


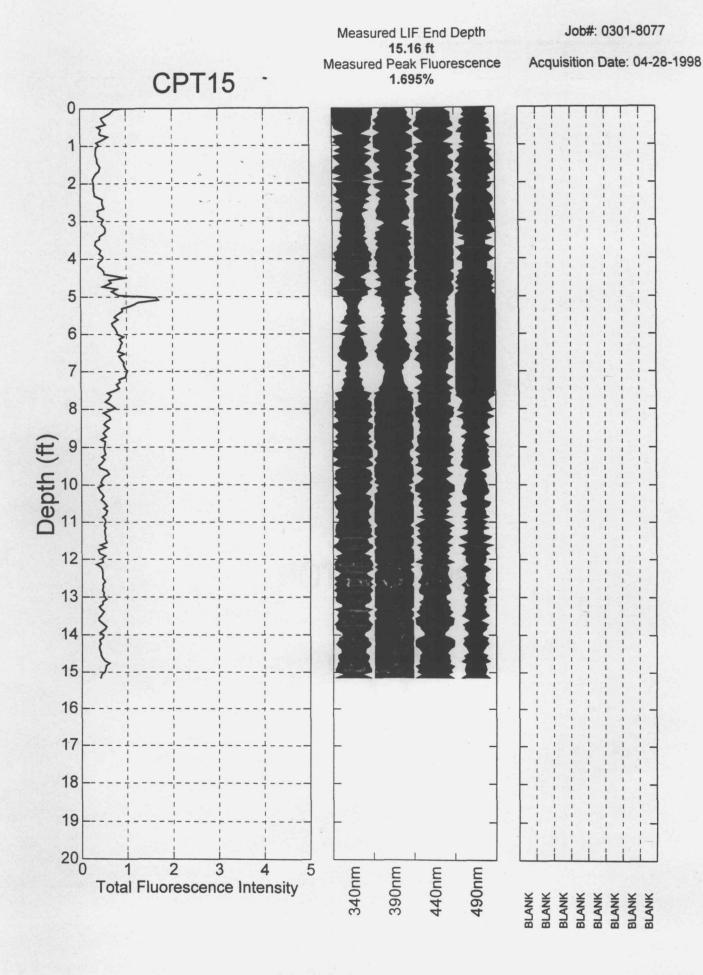


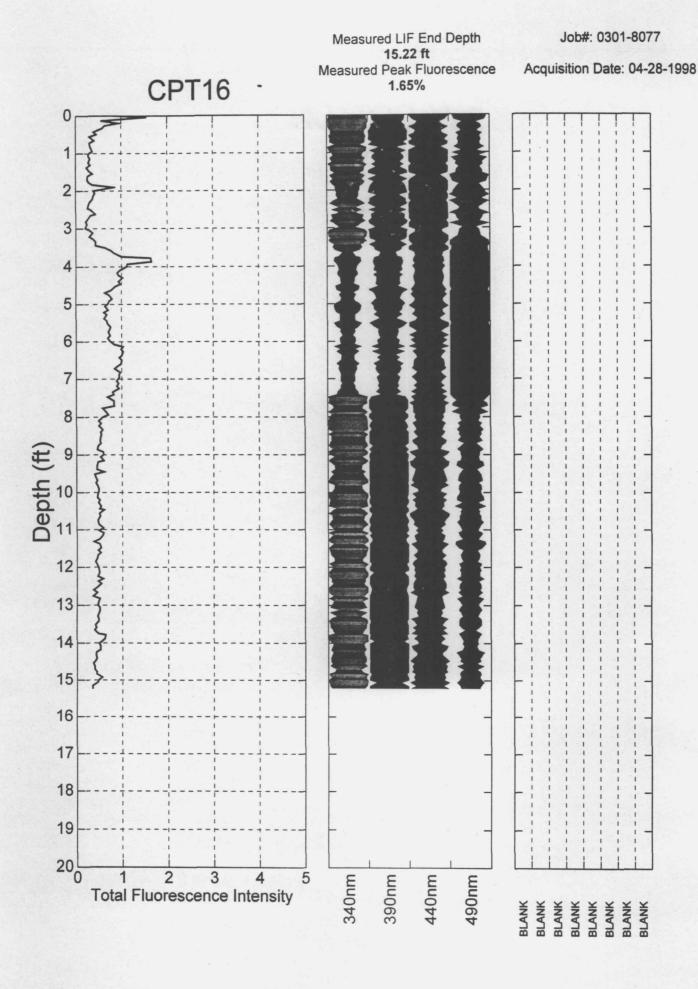


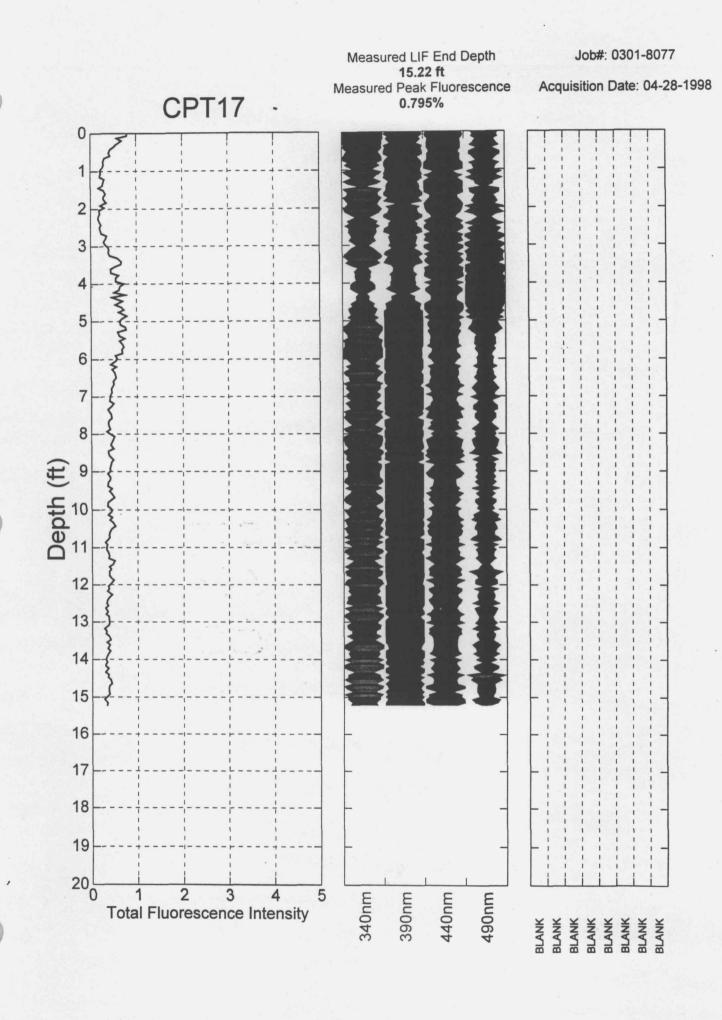


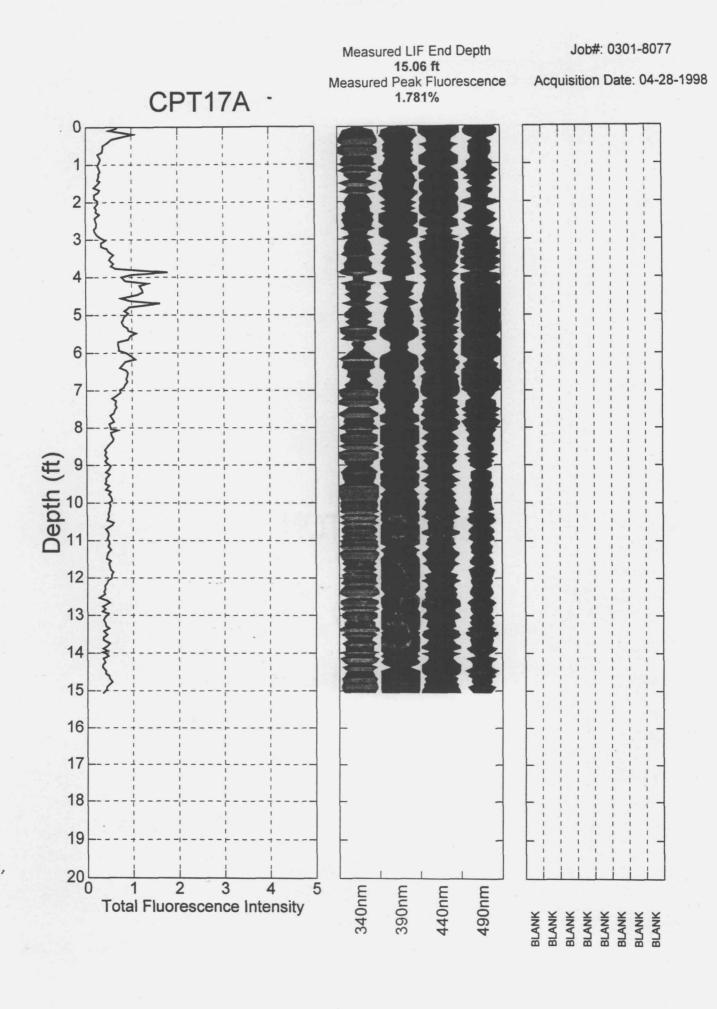


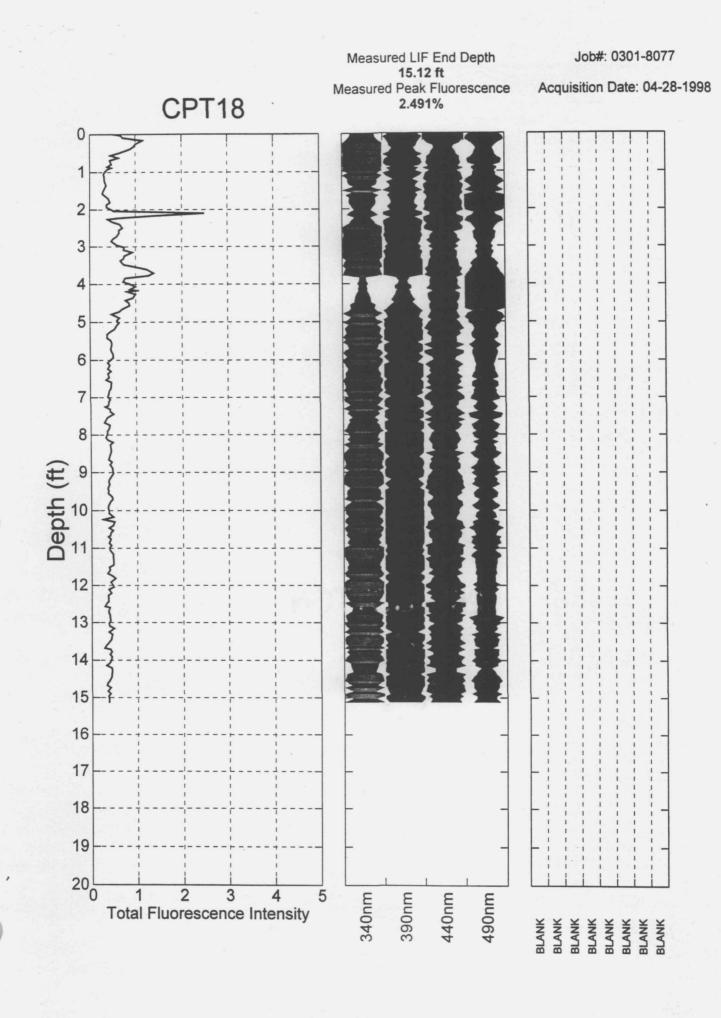


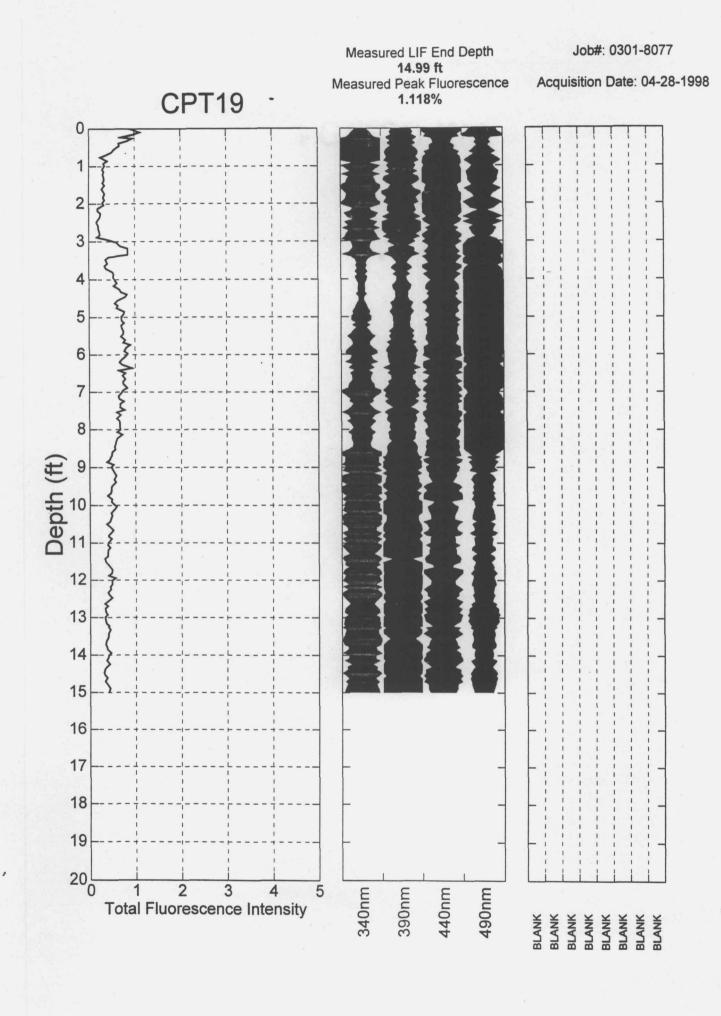


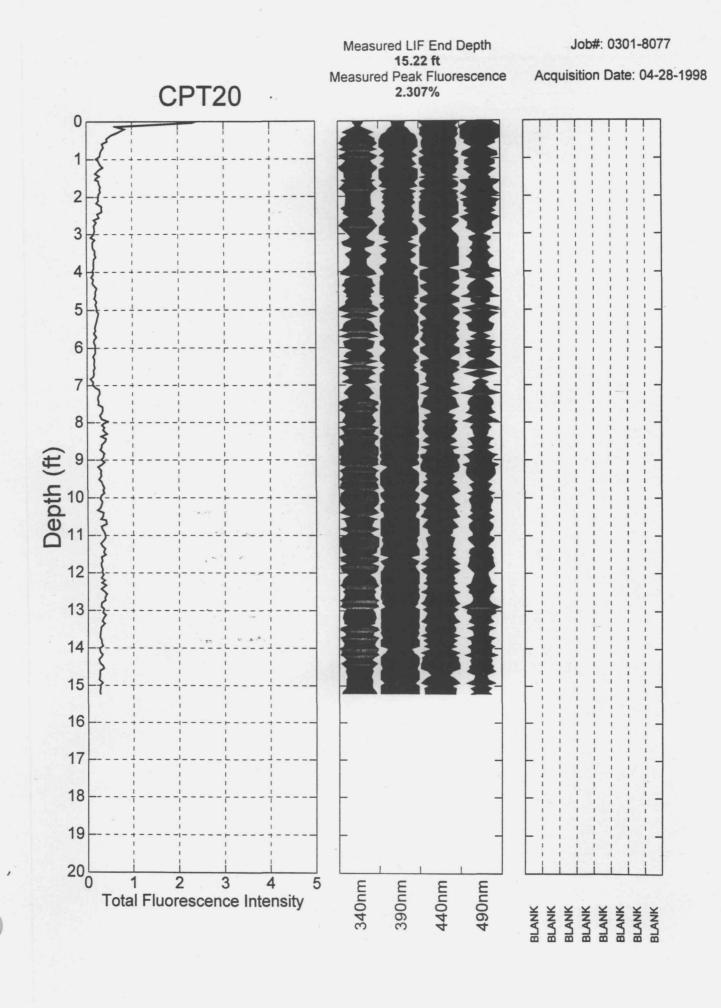


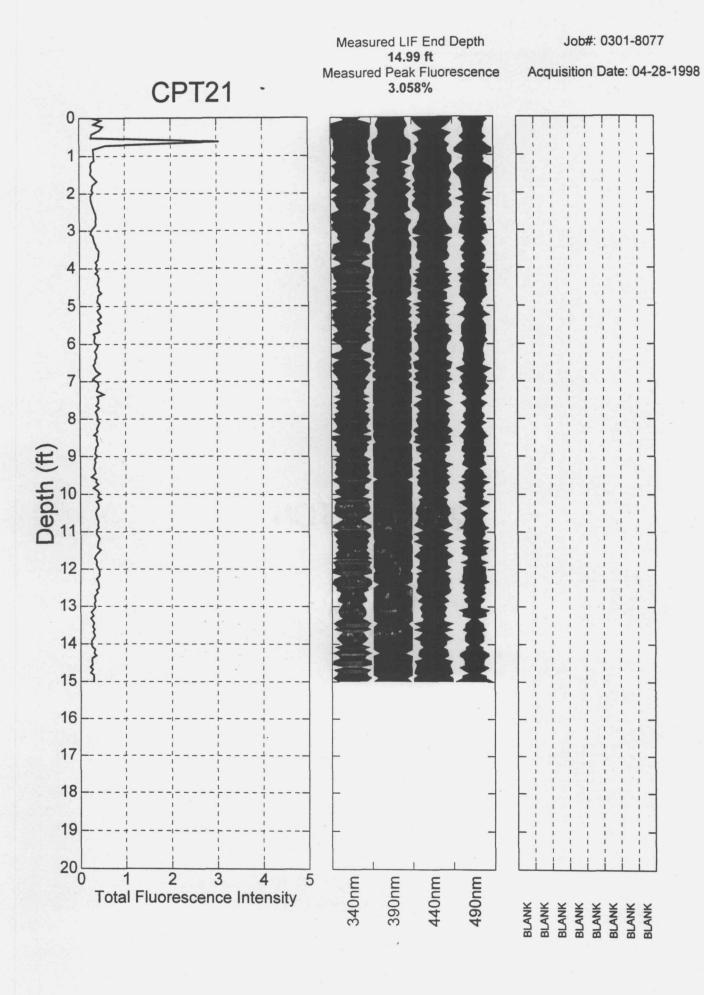


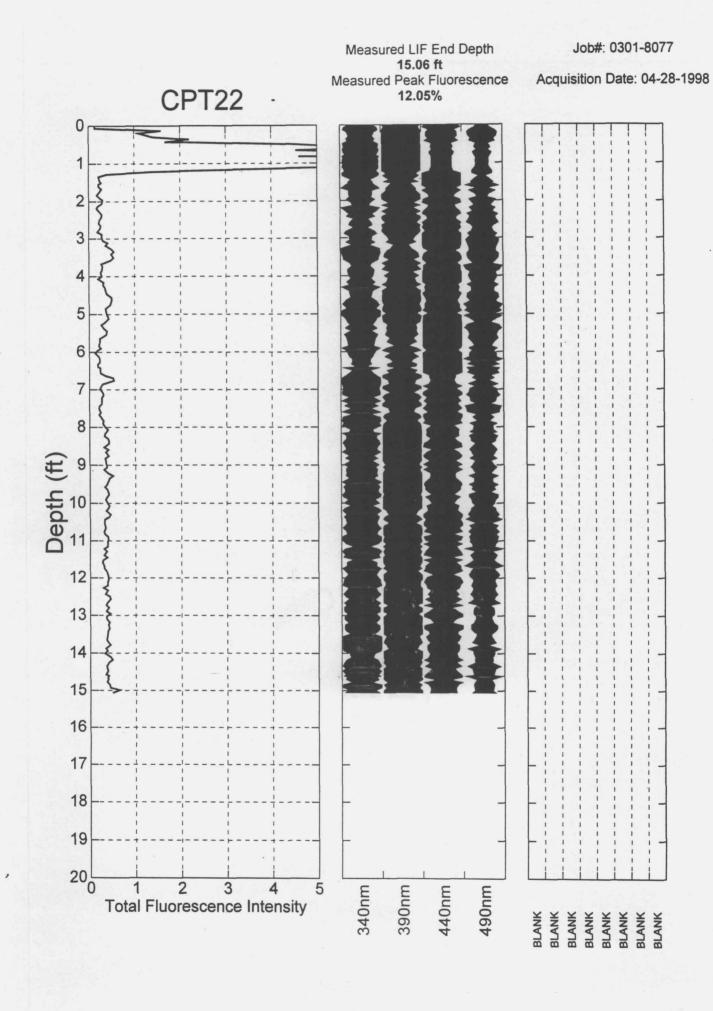


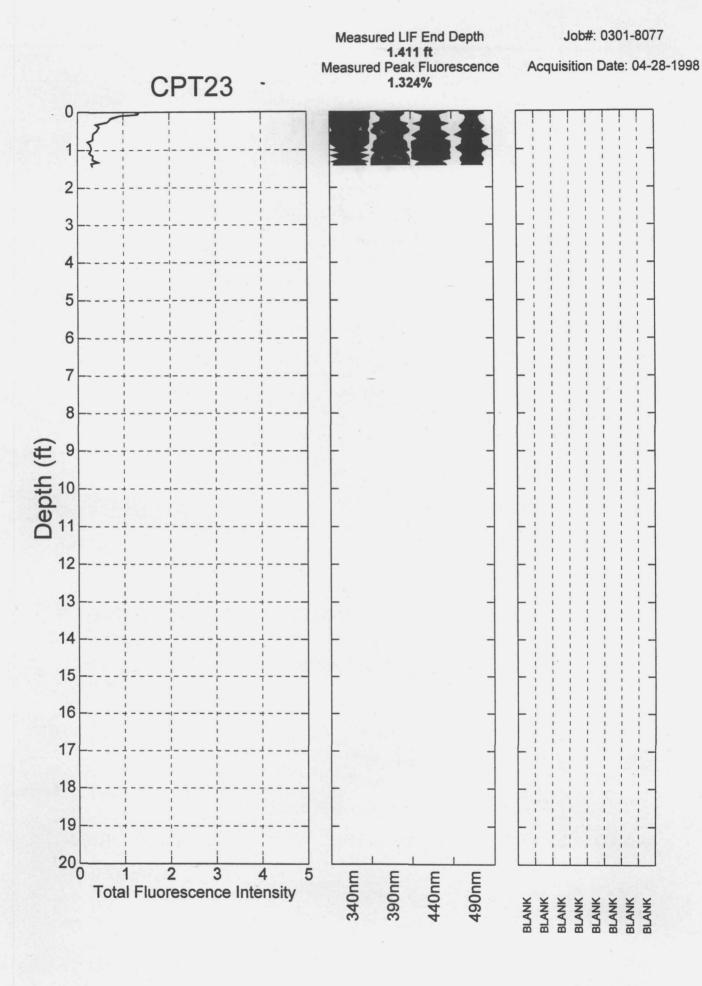


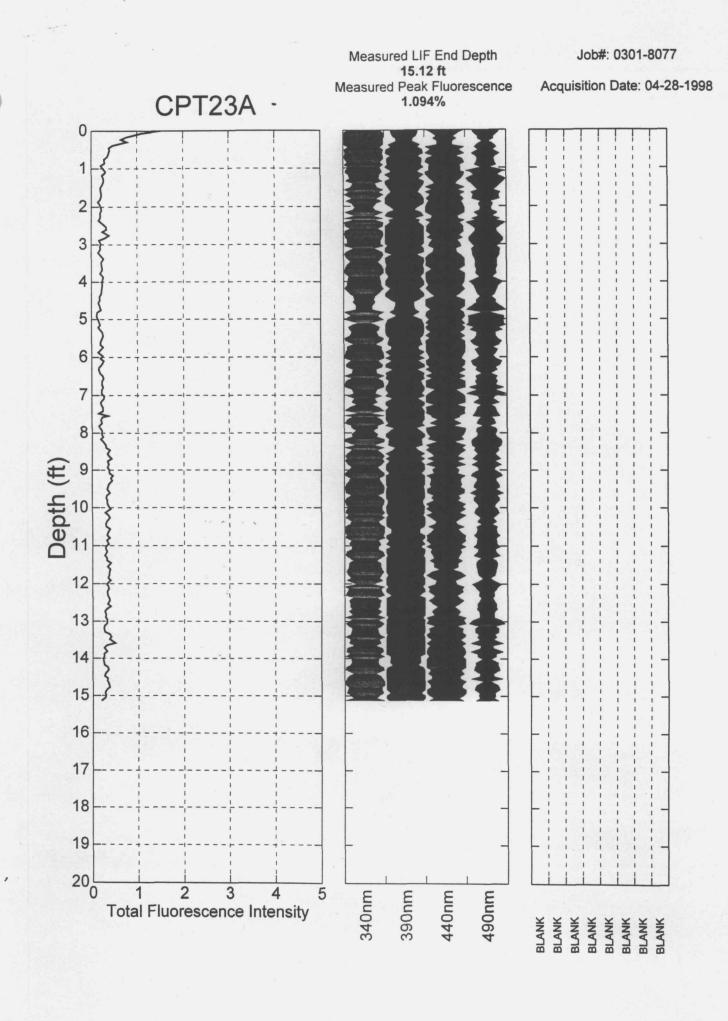


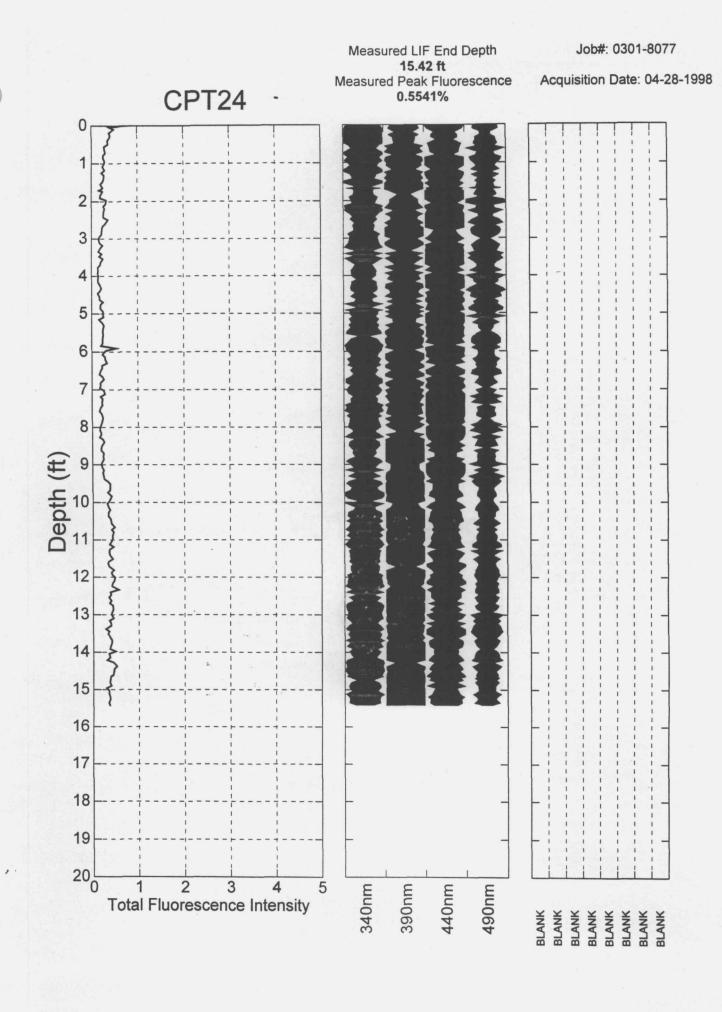


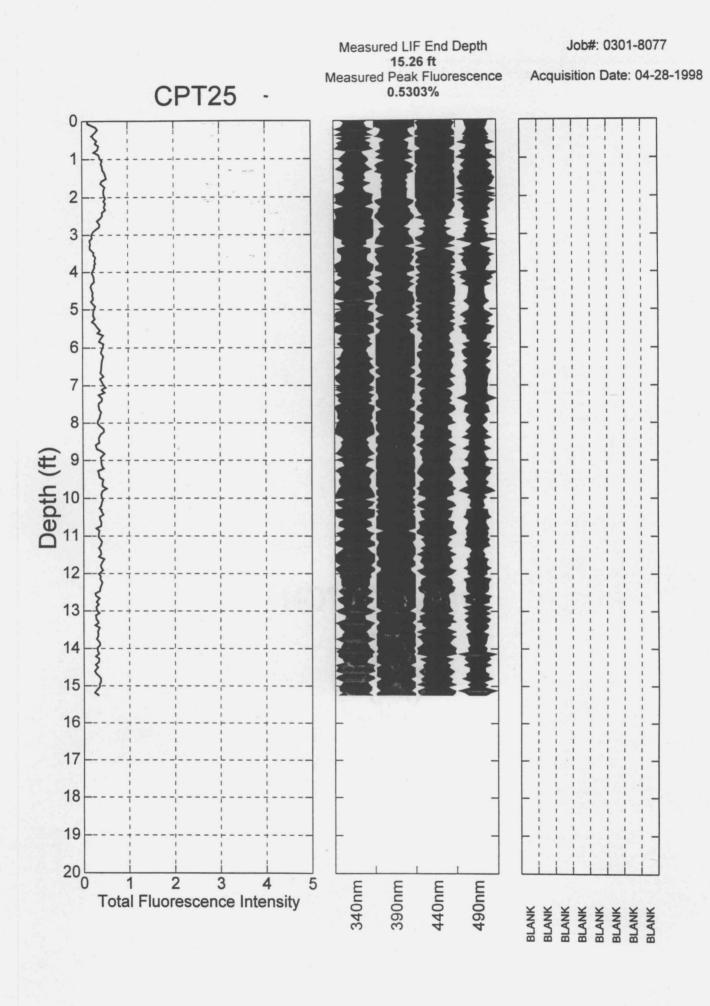


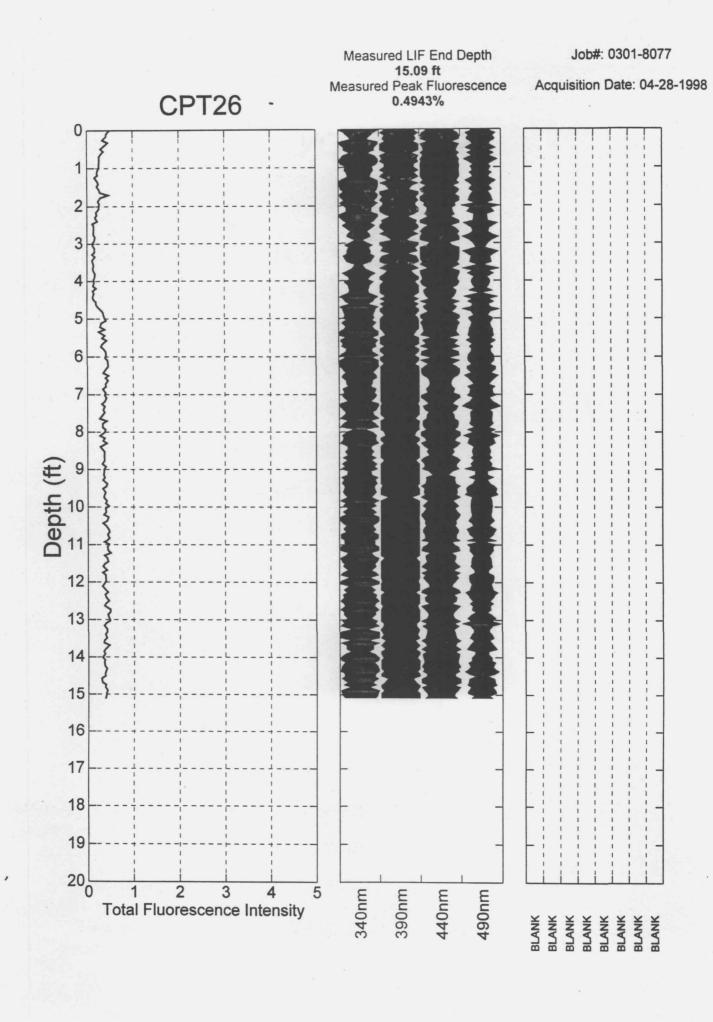


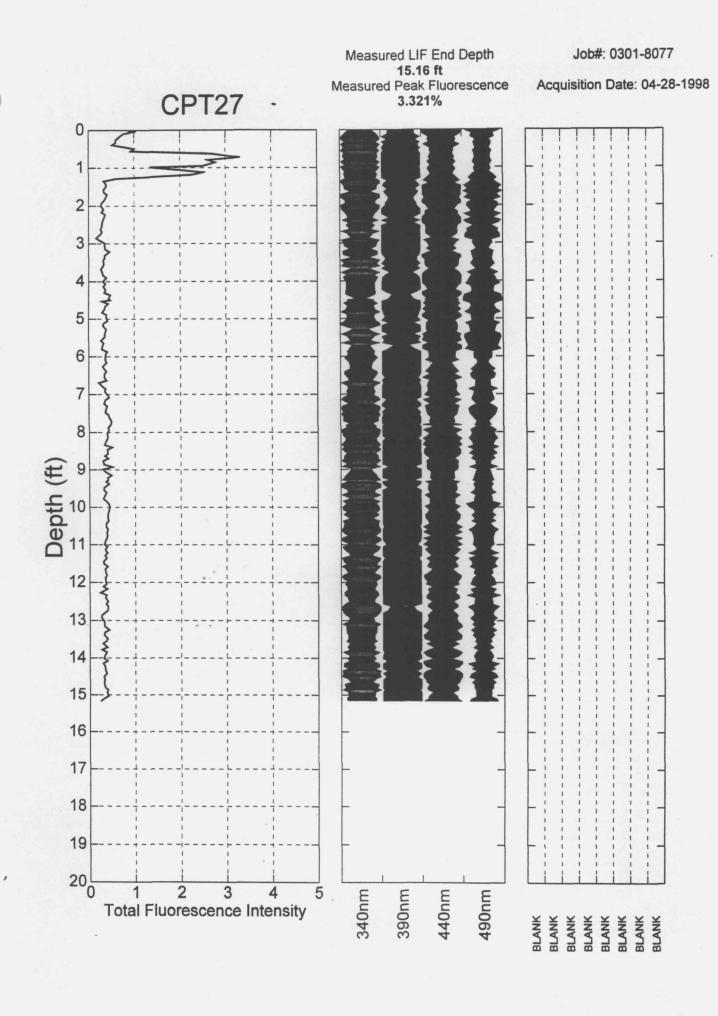


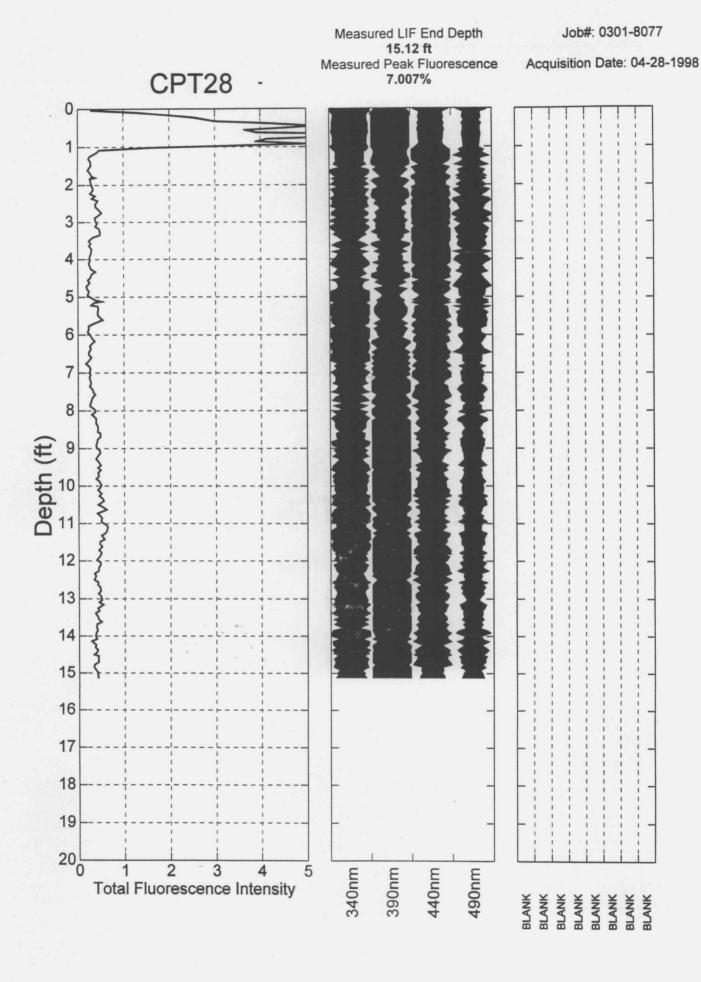


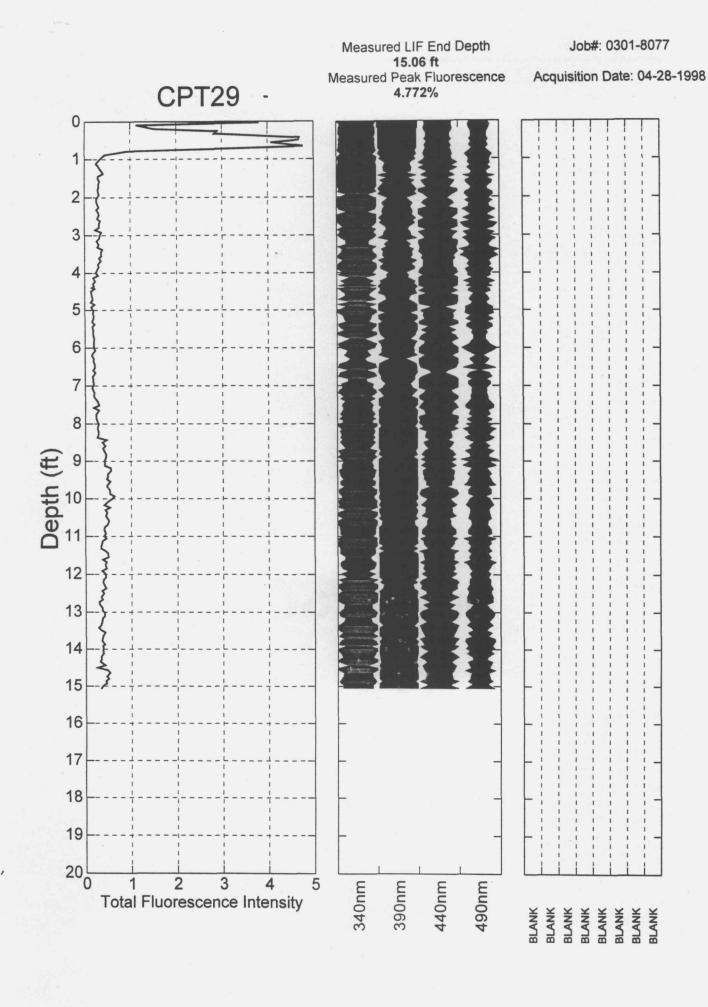


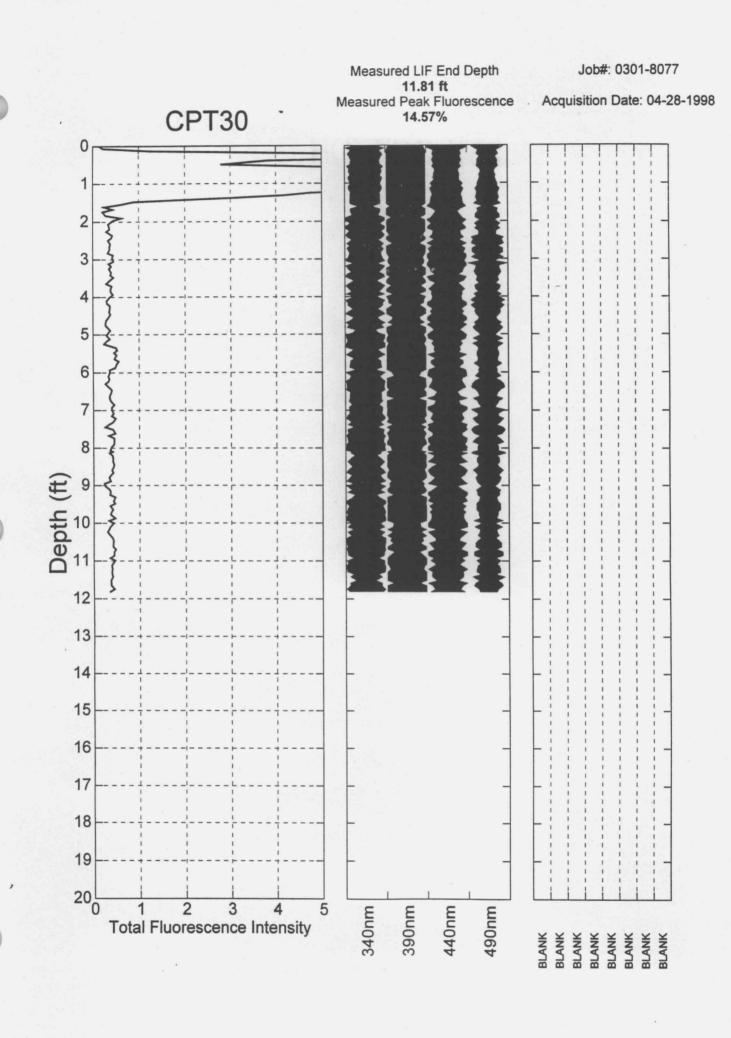


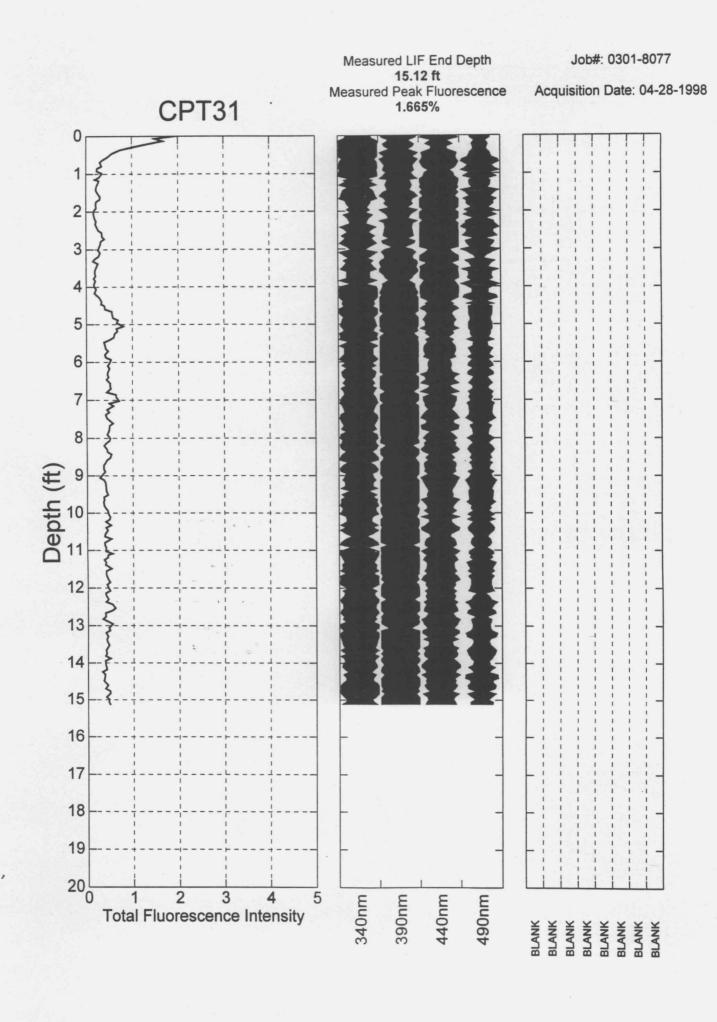


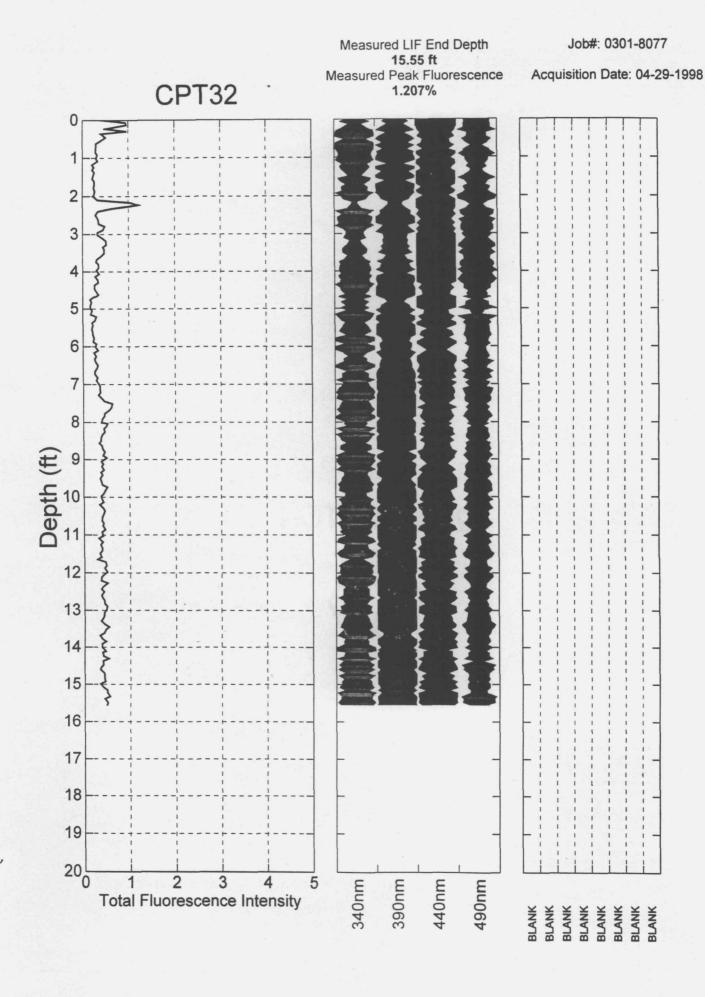


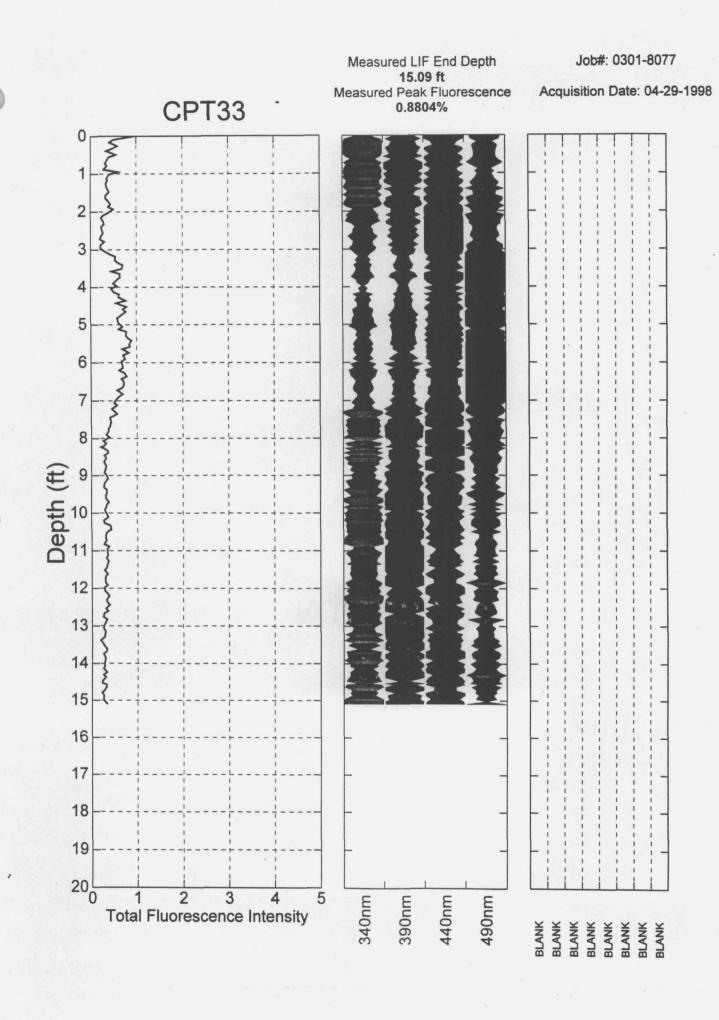


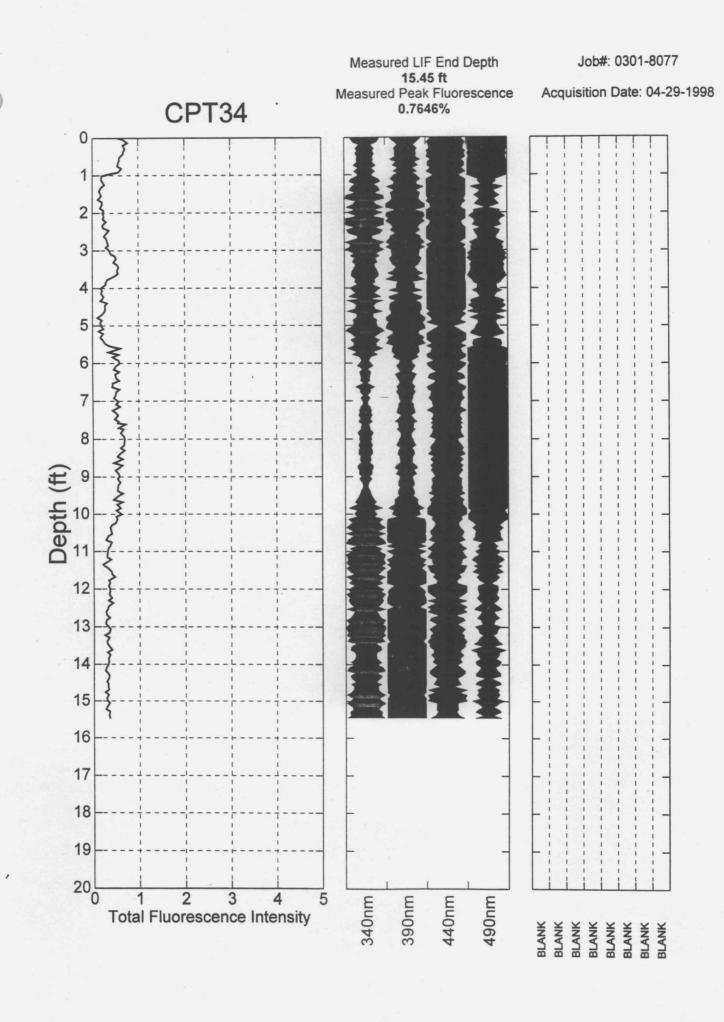


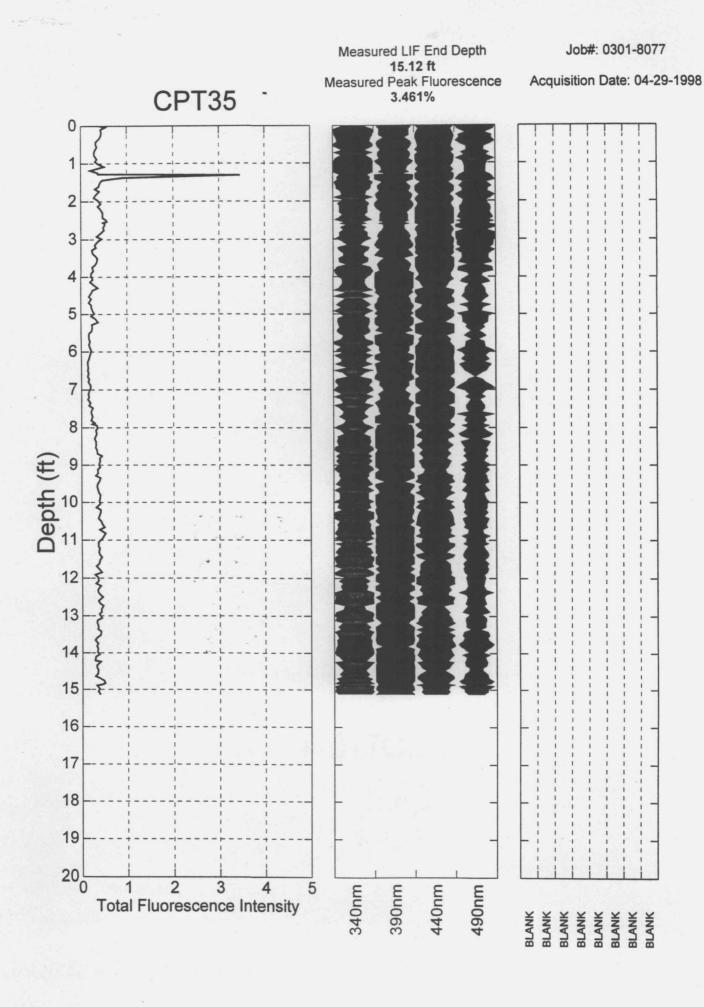


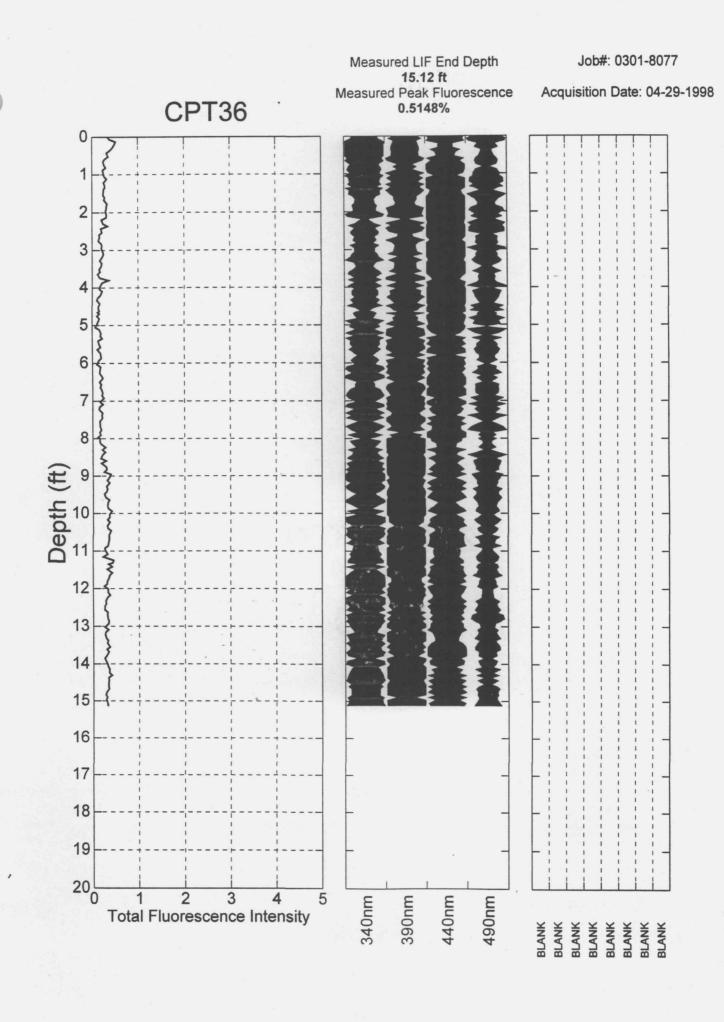


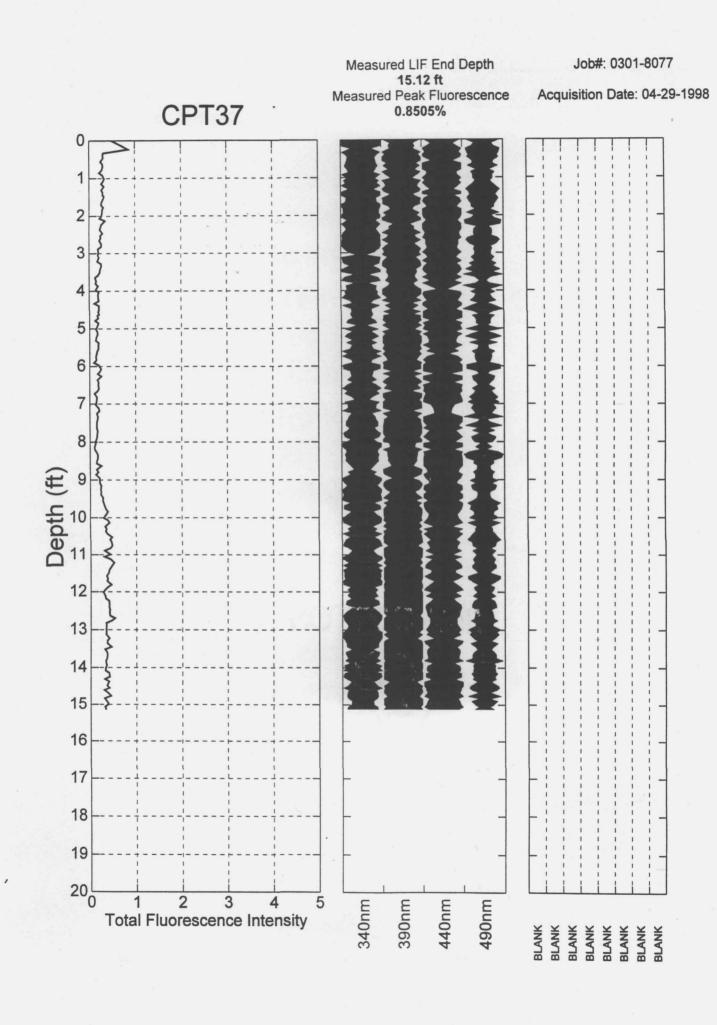


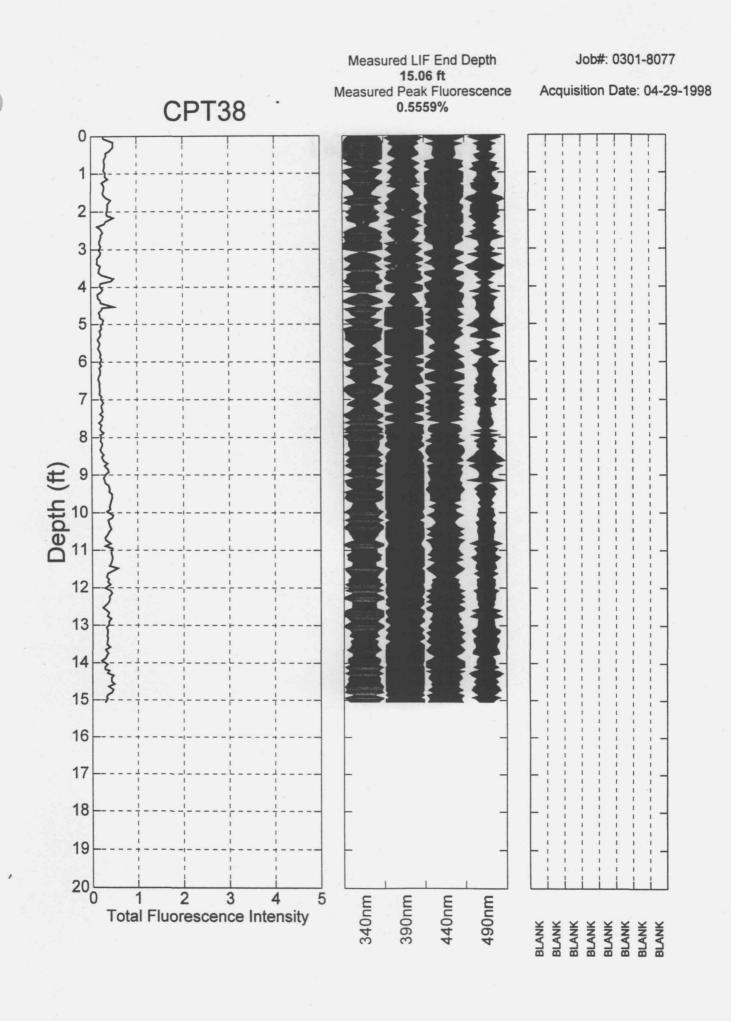


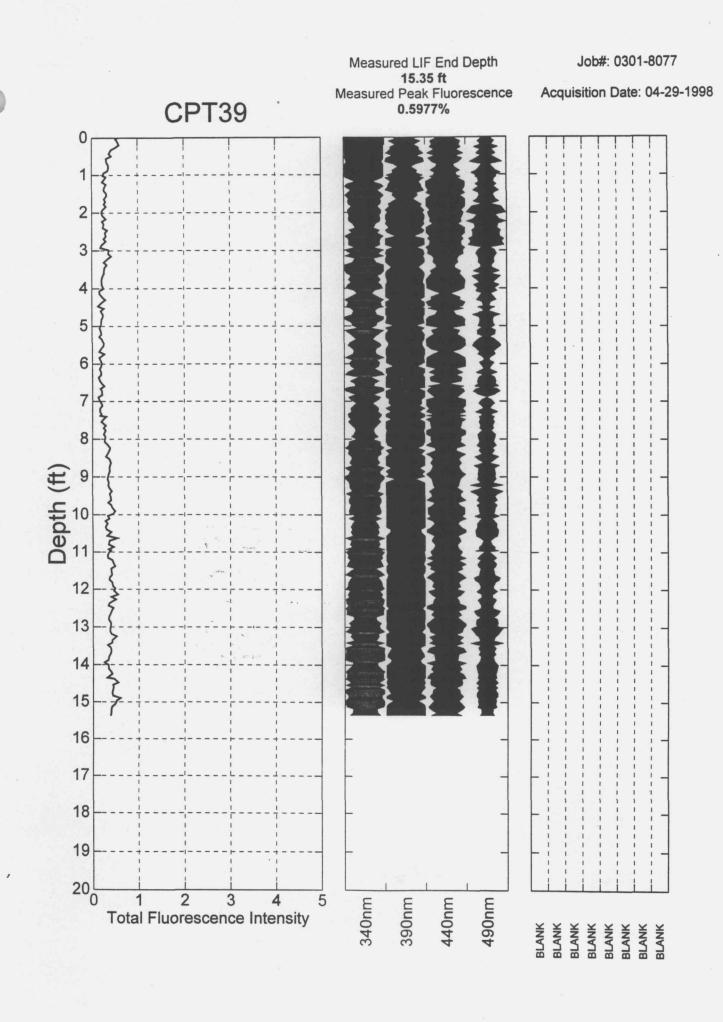


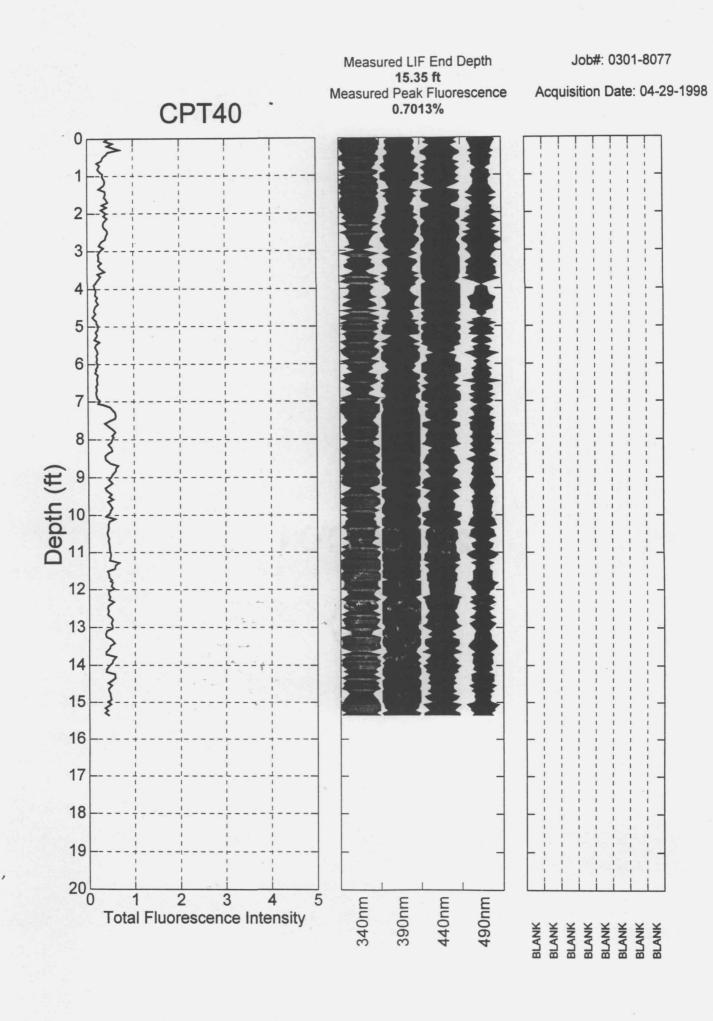


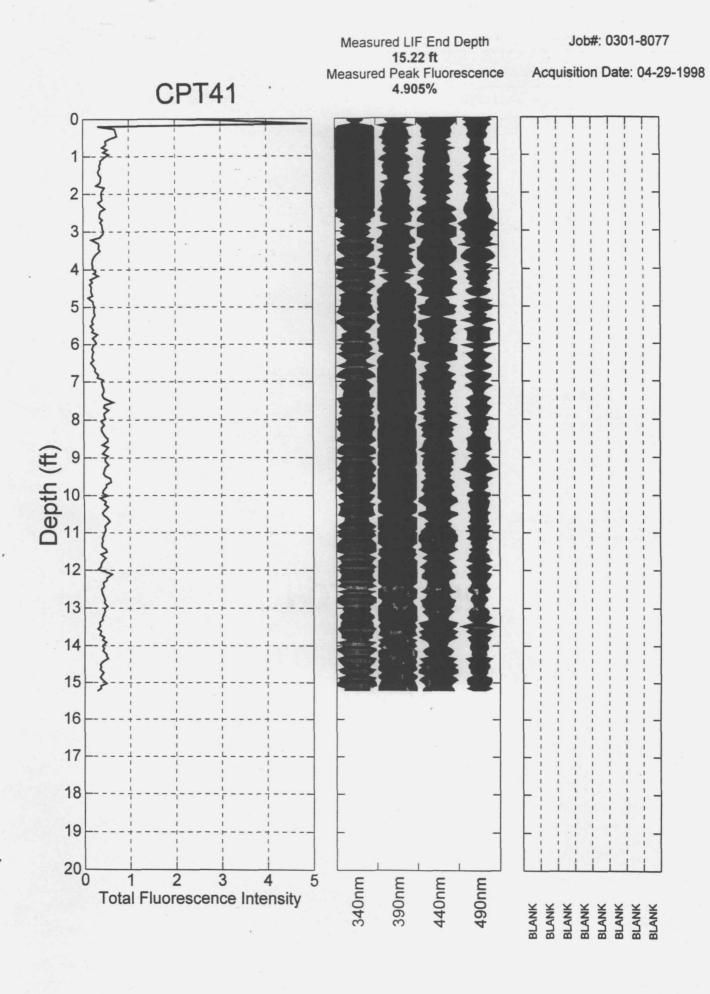


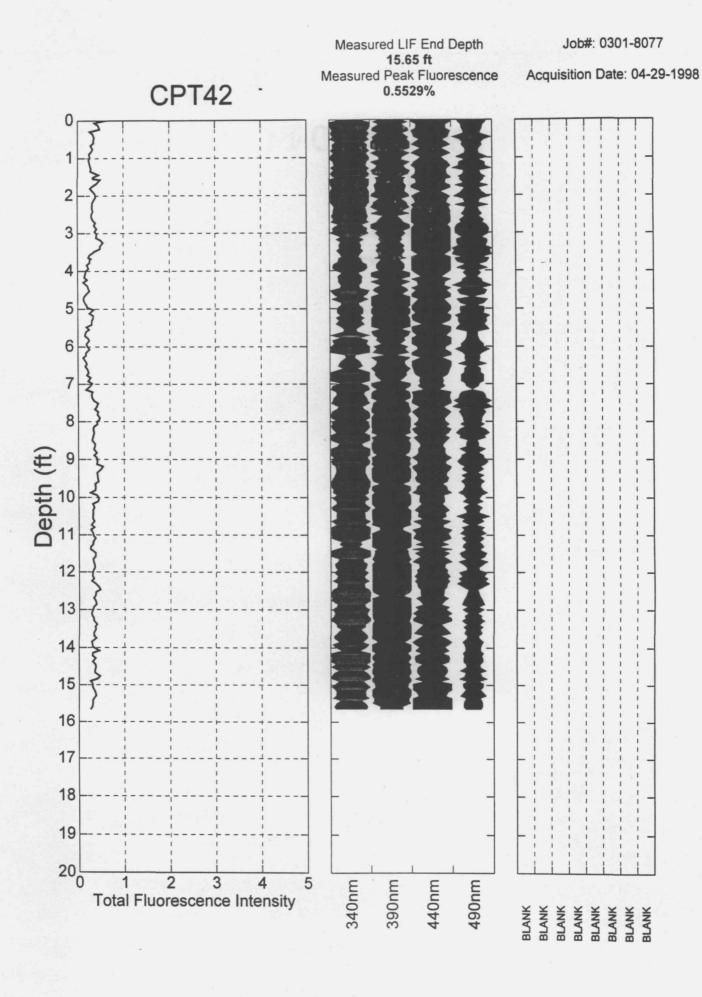


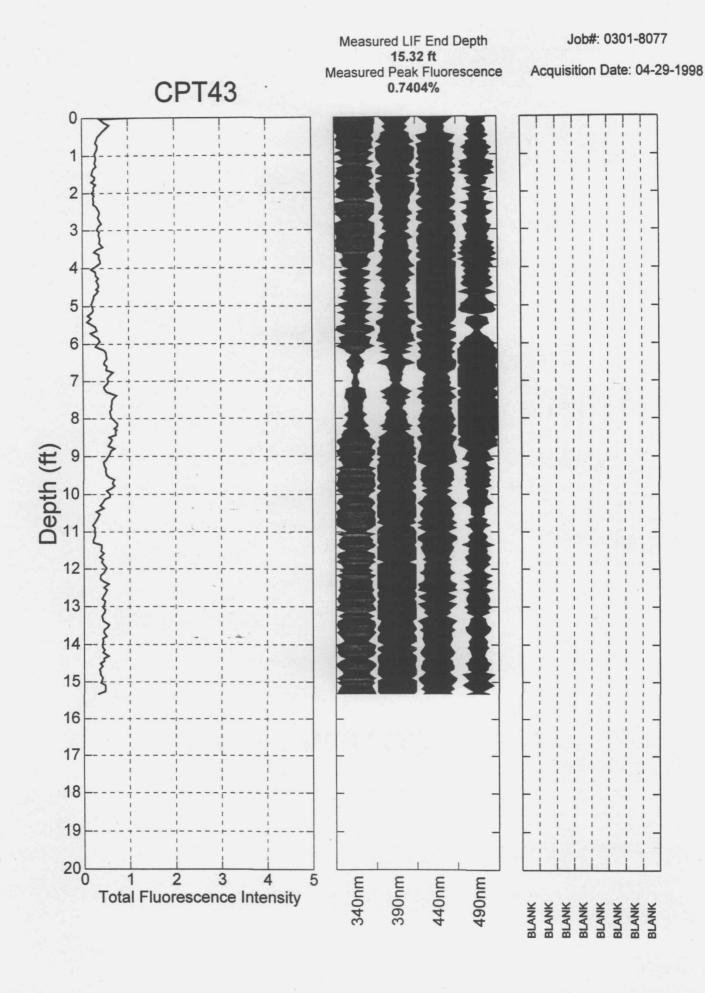


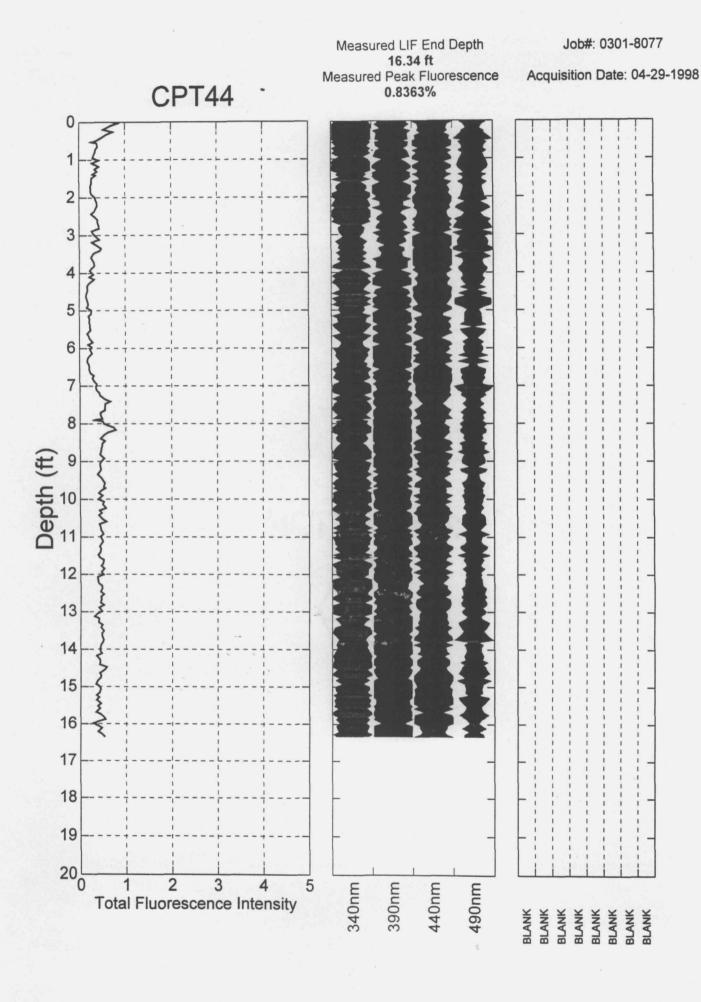


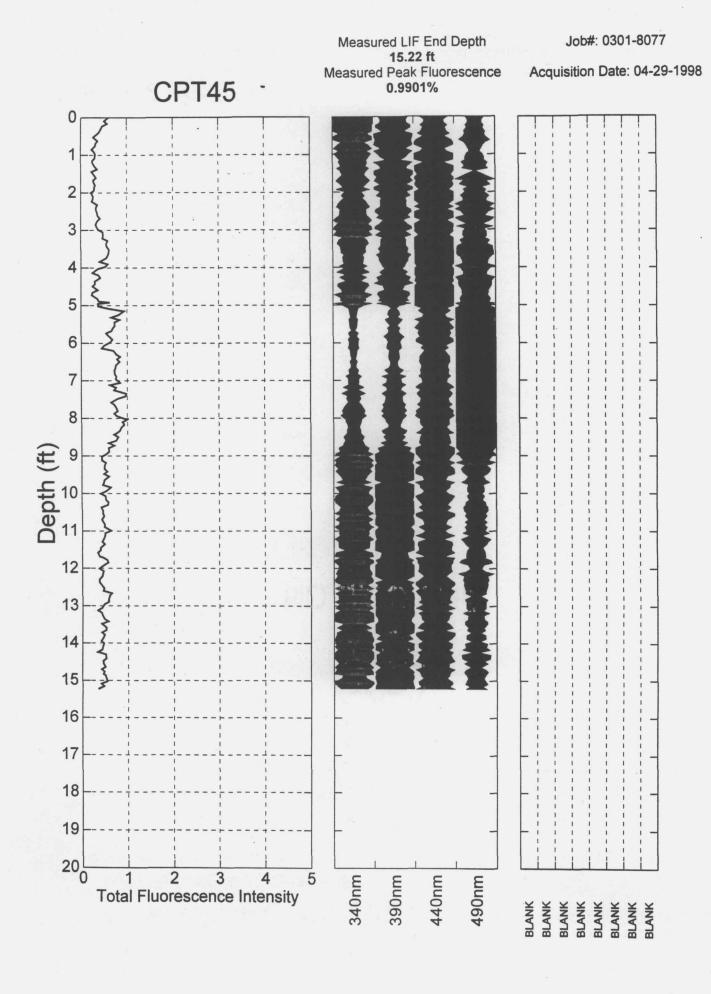


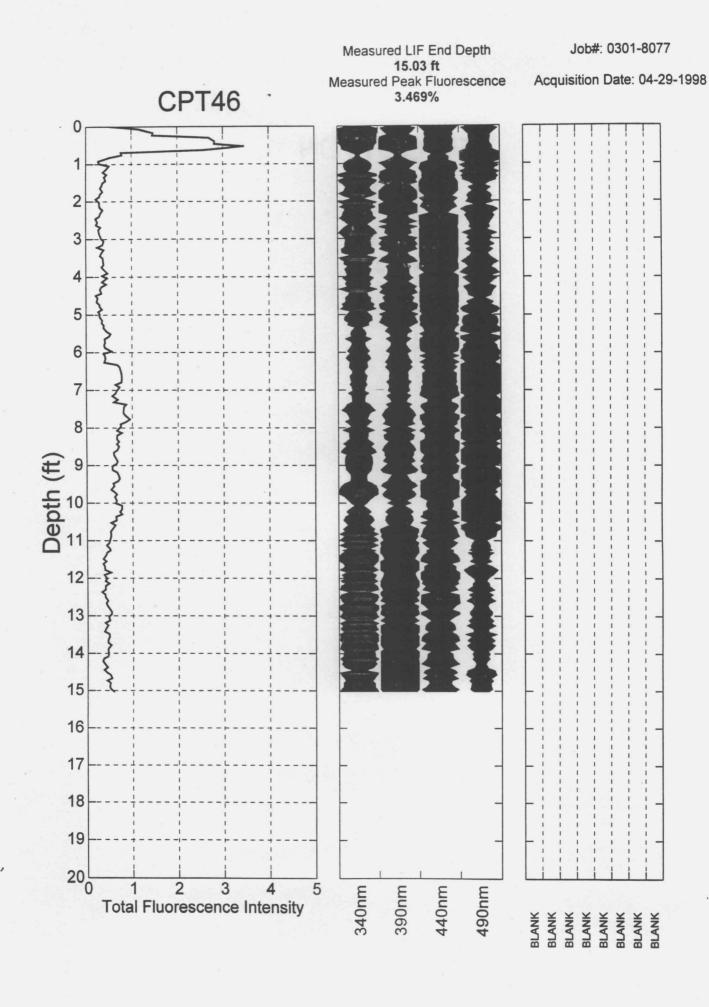


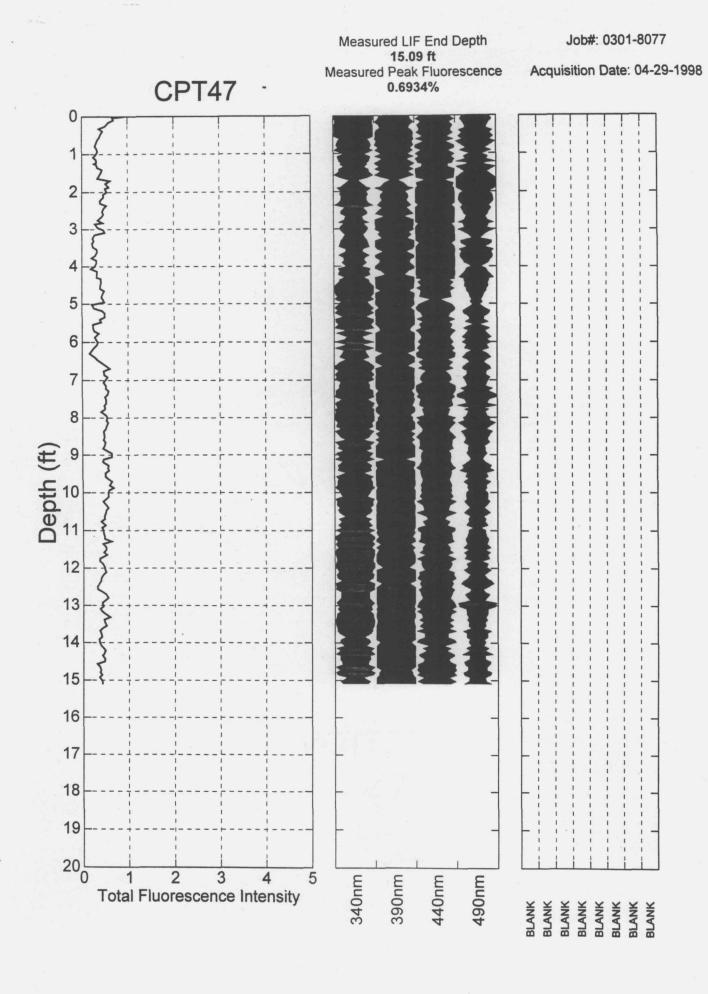


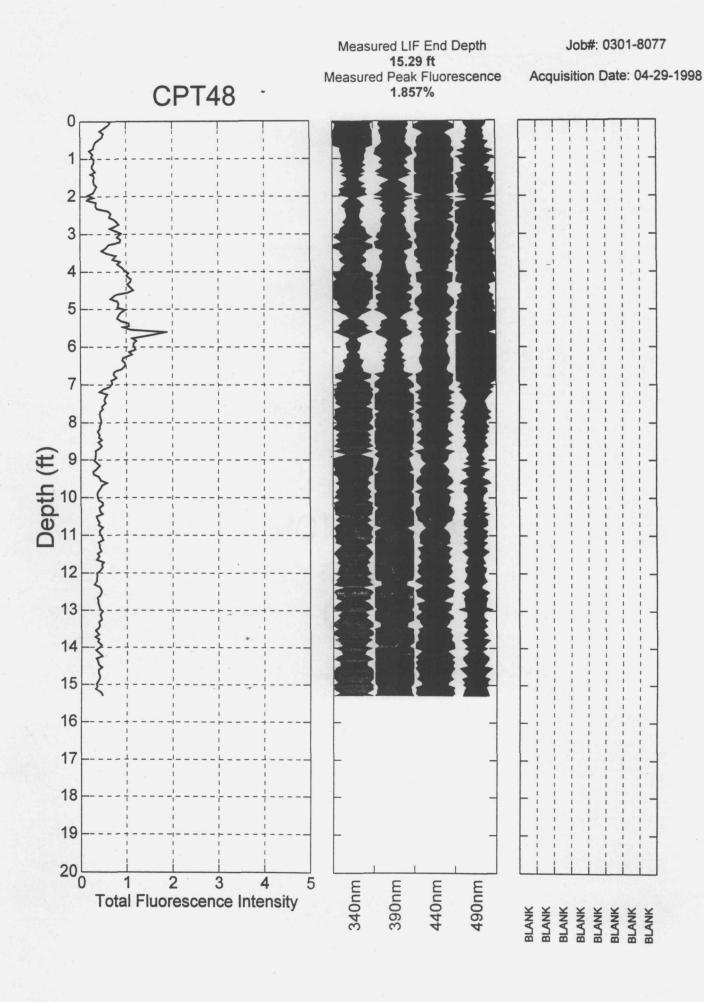


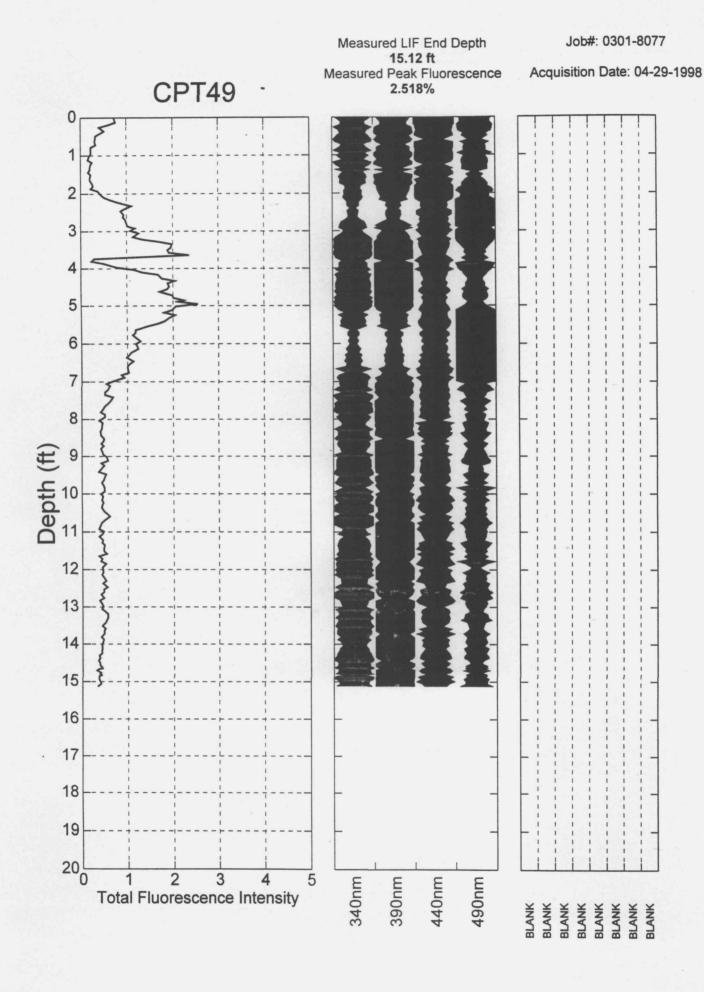


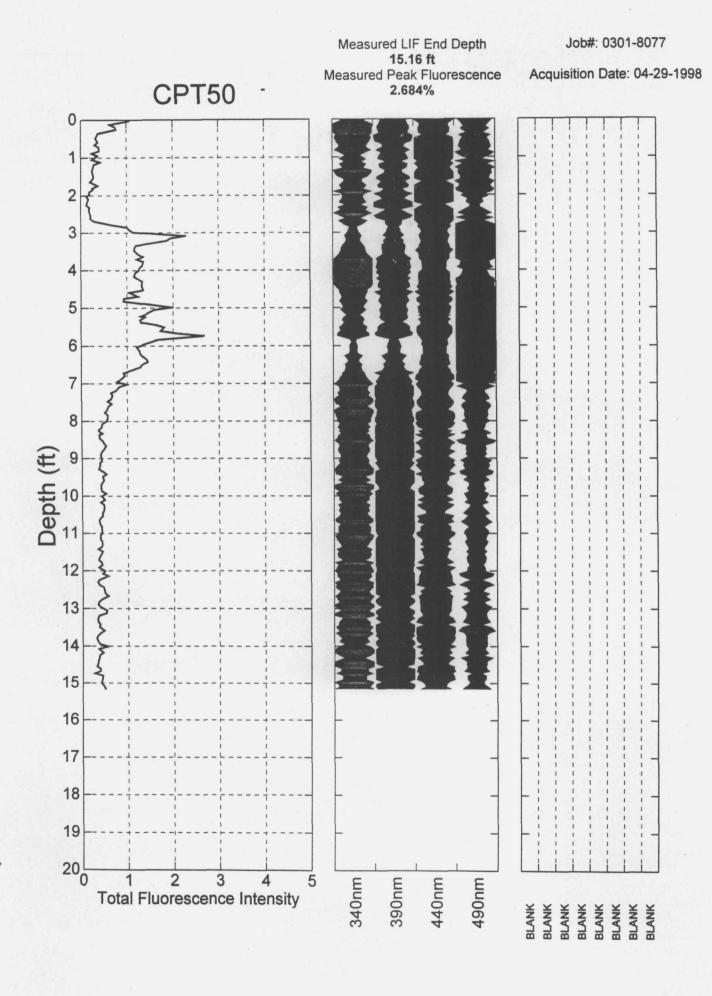


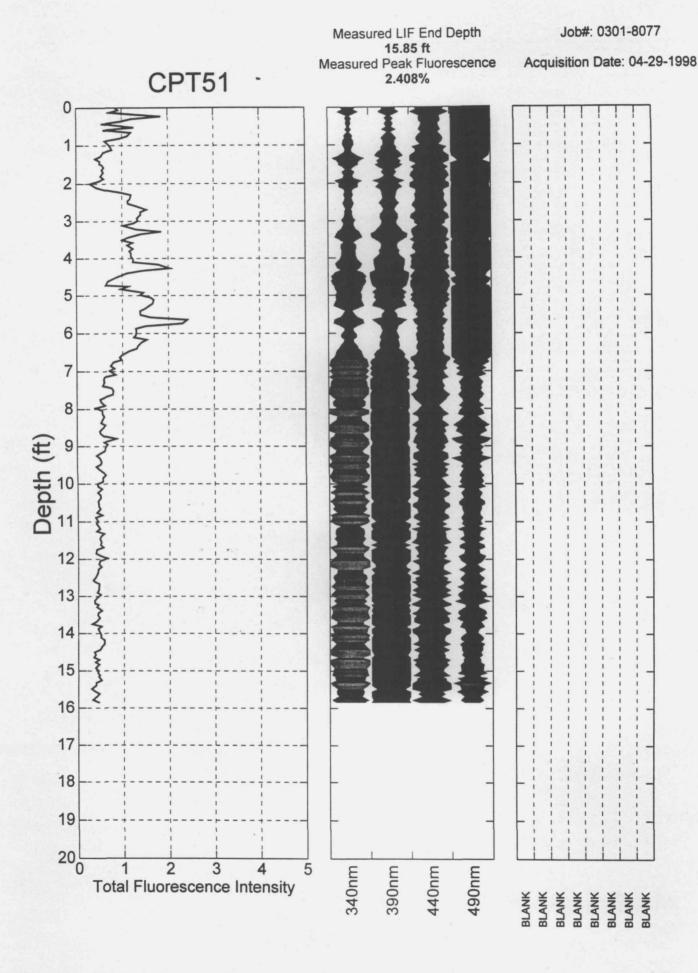


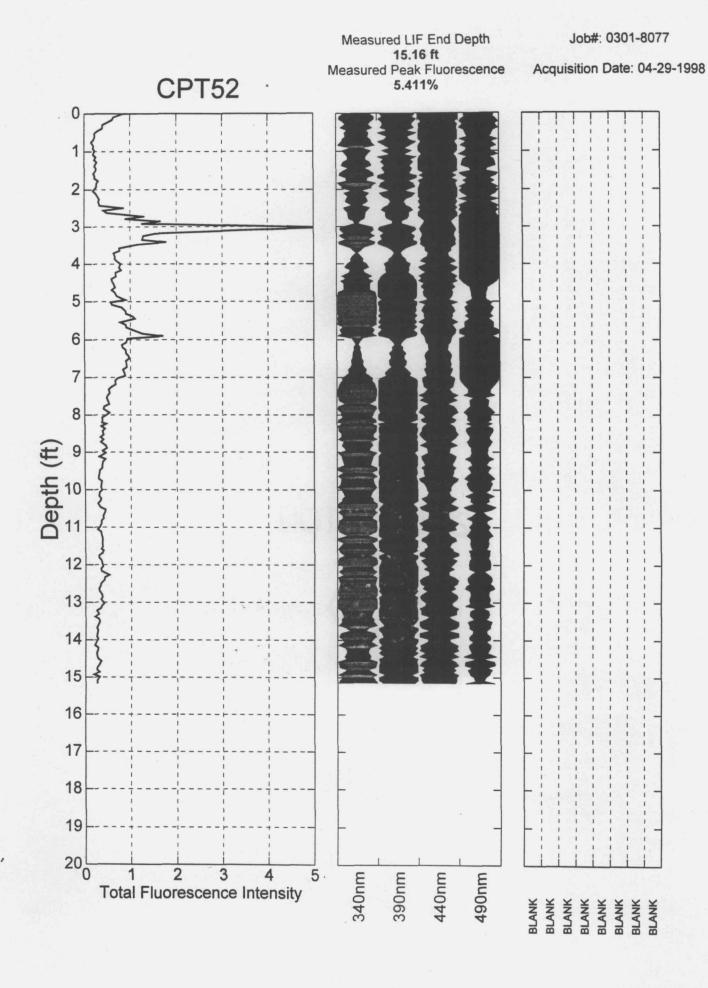


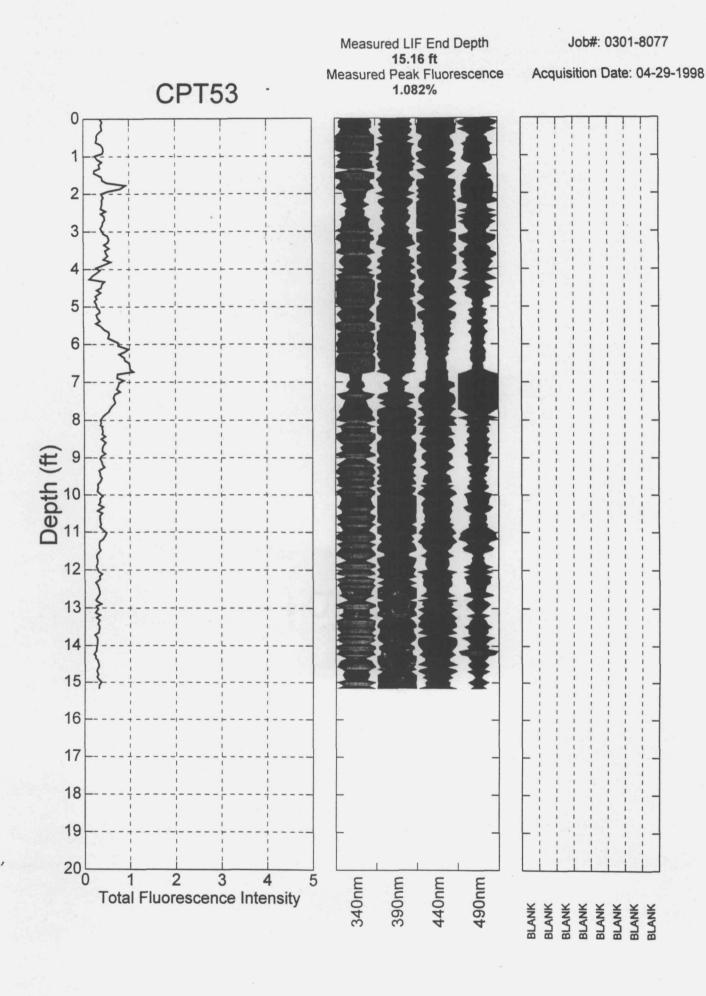


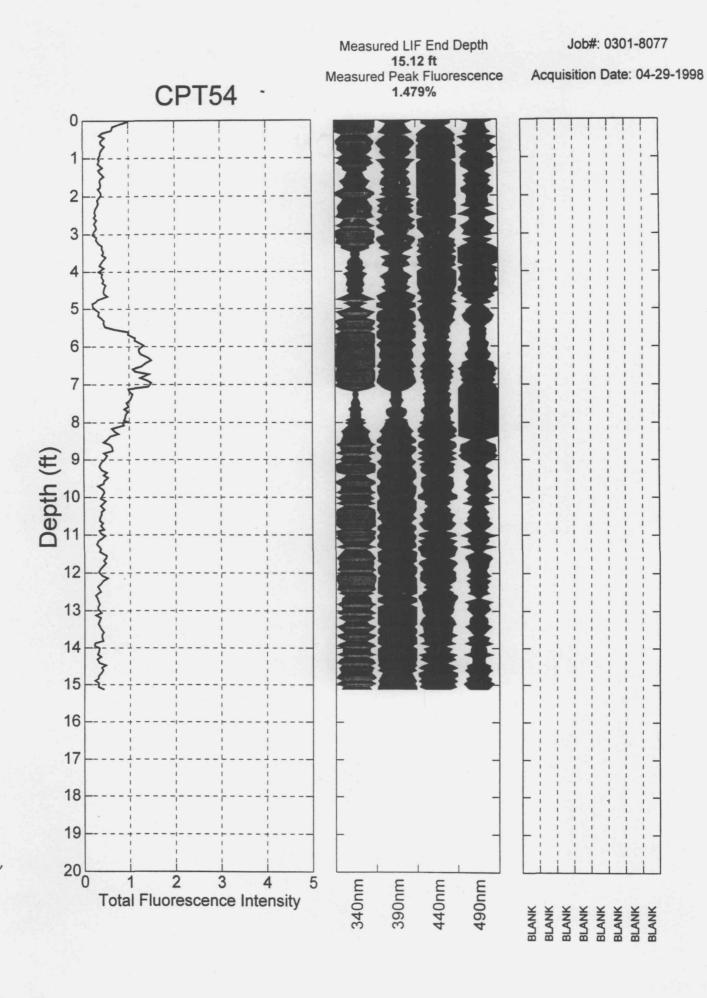


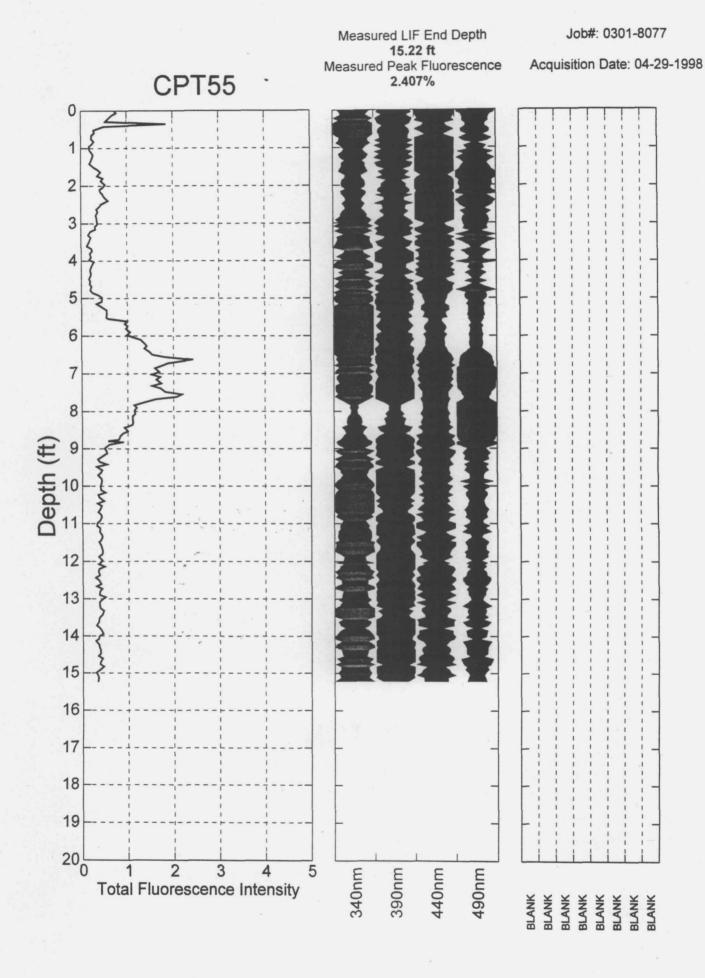


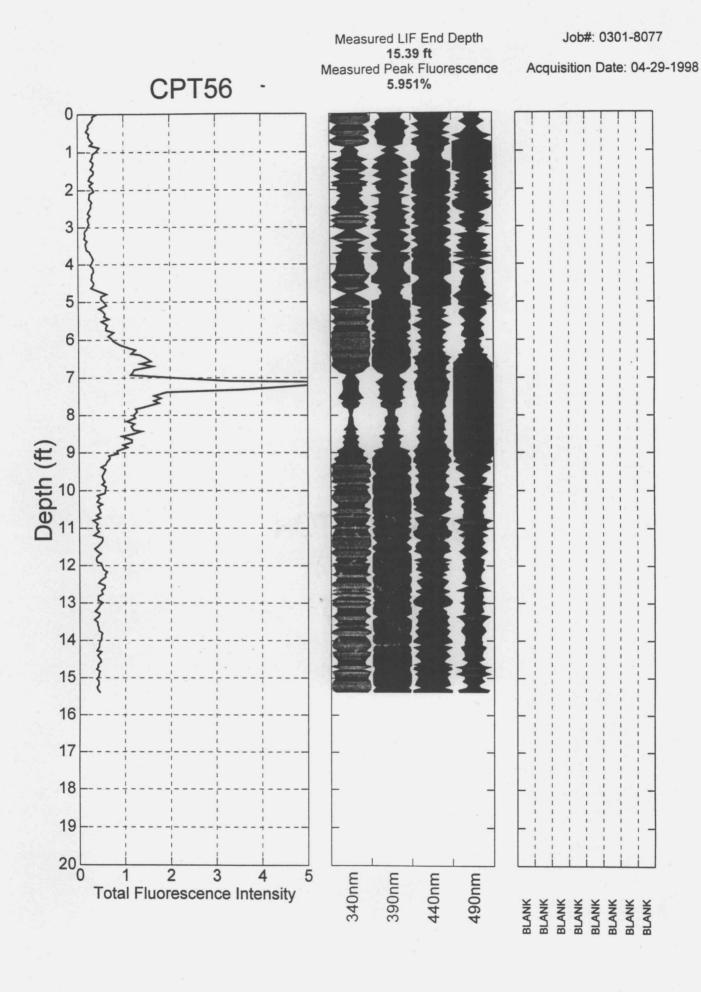


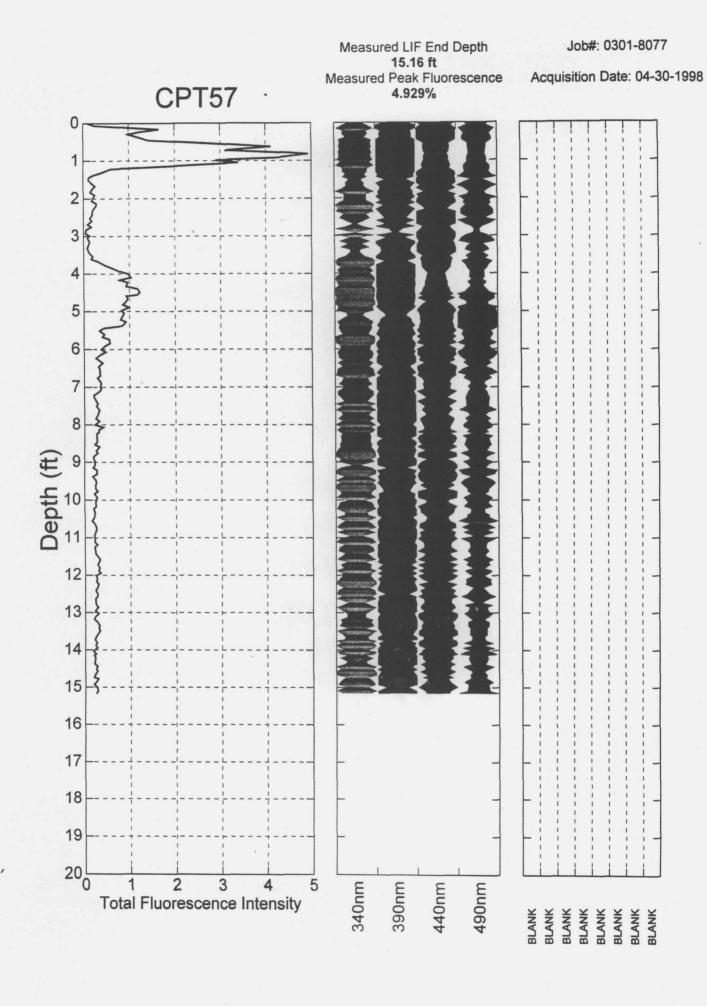


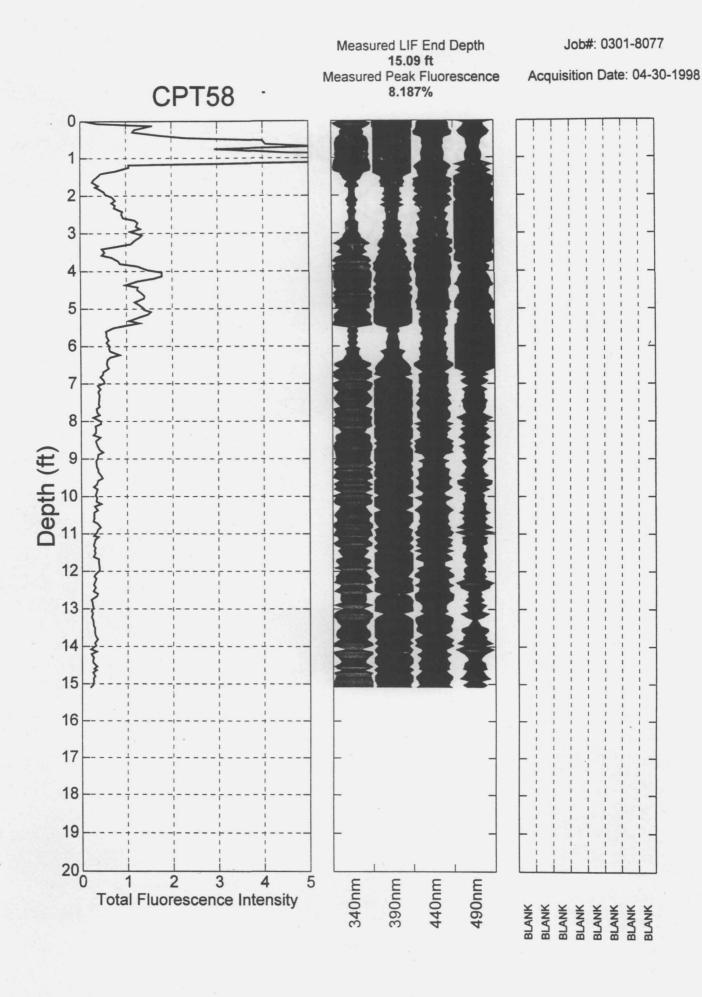


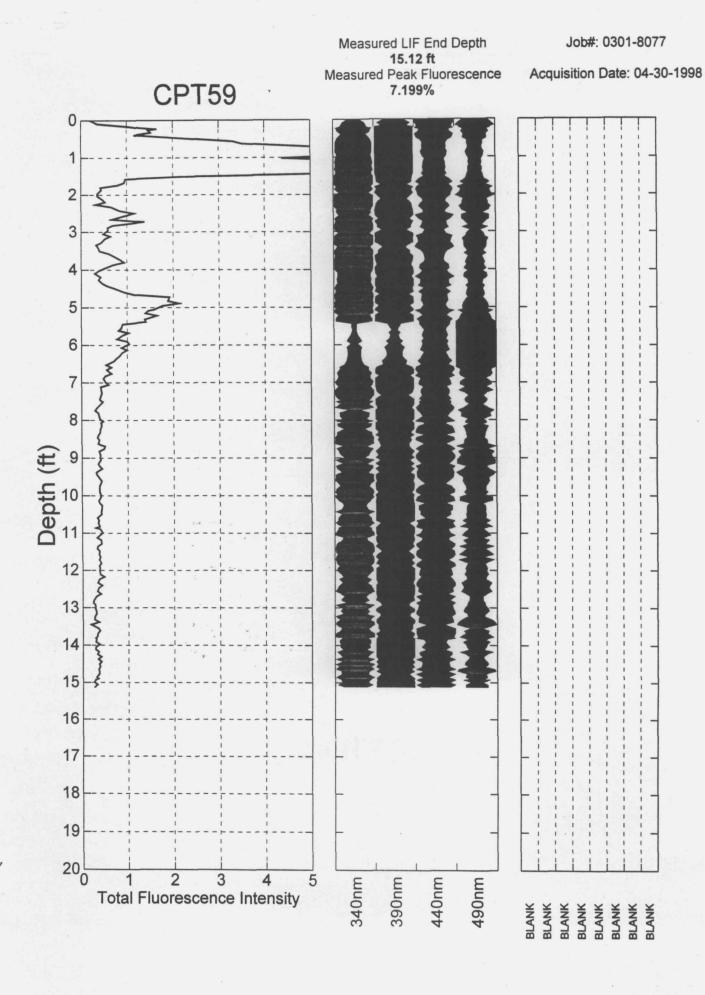


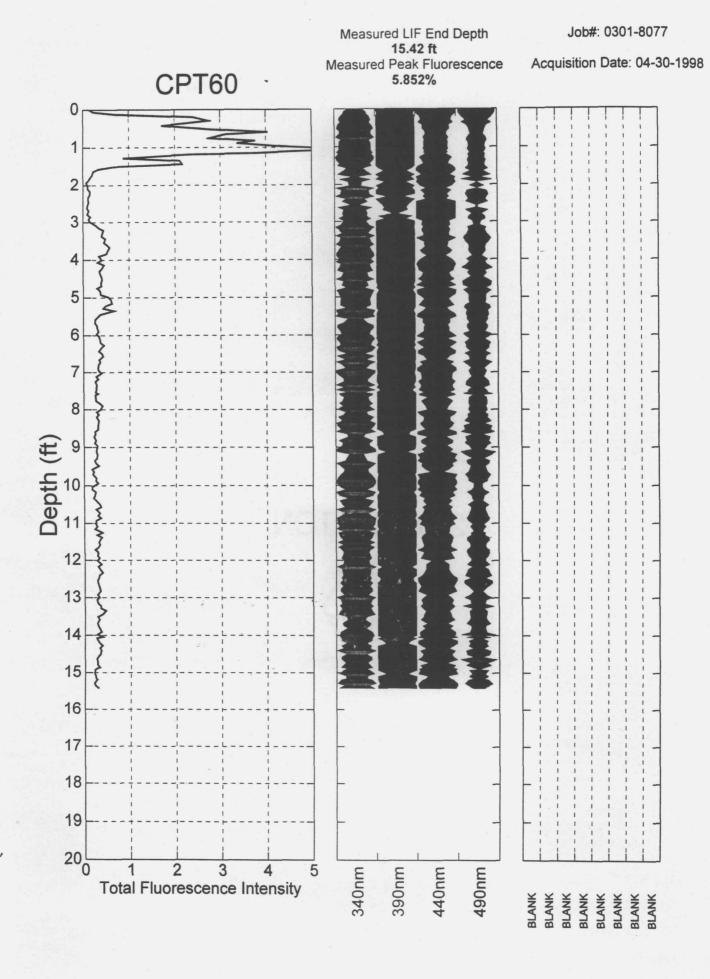


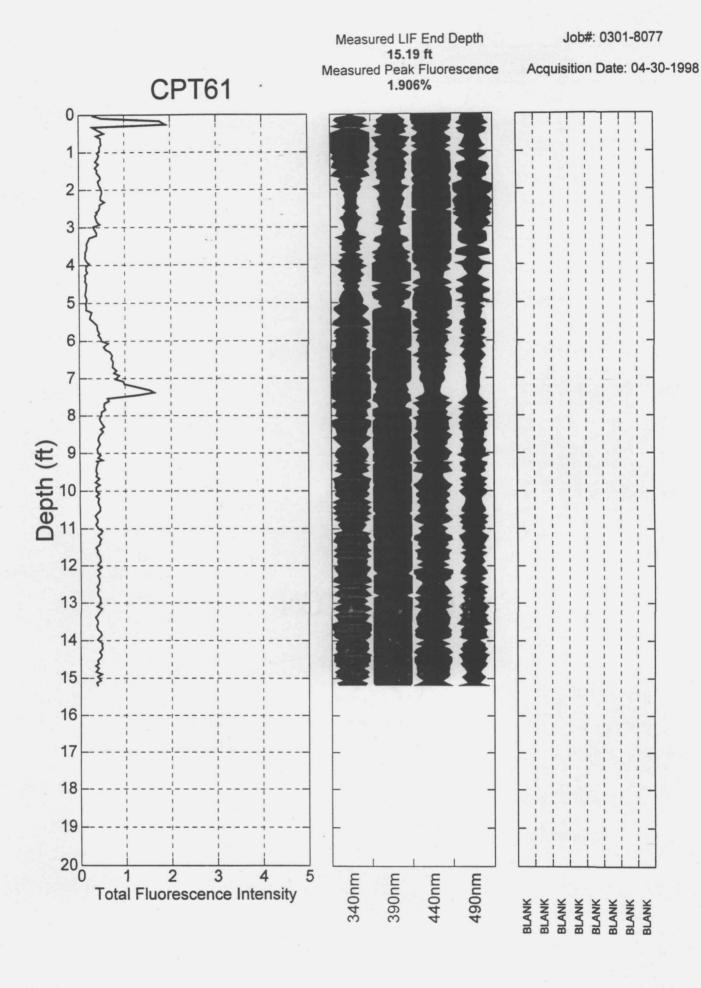


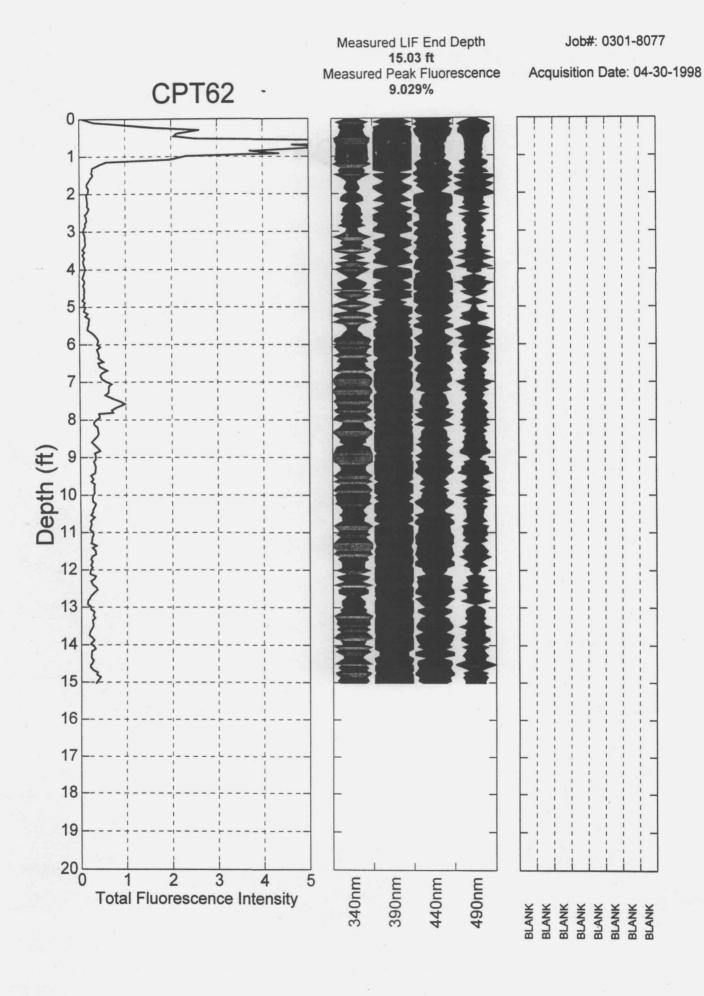


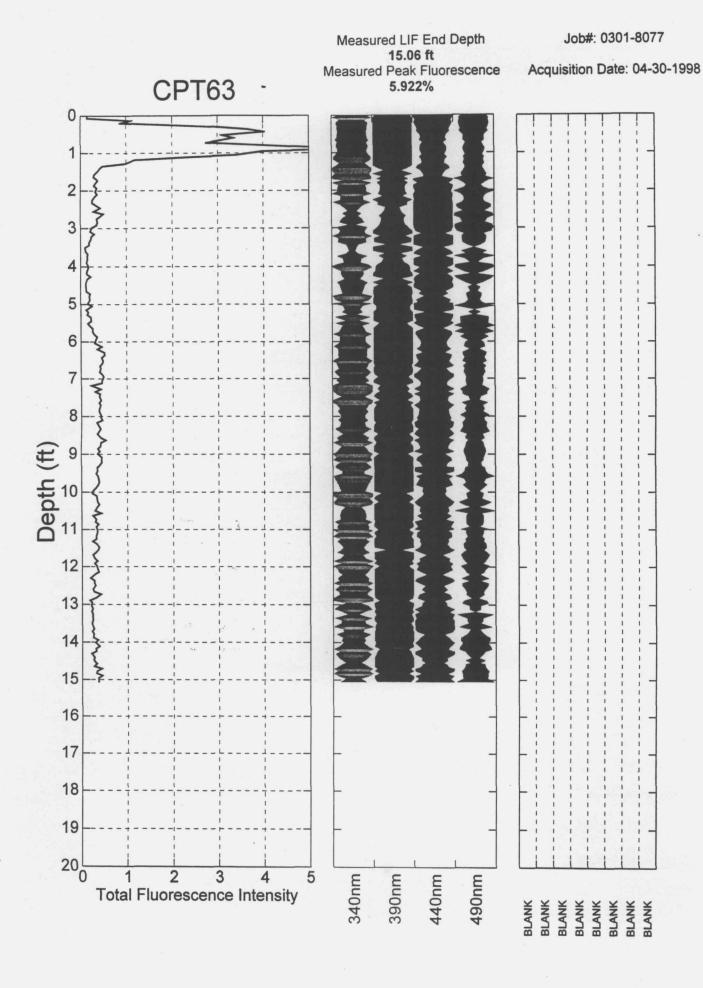


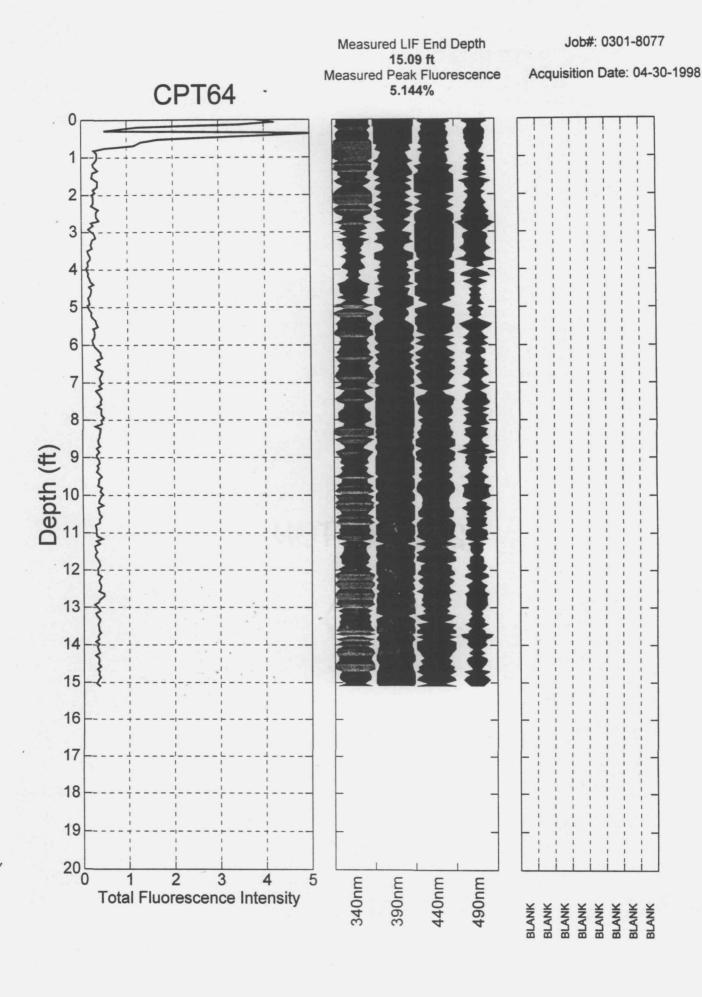


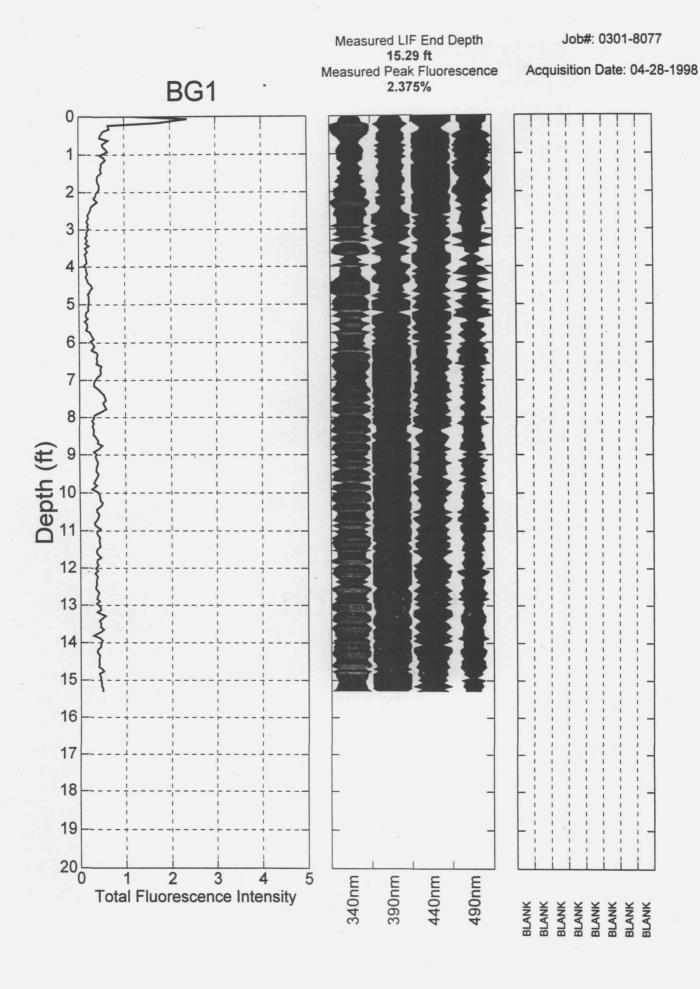












CPT LOGS

Key To Soil Classification and Symbols

SOIL TYPE SAMPLE TYPE (Shown in Symbol Column) (Shown in Samples Column) Silt Sand Clay **Rock Core** Undisturbed Split Spoon Predominant Type Shown Heavy

TERMS DESCRIBING CONSISTENCY OR CONDITION

COARSE GRAINED SOILS (Major portion Retained on No. 200 Sieve)

includes (1) clean gravels and sand described as fine, medium or course, depending on distribution of grain sizes (2) silty or dayey gravels and sands and (3) fine grained low plasticity soils (PI < 10) such as sandy sits. Condition is rated according to relative density, as determined by lab tests or estimated from resistance to sampler penetration.

Descriptive Term	Penetration Resistance*	Relative Density
Loose	0 - 10	0 to 40%
Medium Dense	10 - 3 0	40 to 70%
Dense	30 - 50	70 to 90%
Very Dense	. Over 50	90 to 100%

^{*} Blows/Foot, 140# Harnmer, 30" Drop

FINE GRAINED SOILS (Major Portion Passing No. 200 Sleve)

includes (1) inorganic and organic sits and clays, (2) sandy, gravelly or sity clays, and (3) clayey sits. Consistency is rated according to shearing strength, as indicated by penetrometer readings or by unconfined compression tests for soils with PI > 10.

Descriptive	Cohesive Shear Strength	
Term	Tons/Square Foot	
Very Soft	Less Than 0.125	
Soft	0.125 to 0.25	
Firm	0.25 to 0.50	
Stiff	0.50 to 1.00	
Very Stiff	1.00 to 2.00	
Hard	2.00 and Higher	

Note: Slickensided and fissured clay may have lower unconfined compressive strengths than shown above because of planes of weakness or shrinkage cracks; consistency ratings of such soils are based on hand penetrometer readings.

ing

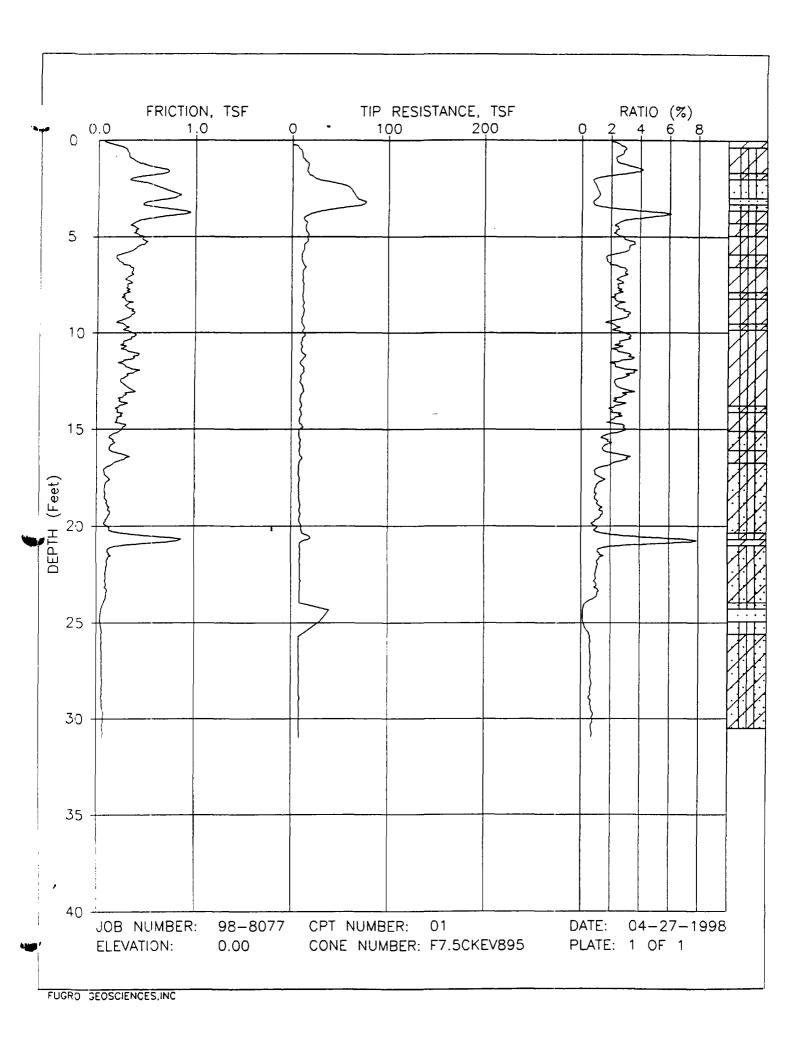
range of sizes with some intermediate size miss-

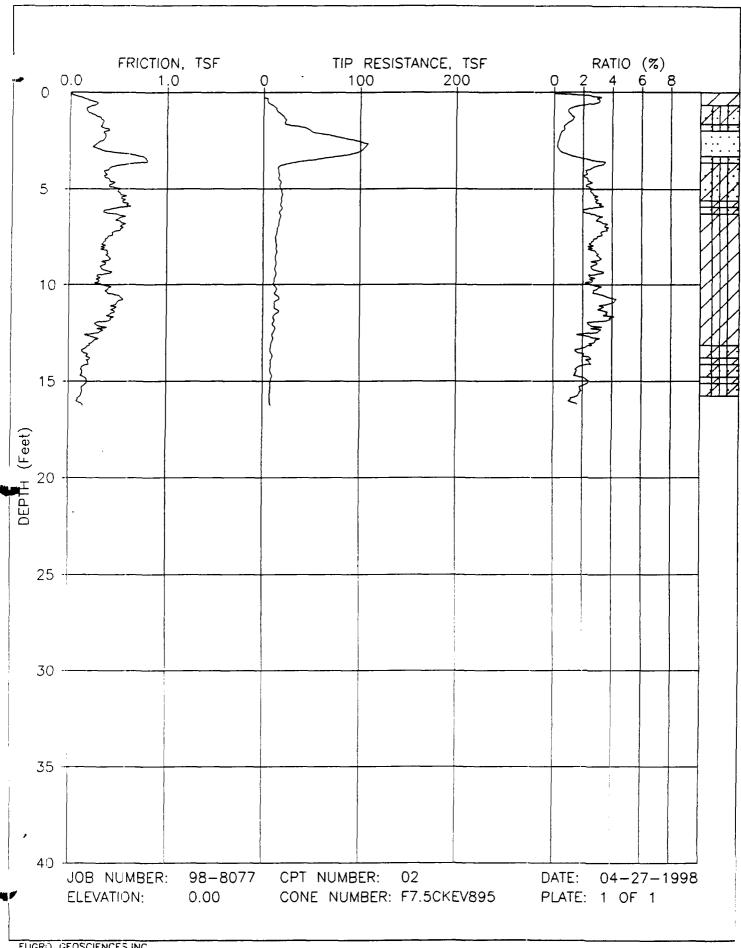
Parting:	paper thin in size		pertaining to cohesive soils that exhibit a loose
Seam: Layer: Fissured:	1/8° to 3° thick greater than 3° containing shrinkage cracks, frequently filled with	Slickensided:	knit or flakey structure having inclined planes of weakness that are slick and glossy in appearance.
	fine sand or silt, usually more or less vertical	Degree of Slickensided Development	
Sensitive:	pertaining to cohesive soils that are subject to appreciable loss of strength when remoided	Slightly Slickensided:	slickensides present at intervals of 1' to
Interbedded:	composed of alternate layers of different soil types		2', soil does not easily break along these plates
Laminated:	composed of thin layers of varying color and texture	Moderately Slickensided	 d: slickensides spaced at intervals of 1' to 2', soil breaks easily along these planes
Calcareous:	containing appreciable quantities of calcium carbonate	Extremely Slickensided:	sides spaced at intervals of 4° to 12'
Well Graded:	having wide range in grain sizes and substantial amounts of all intermediate particle sizes		soil breaks along the slickensides into pieces 3° to 6° in size
Poorty Graded:	predominantly of one grain size, or having a range of sizes with some intermediate size miss-	Intensely Slickensided:	slickensides spaced at intervals of less than 4°, continuous in all directions; so

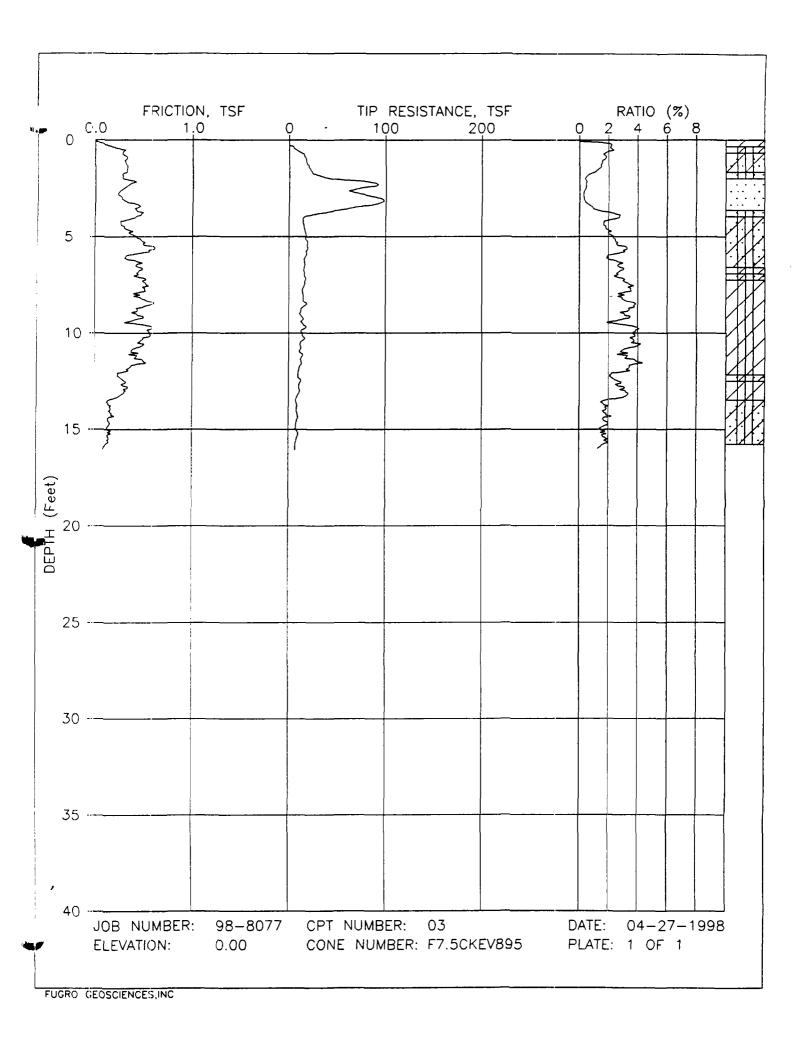
breaks down along planes into nodules

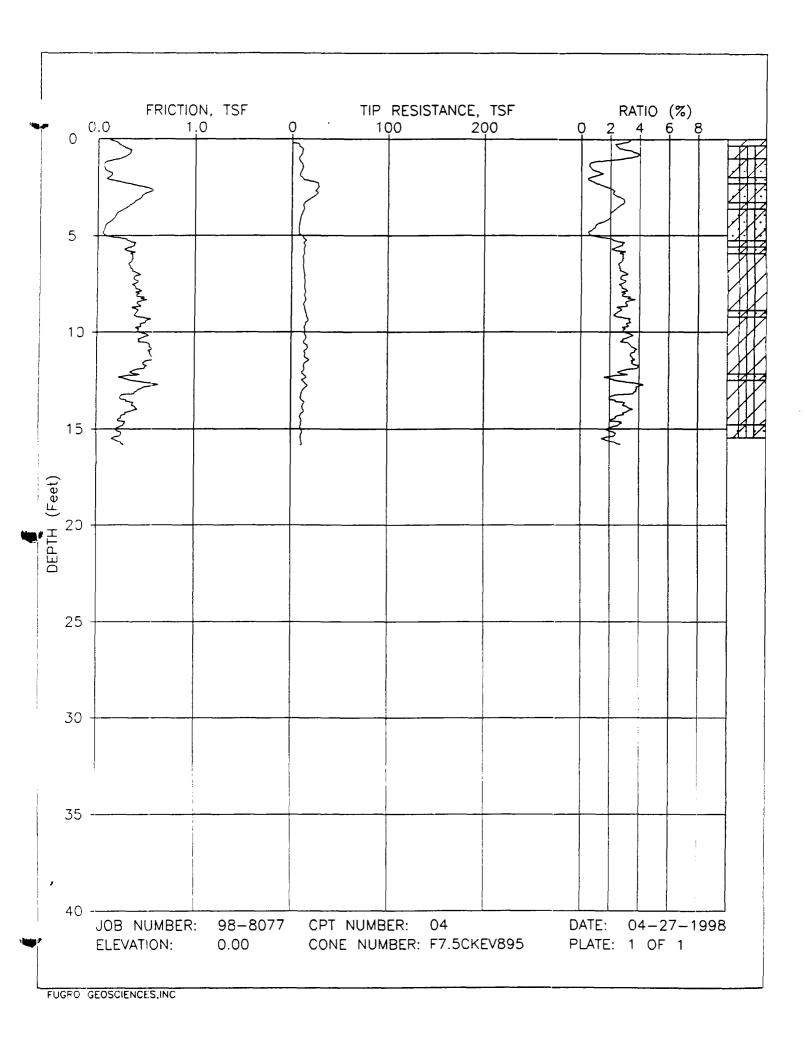
1/4" to 2" in size.

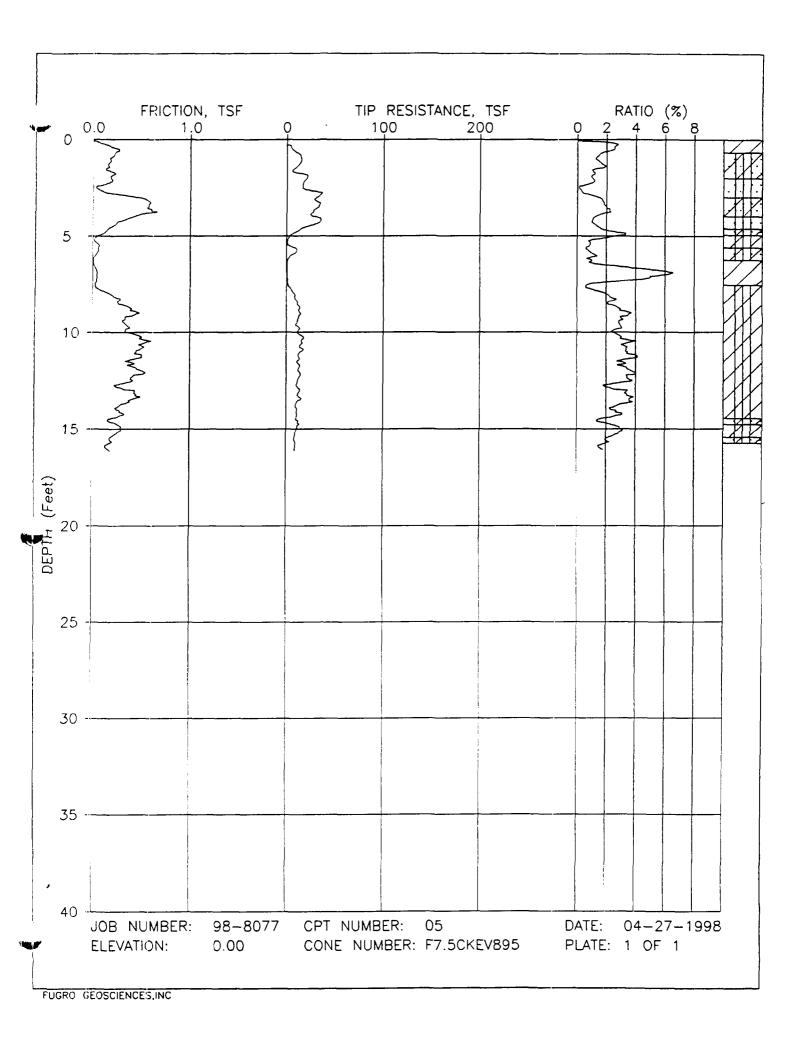
ROBERTSON AND CAMPANELLA SIMPLIFIED SOIL BEHAVIOR CHART (1983)

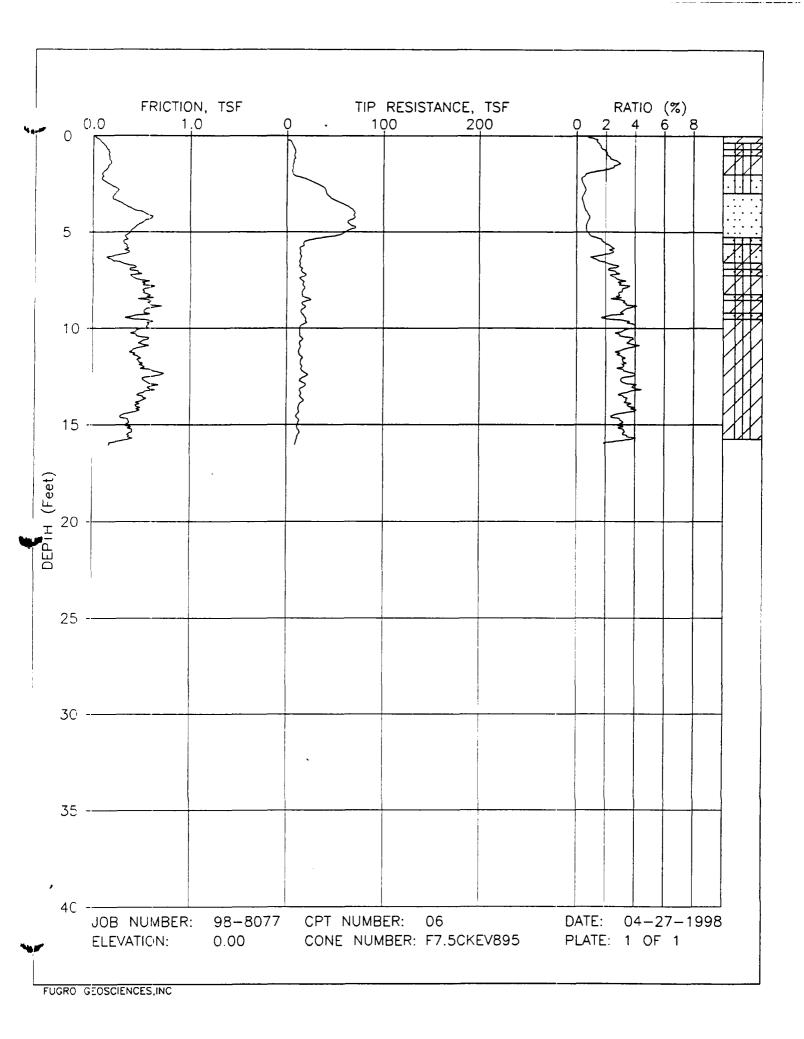


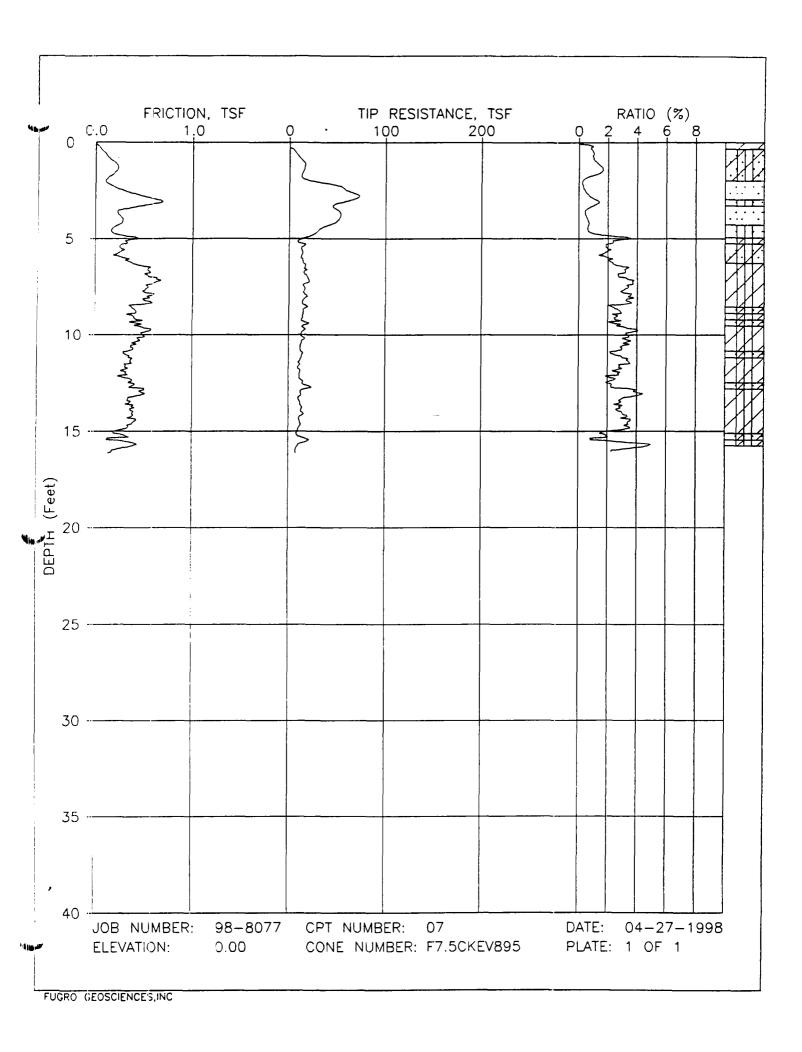


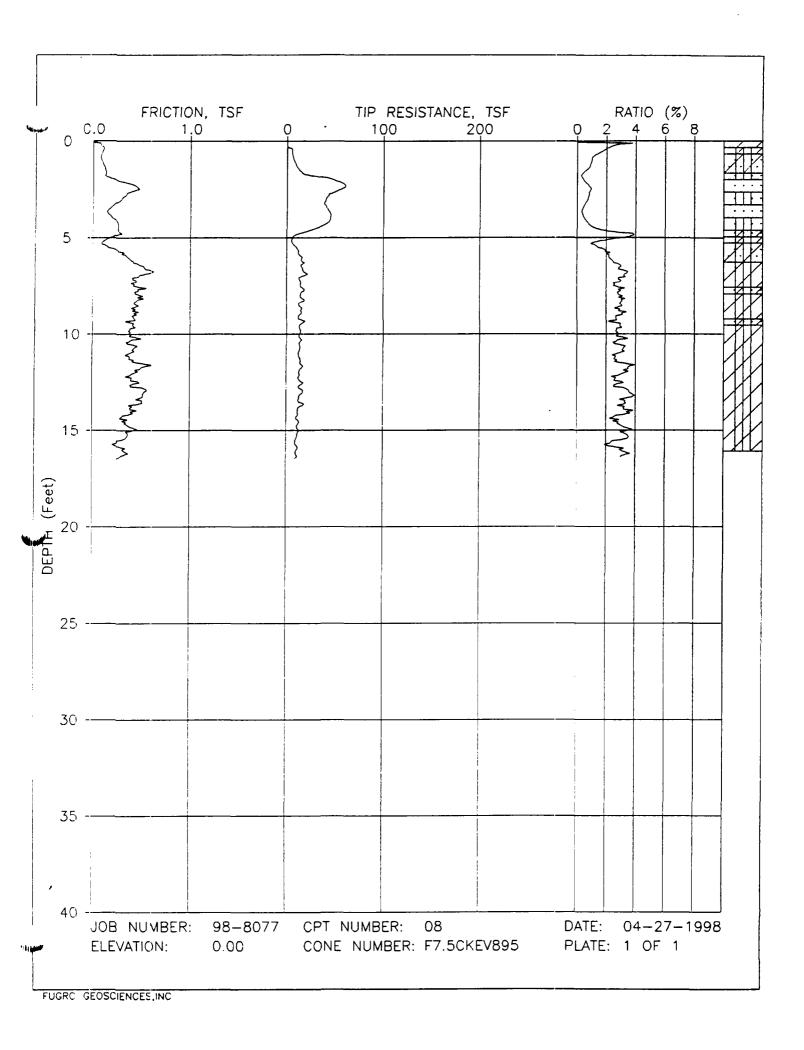


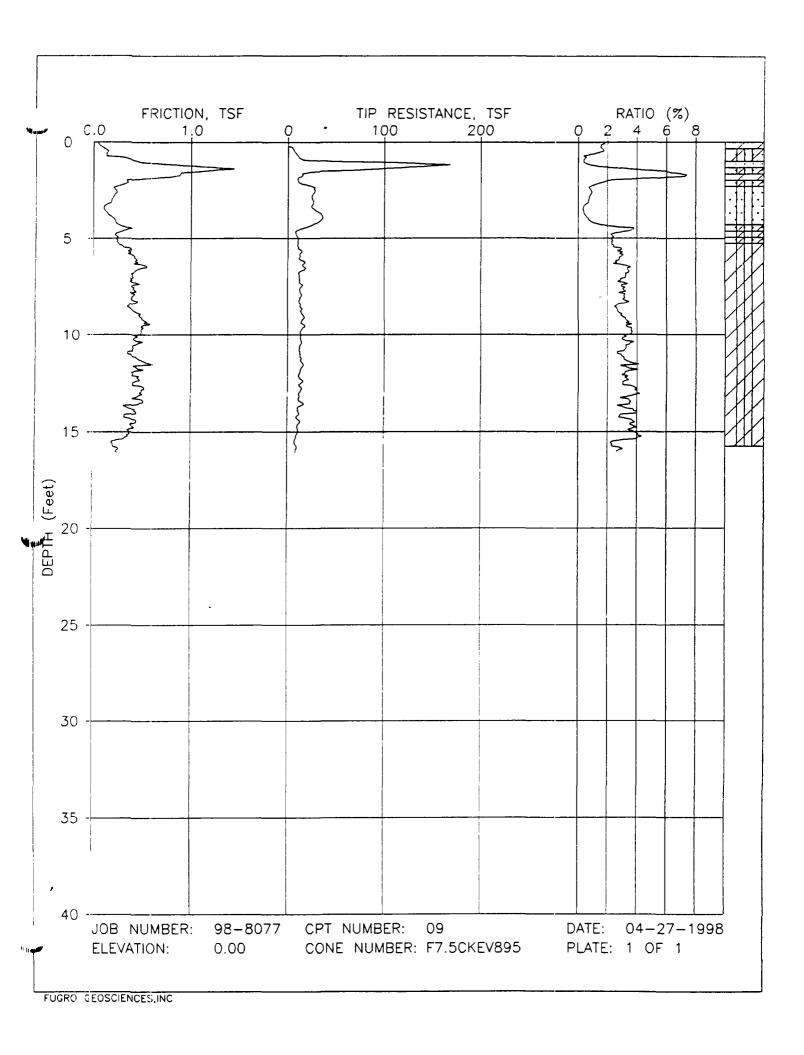


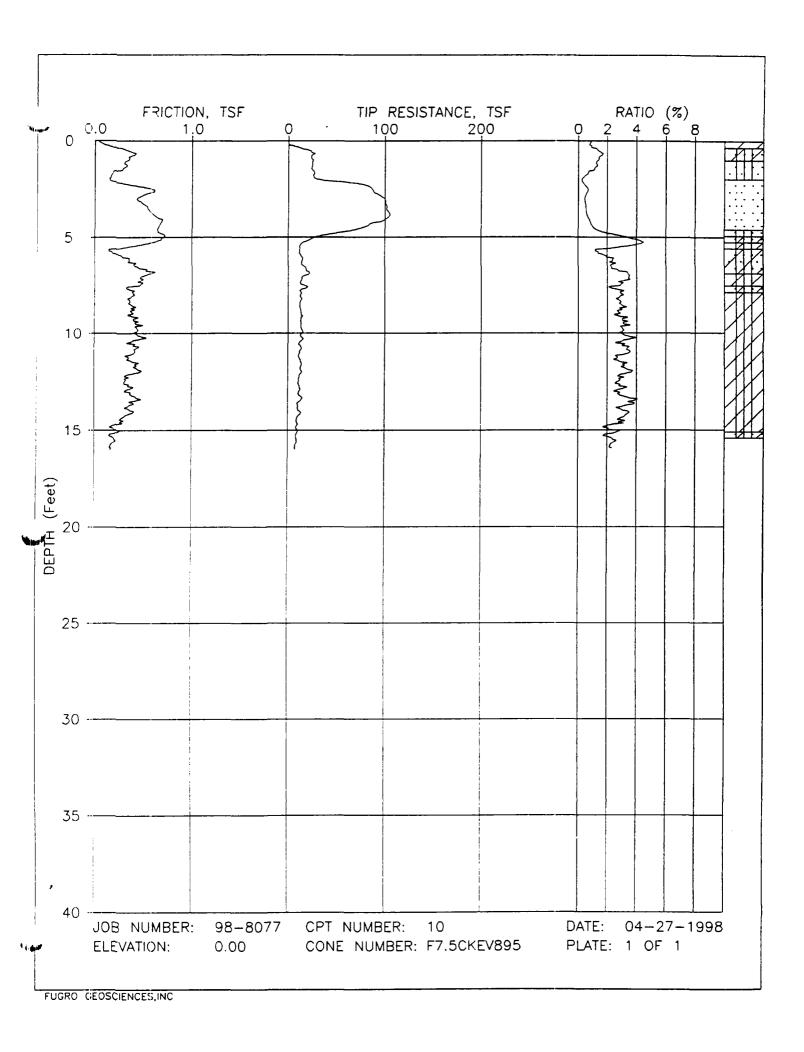


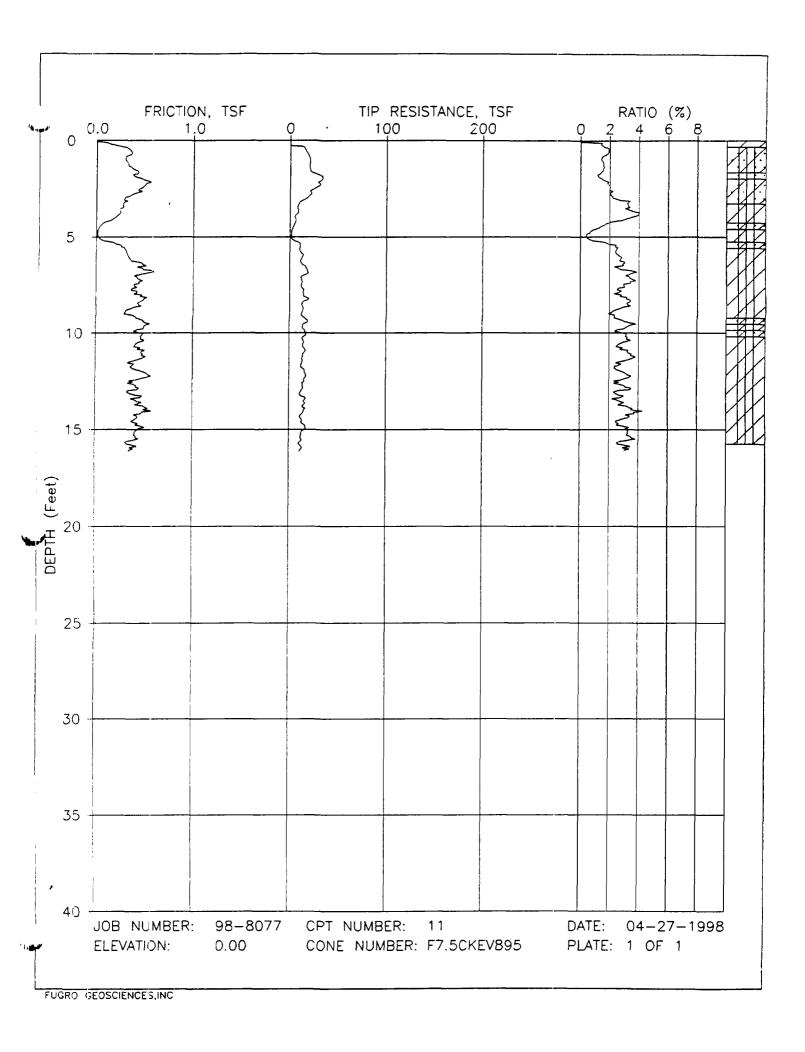


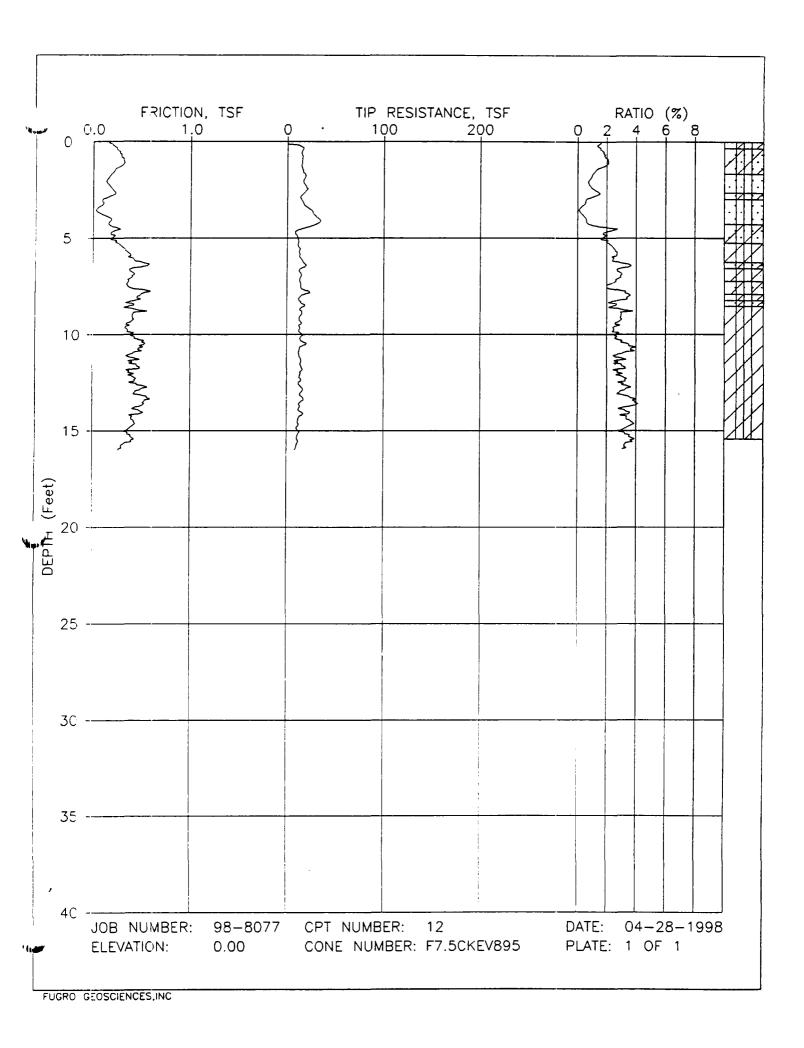


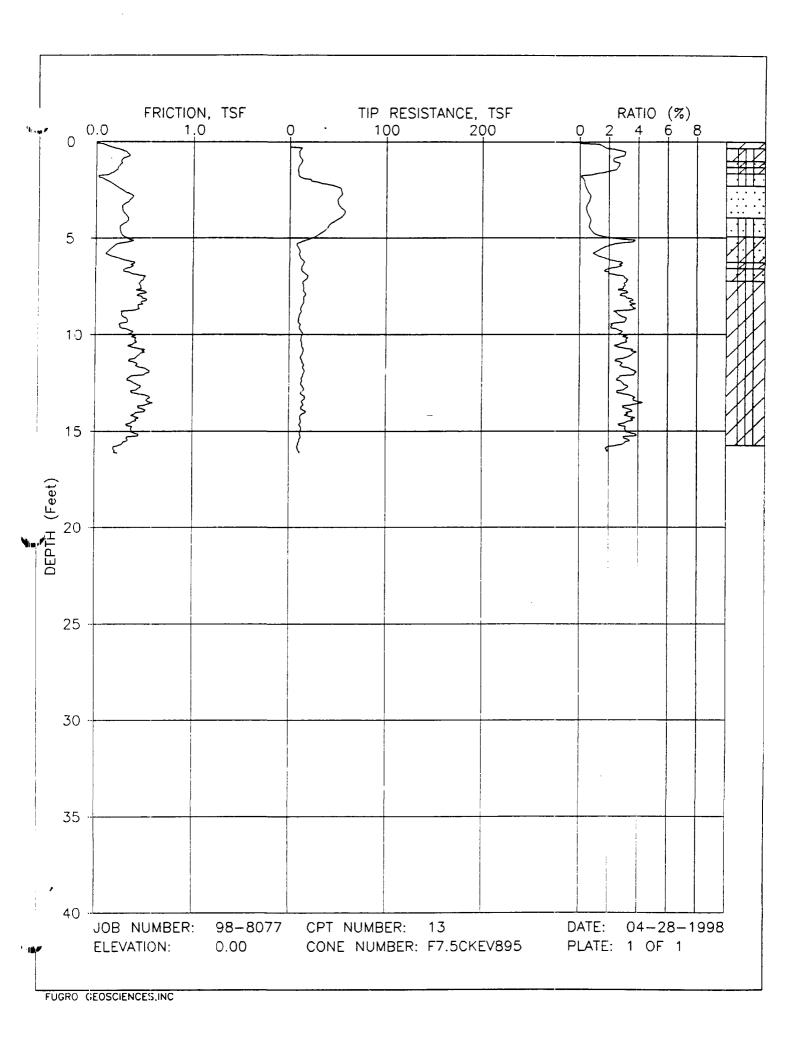


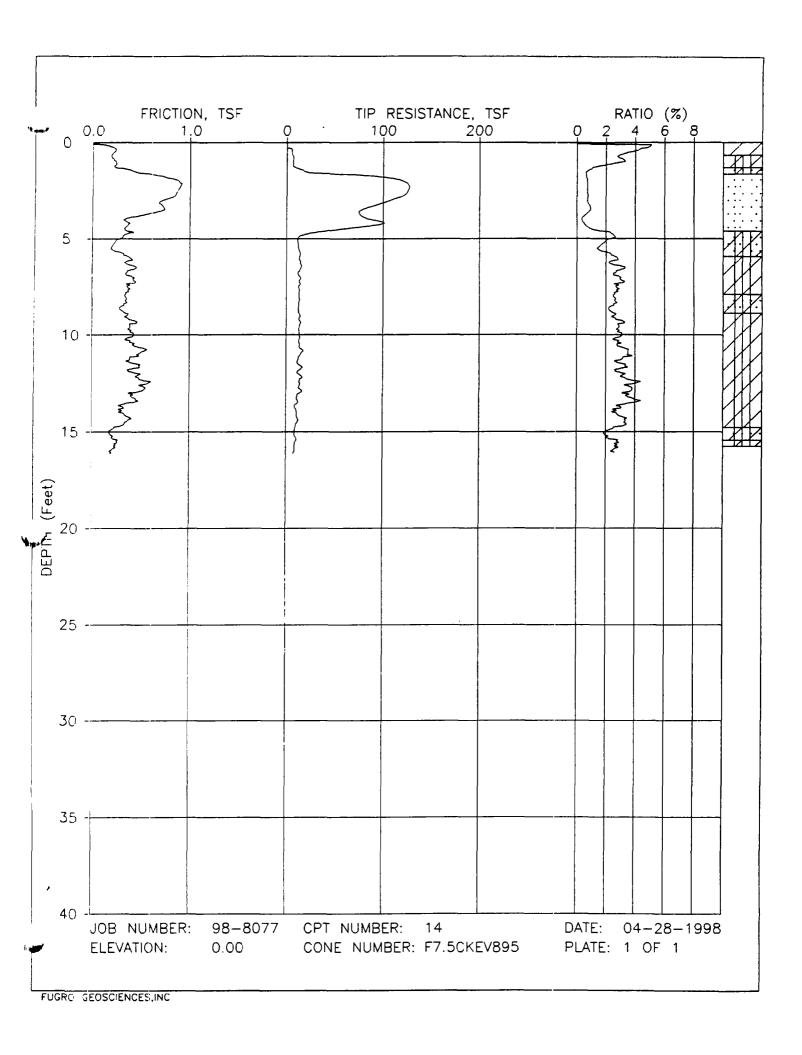


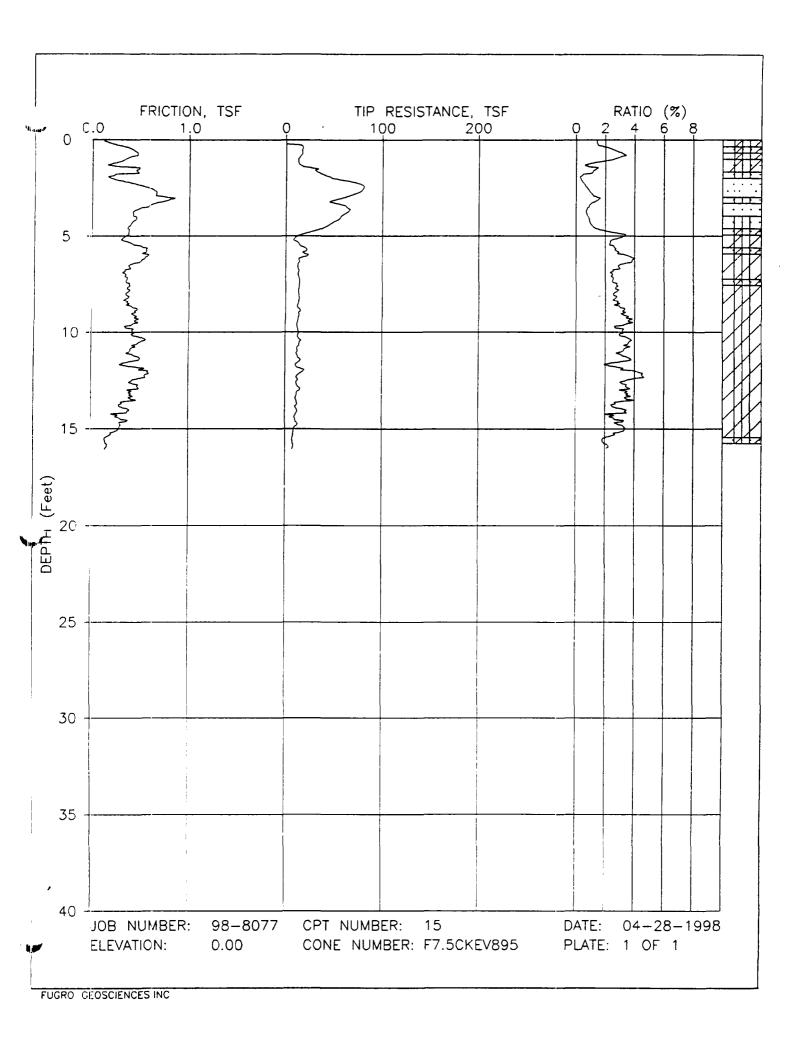


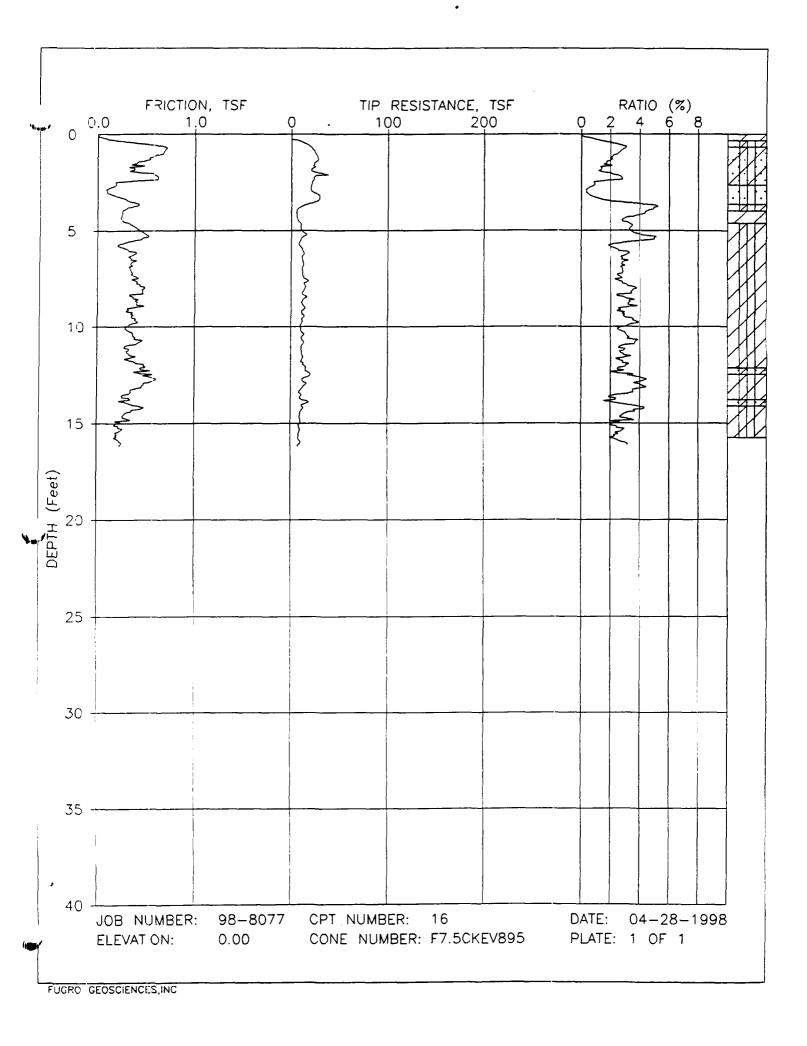


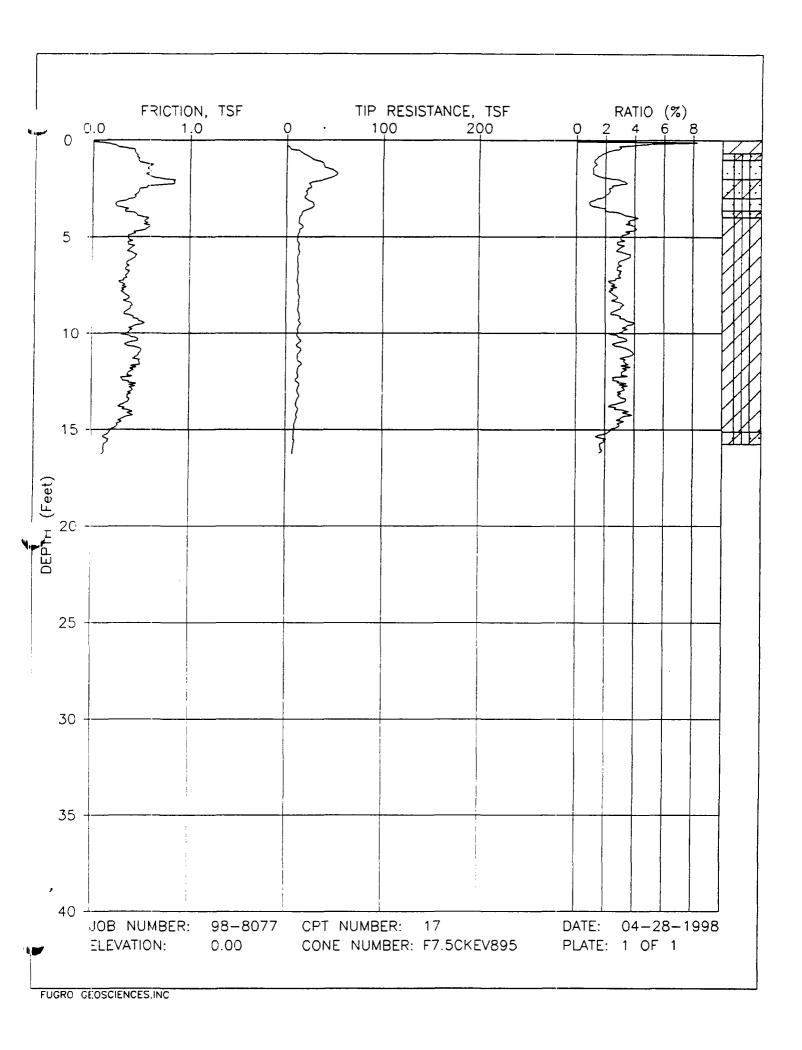


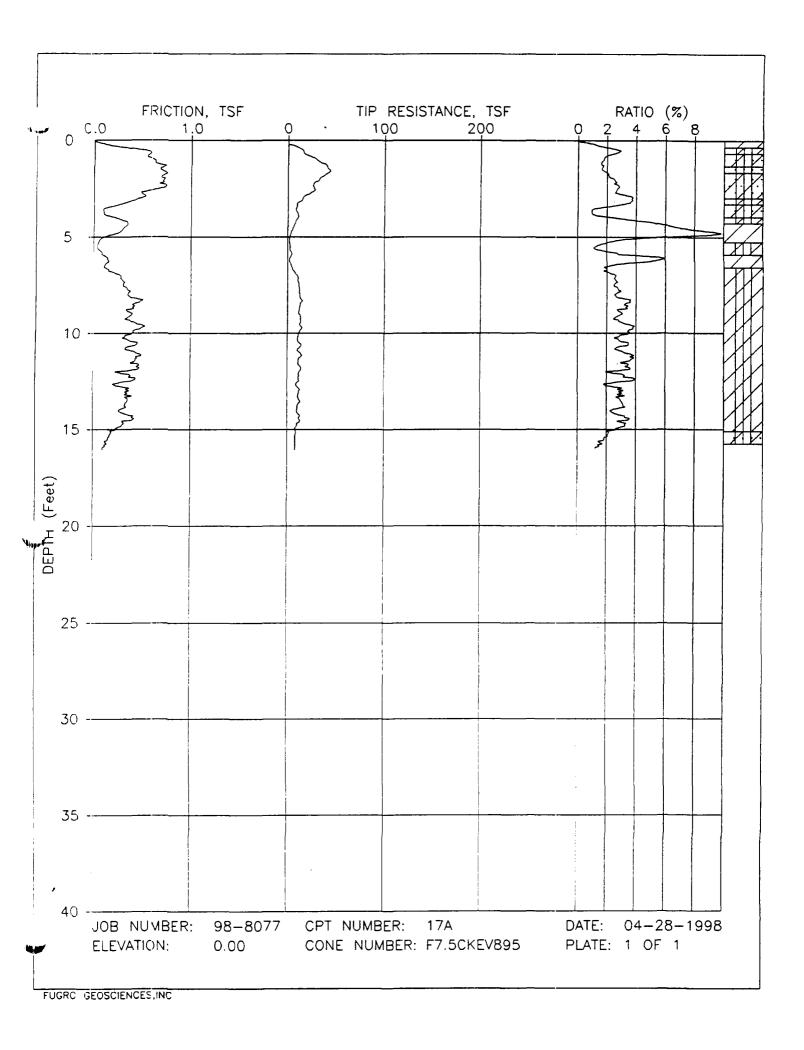


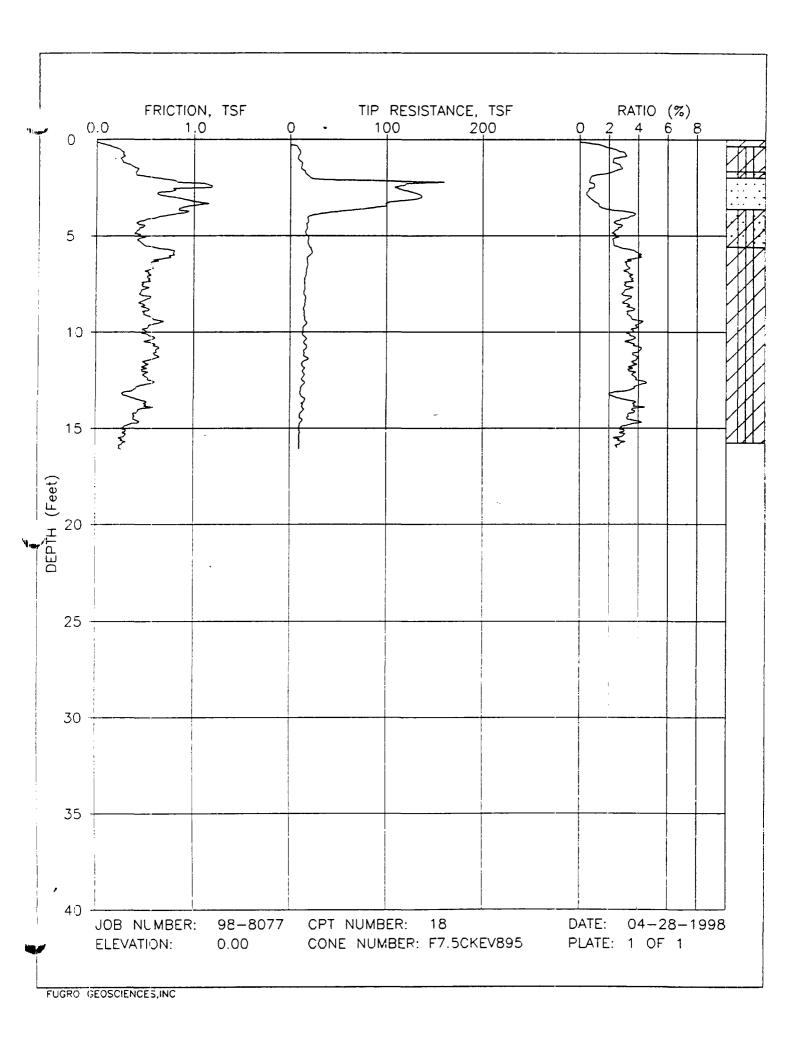


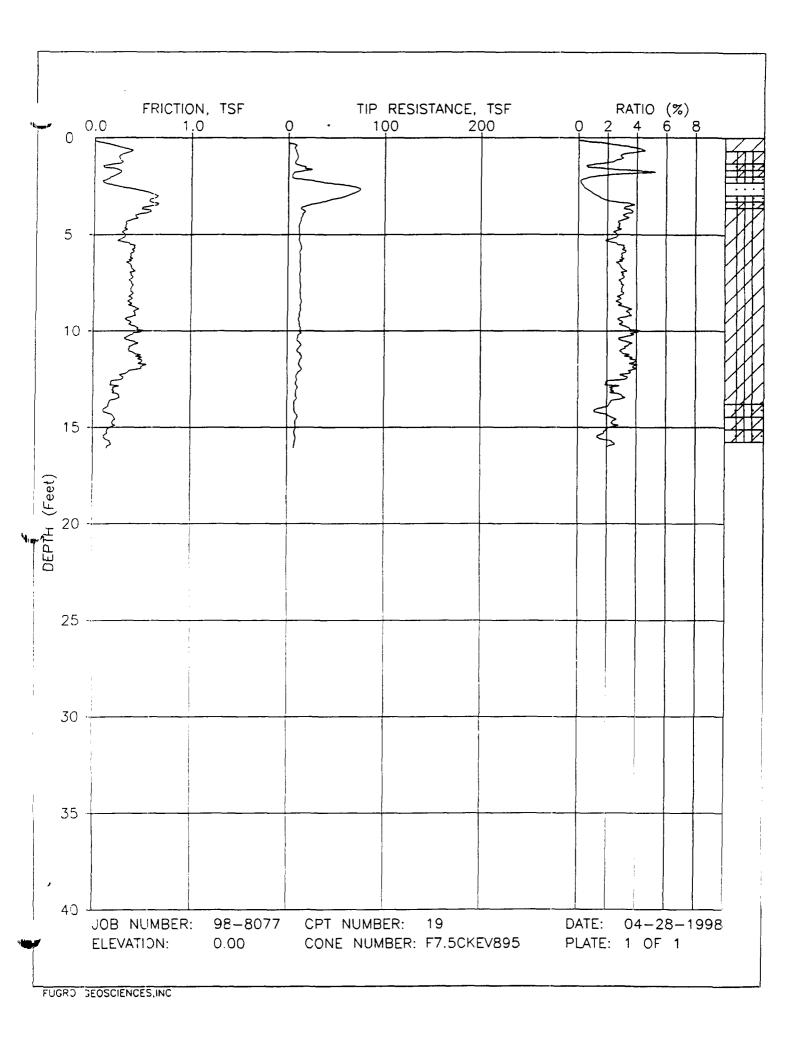


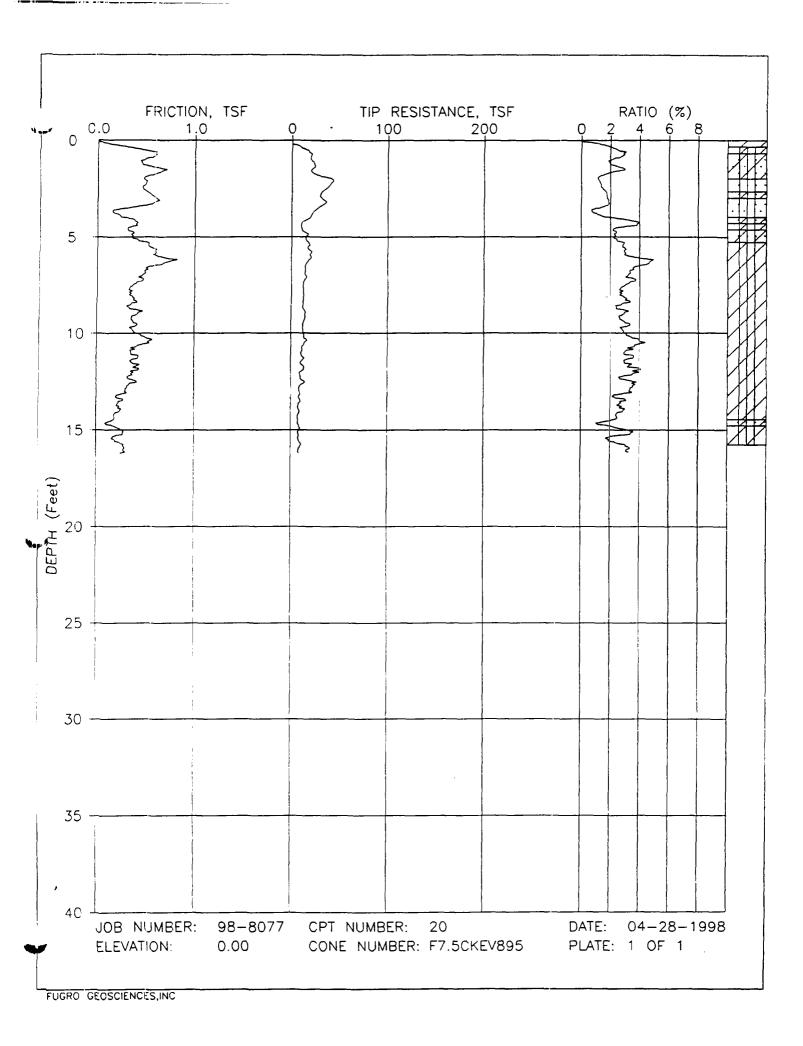


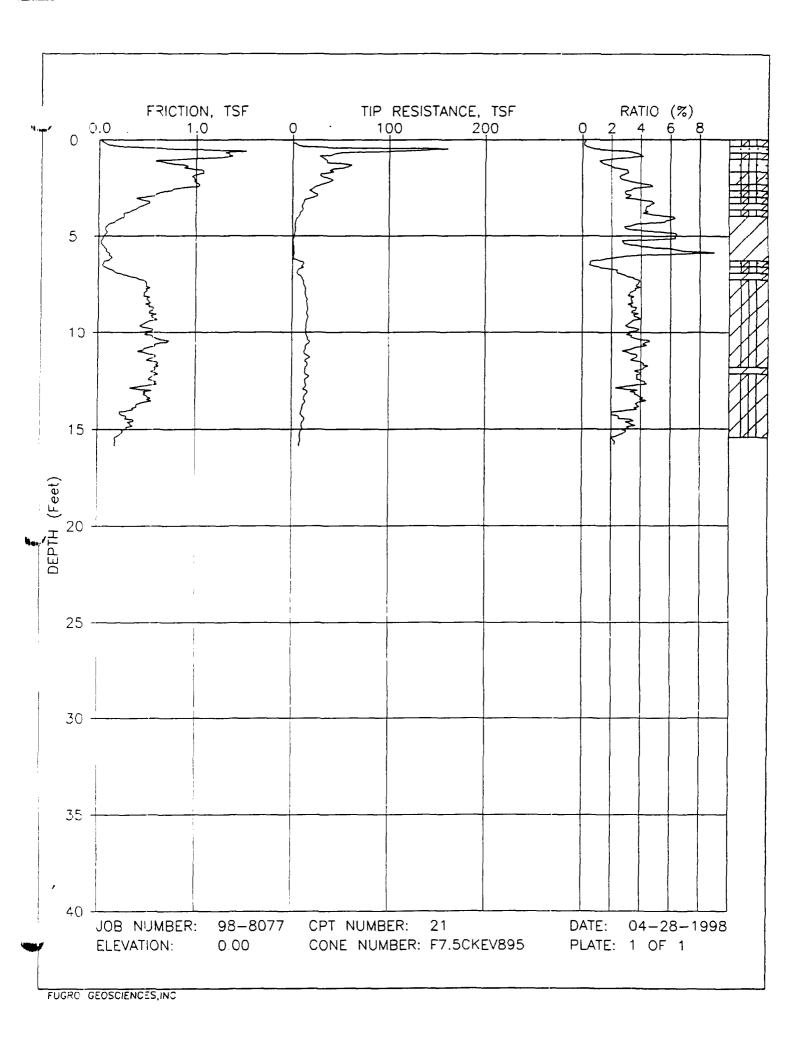


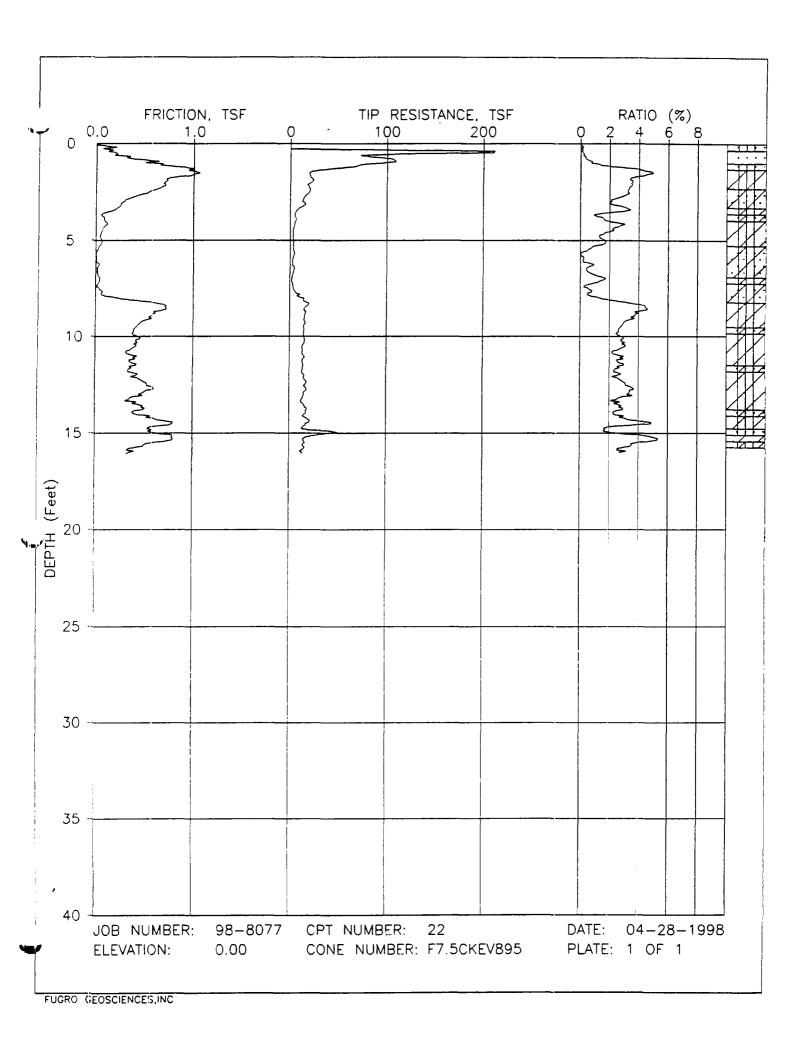


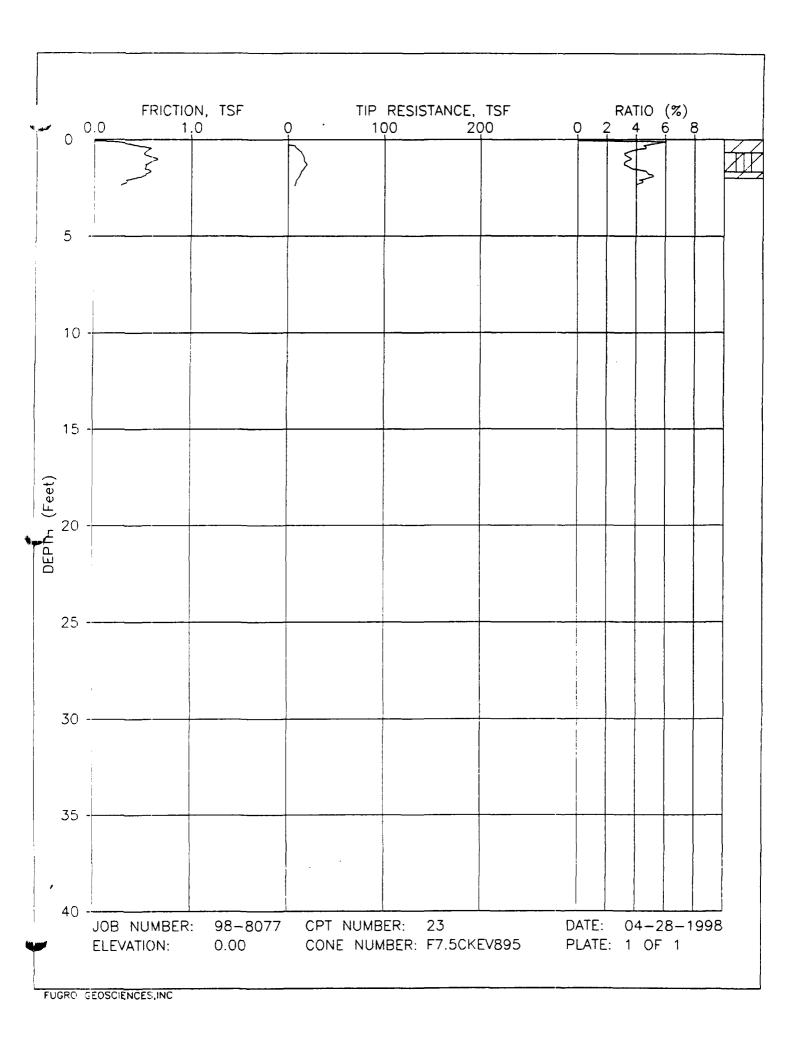


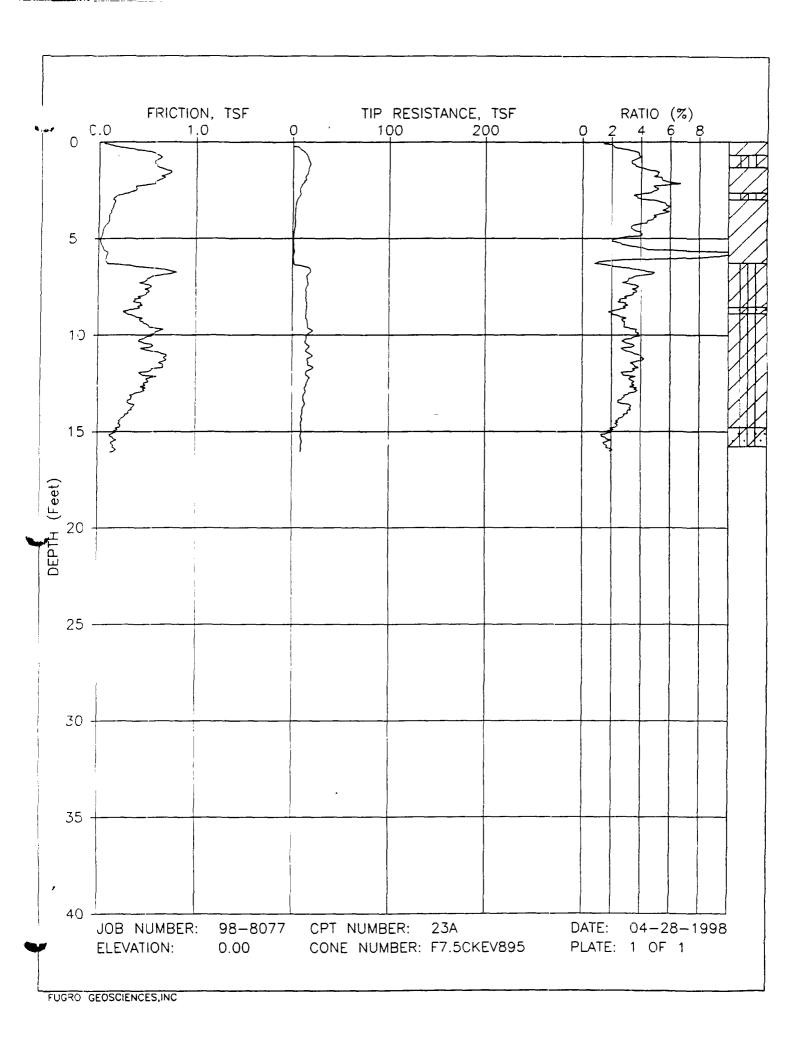


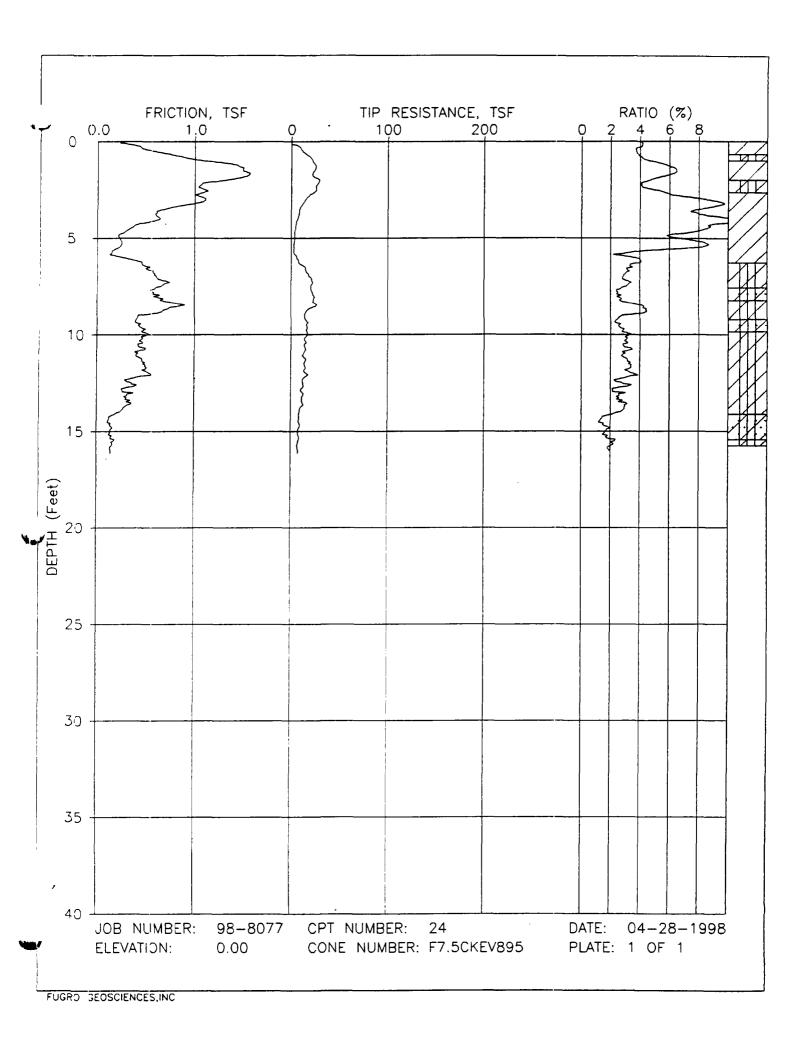


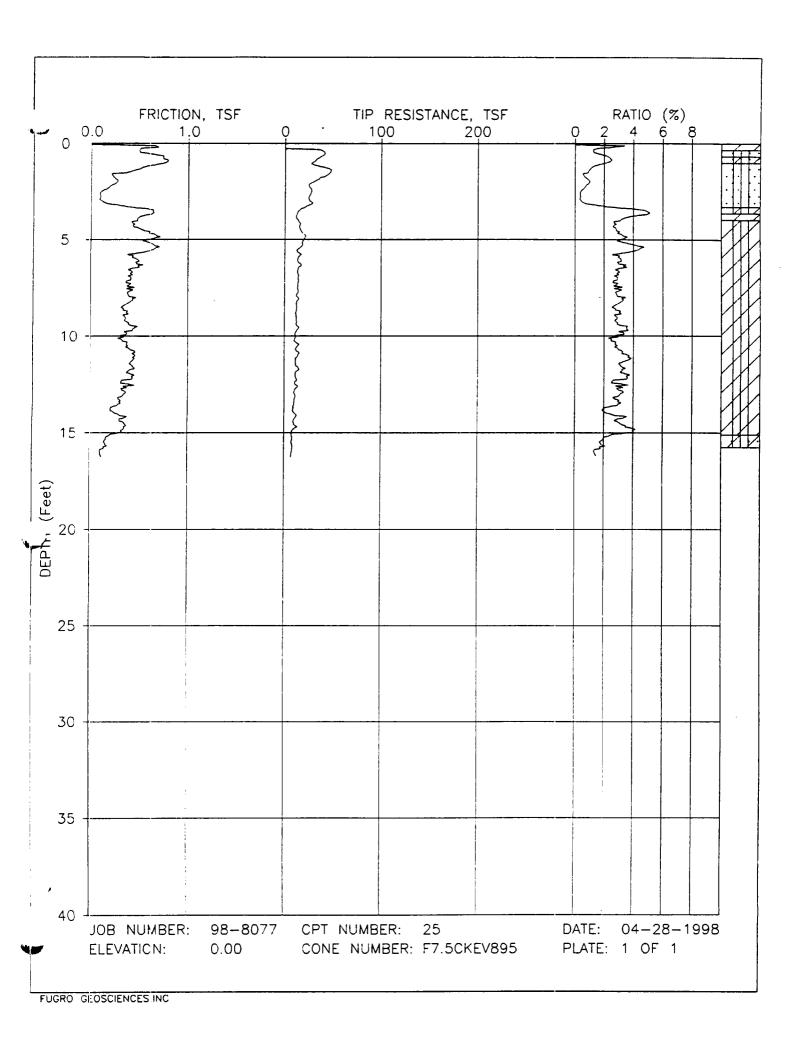


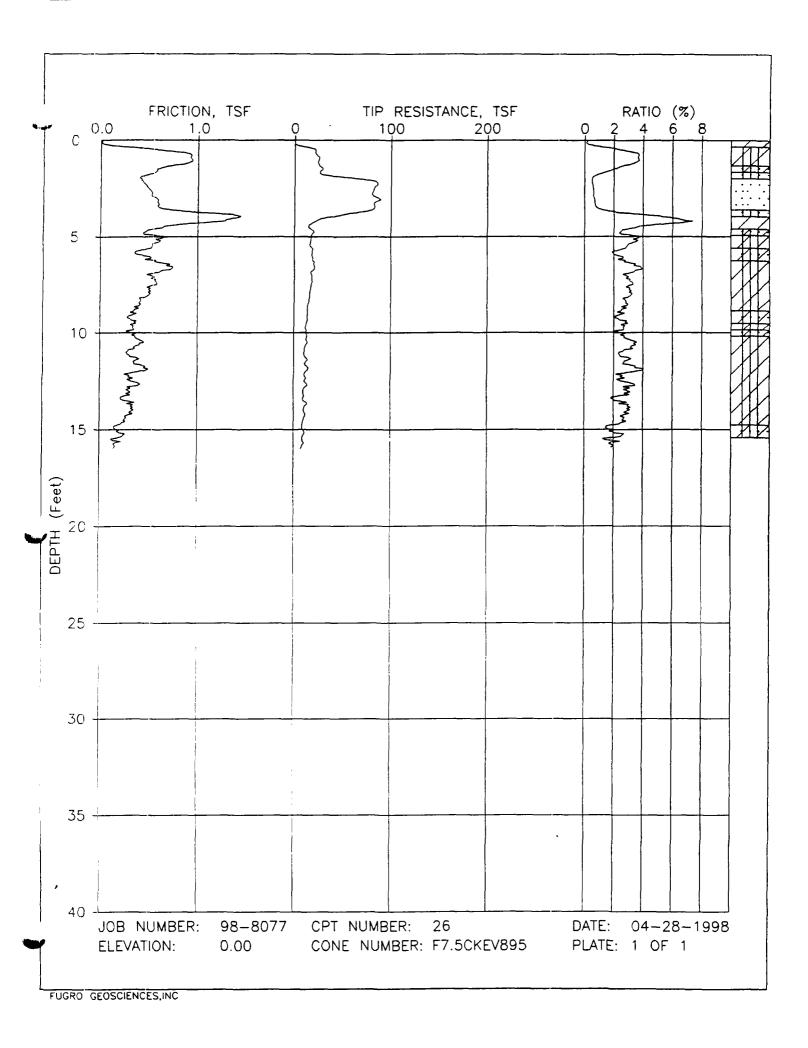


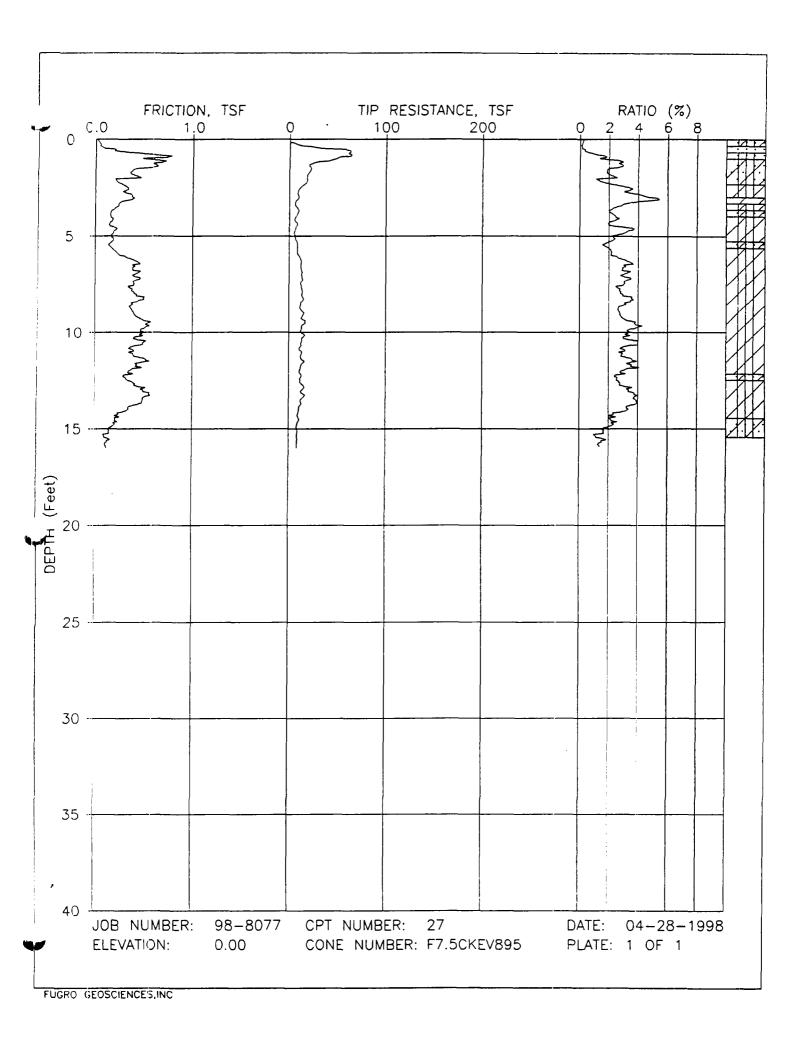


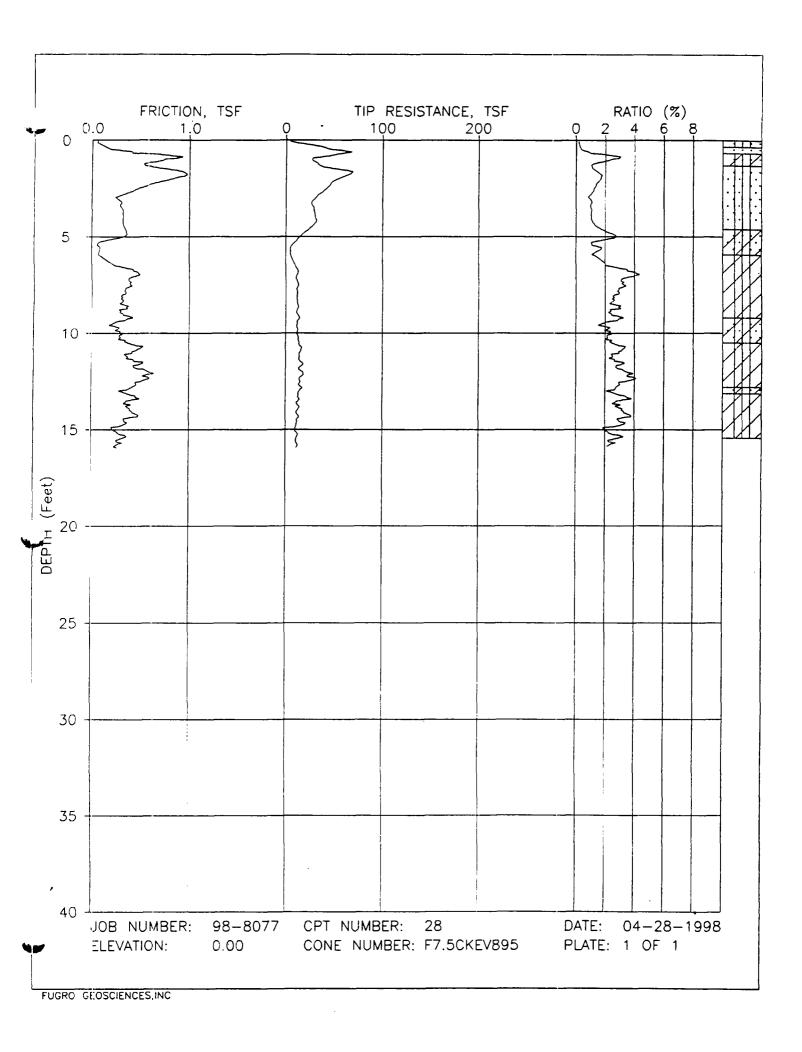


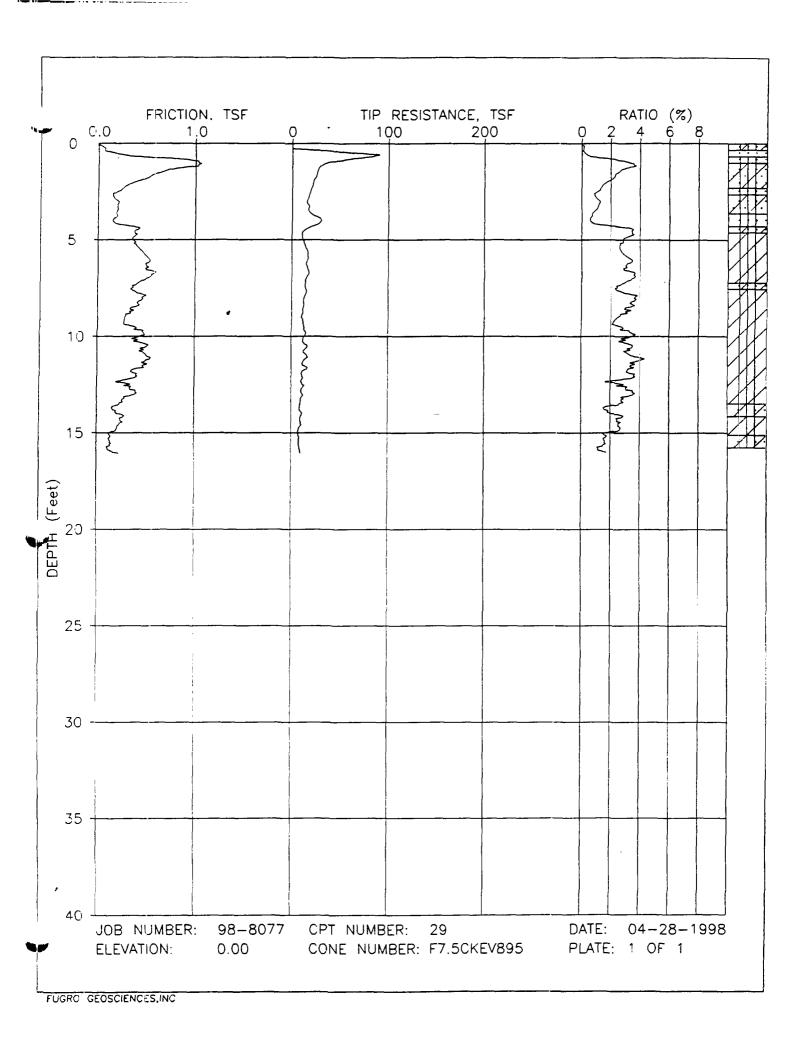


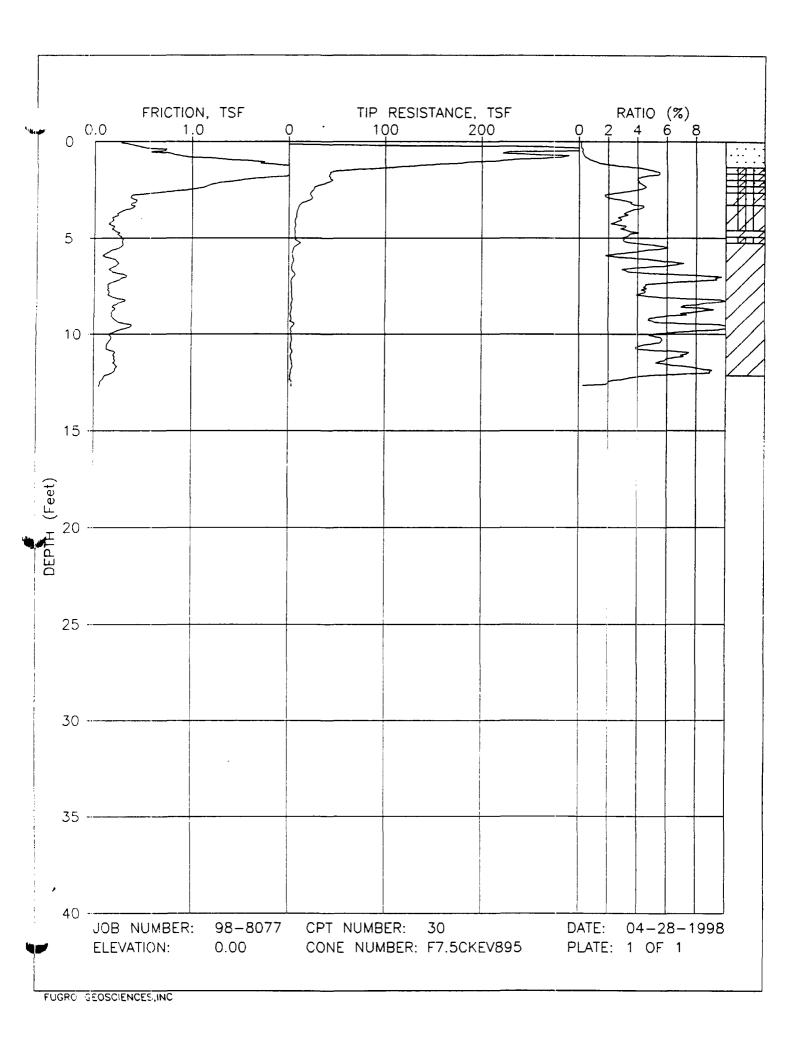


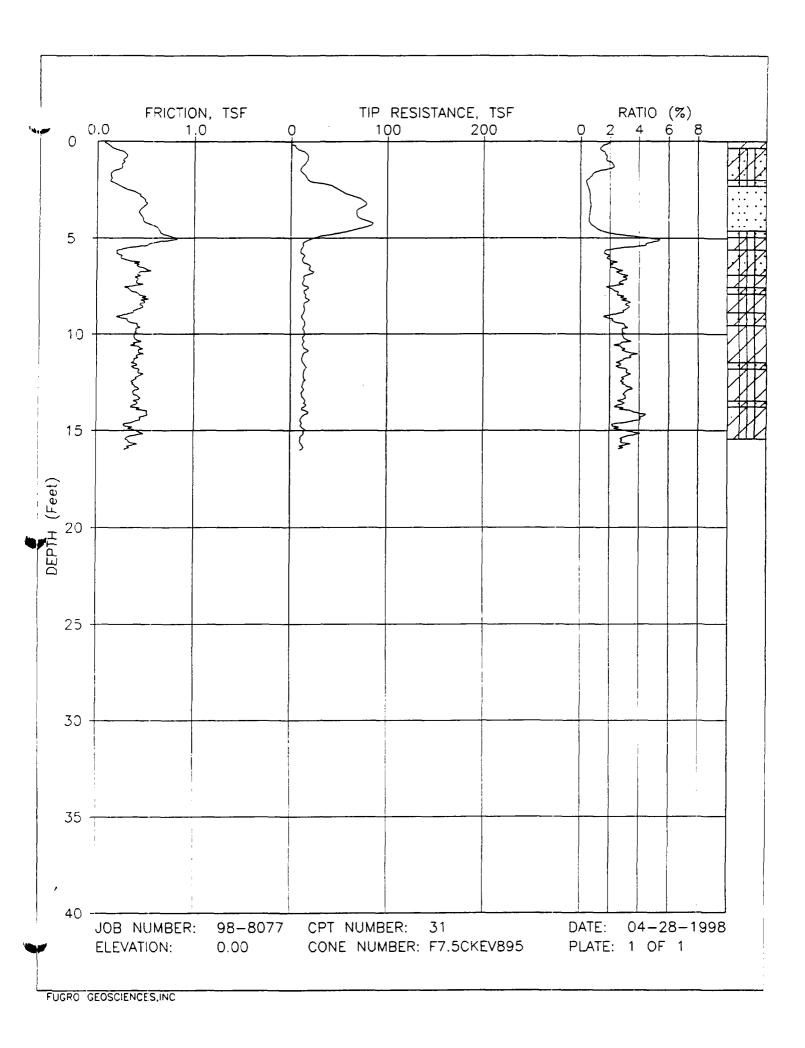


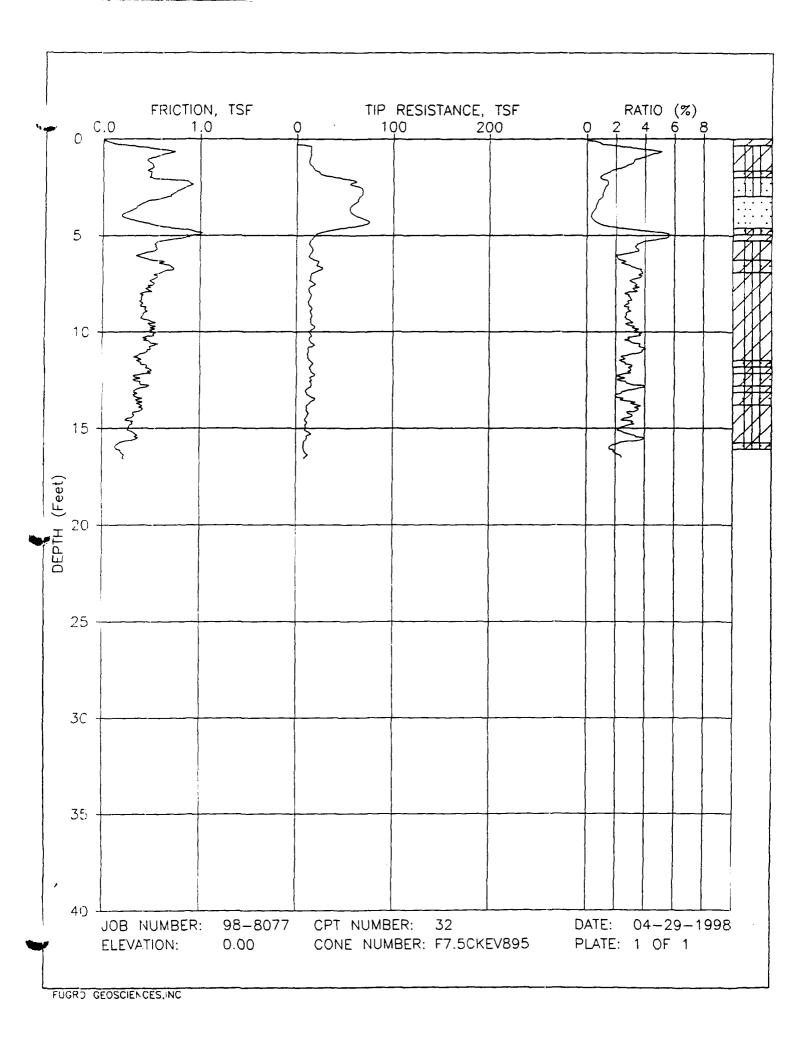


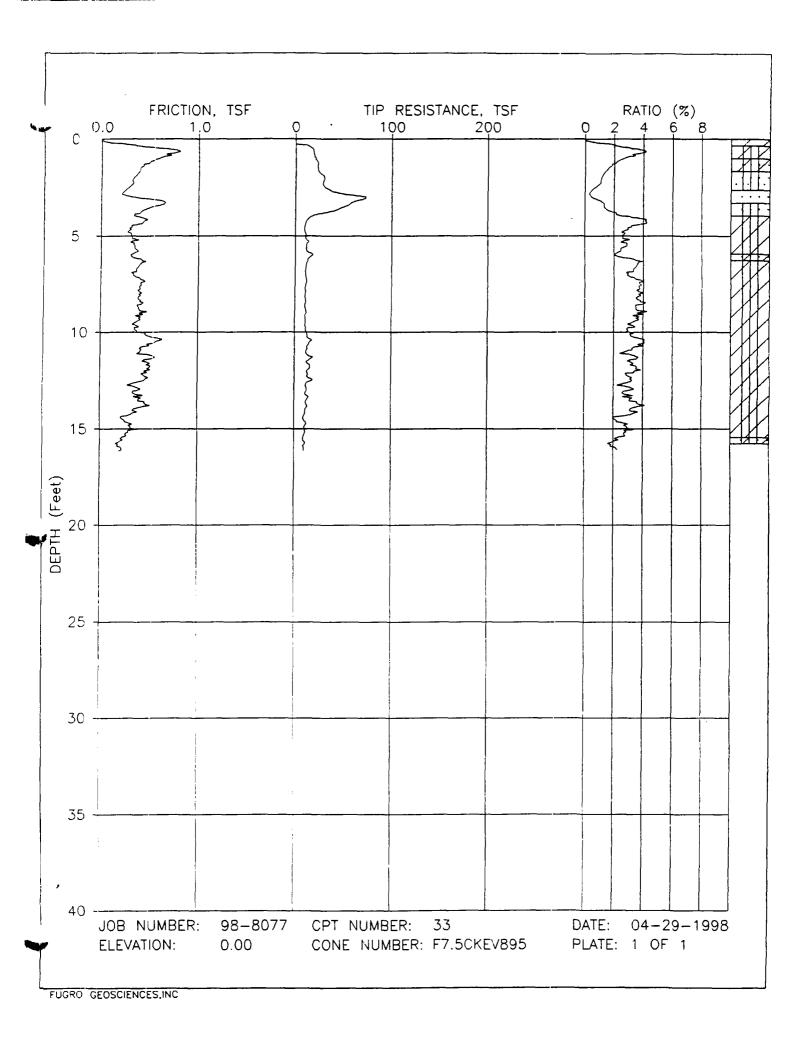


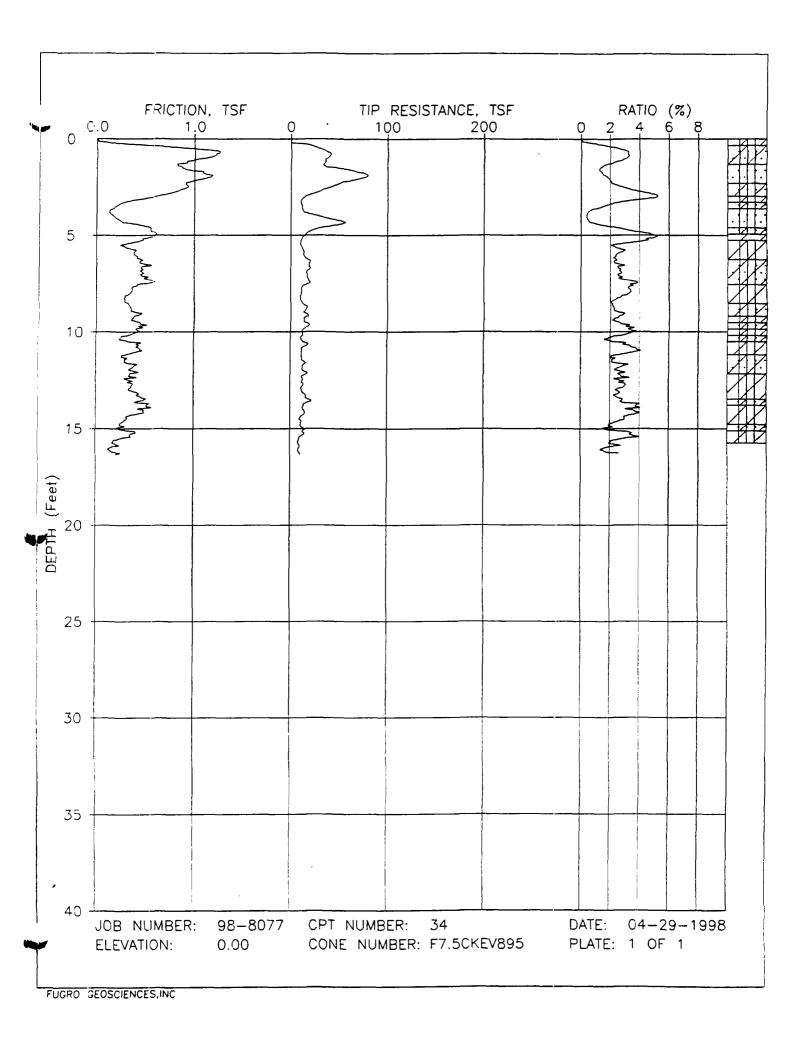


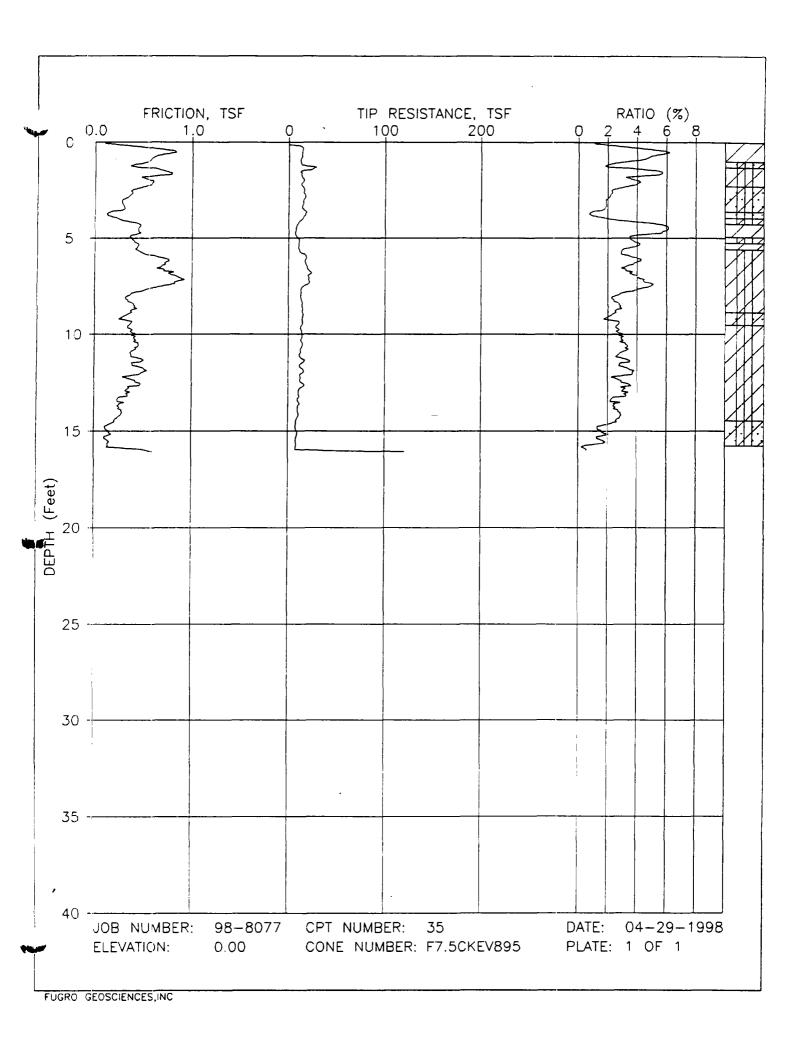


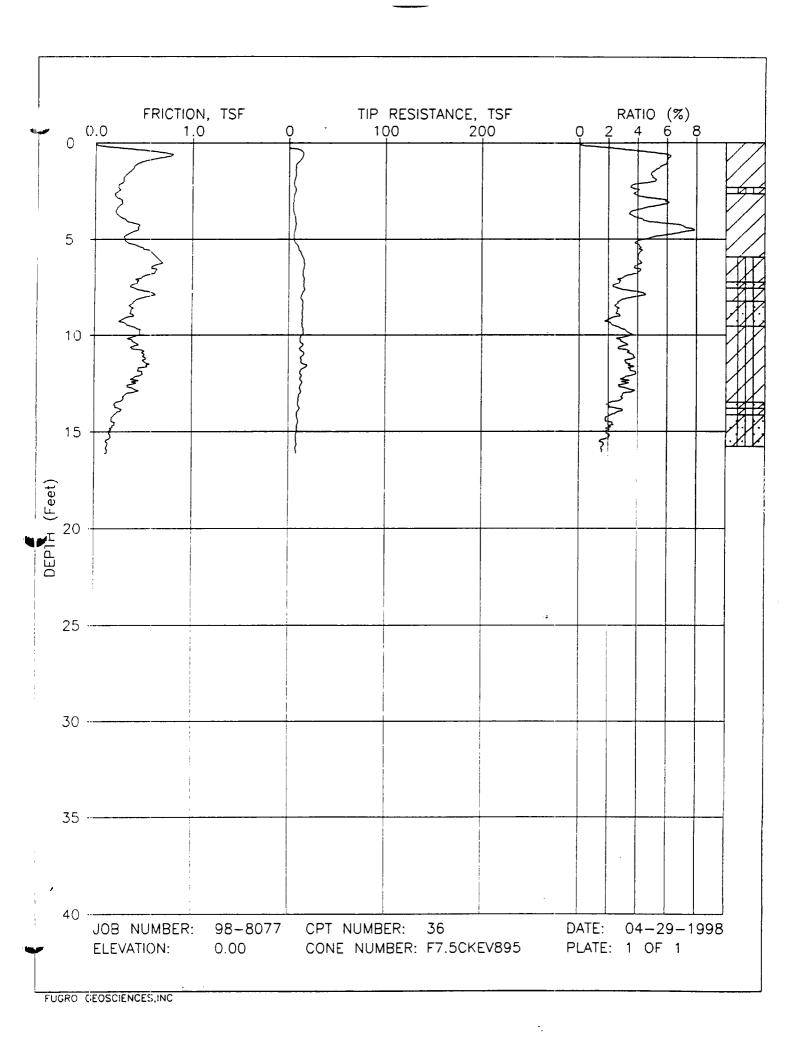


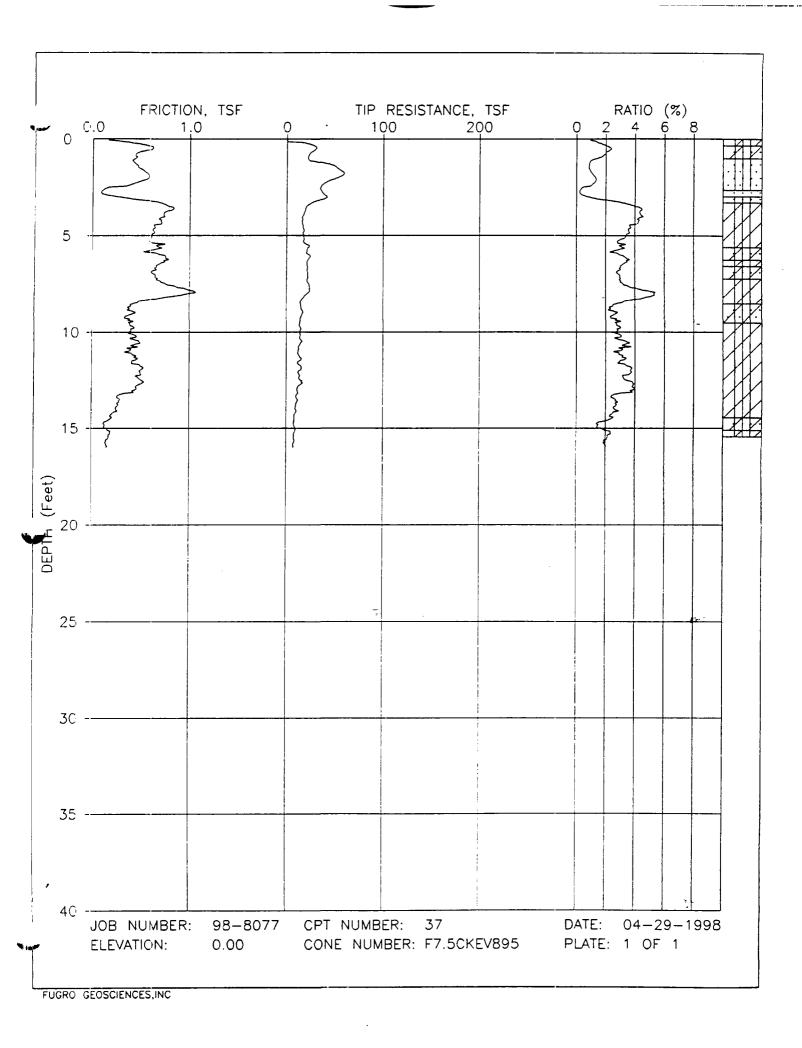


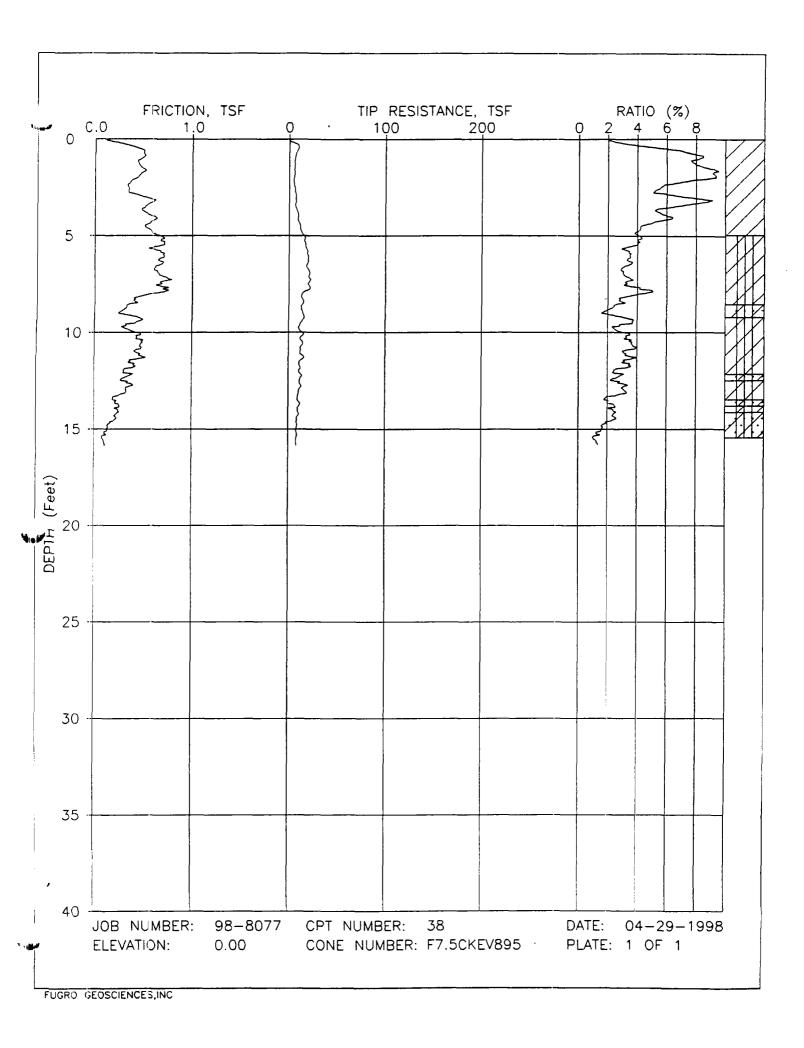


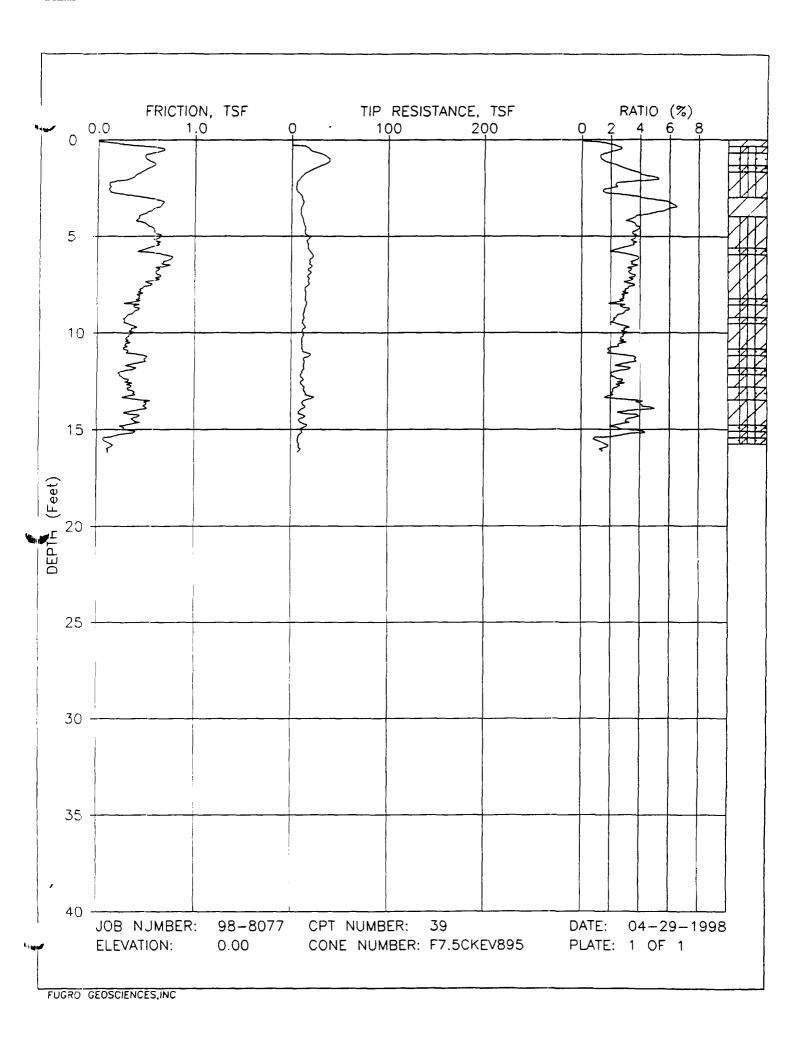


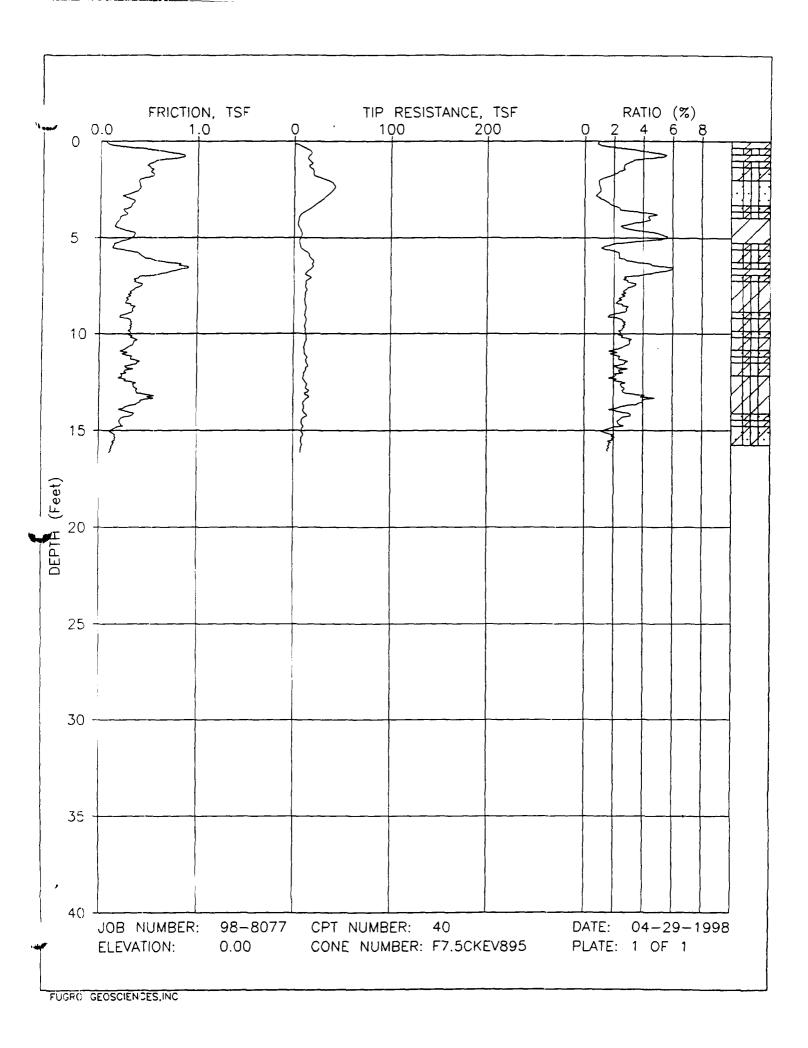


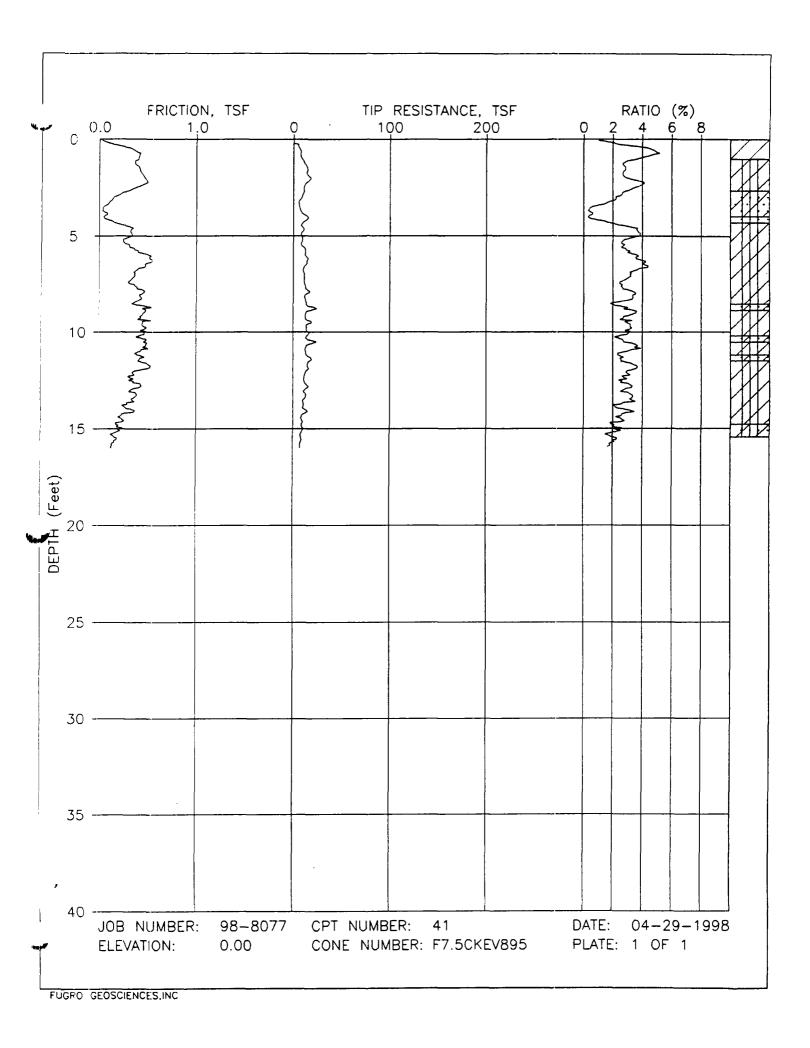


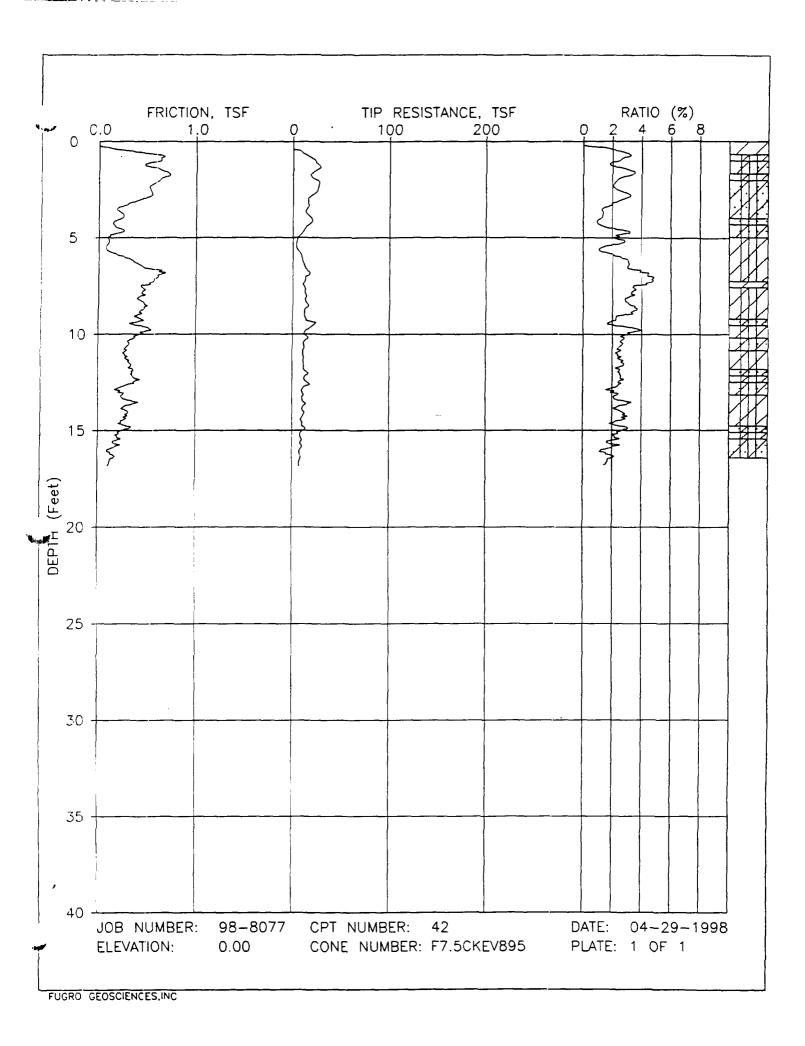


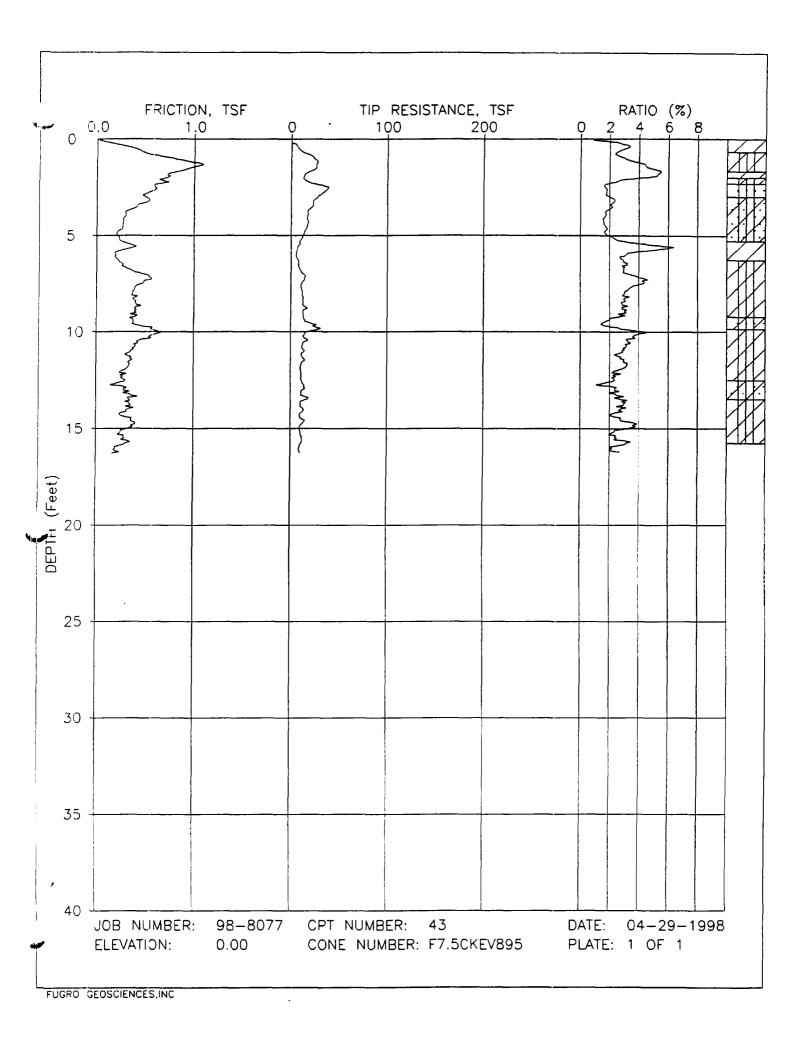


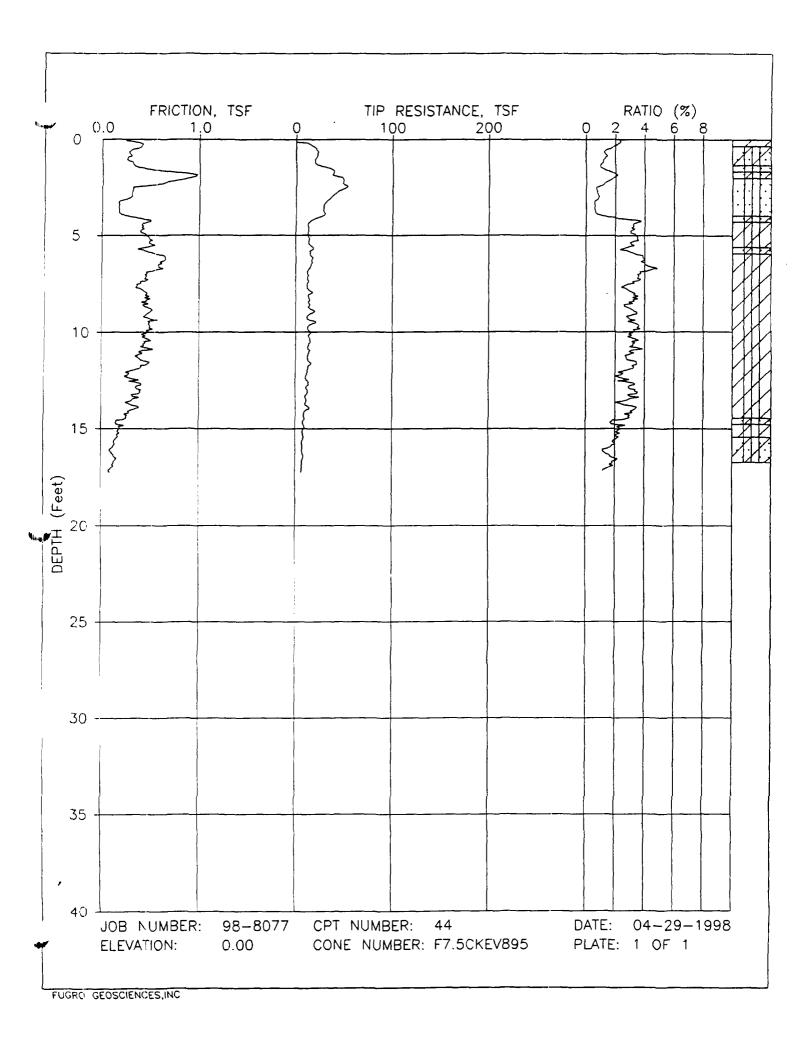


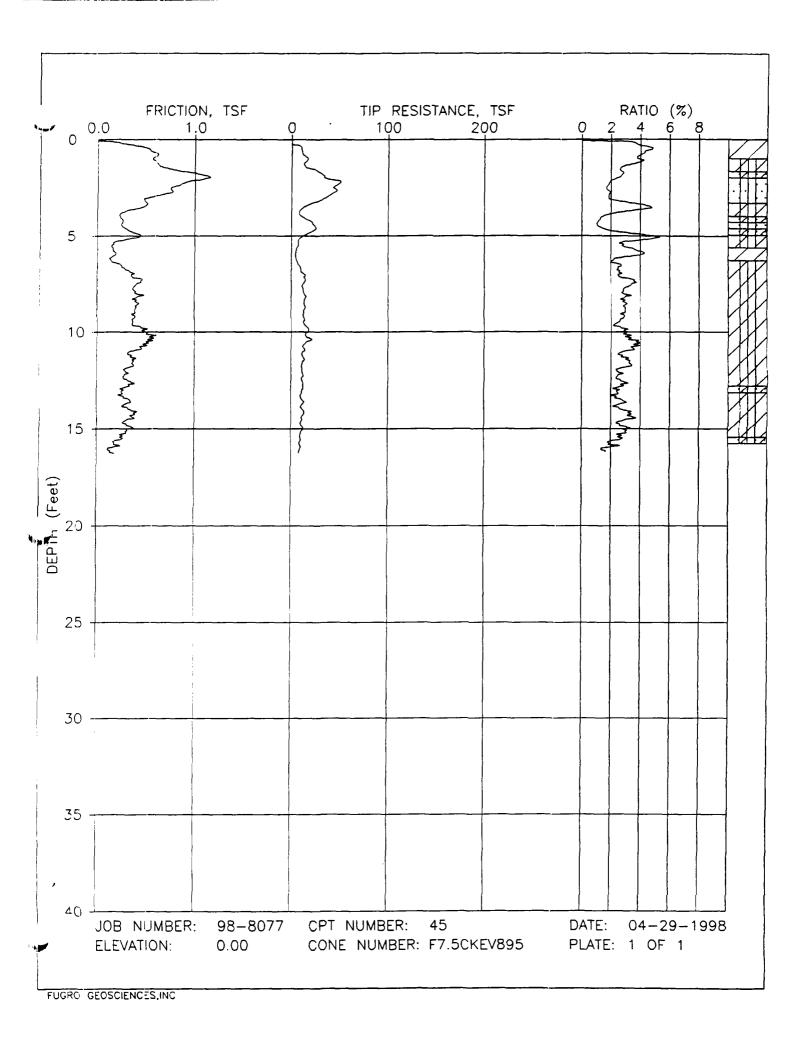


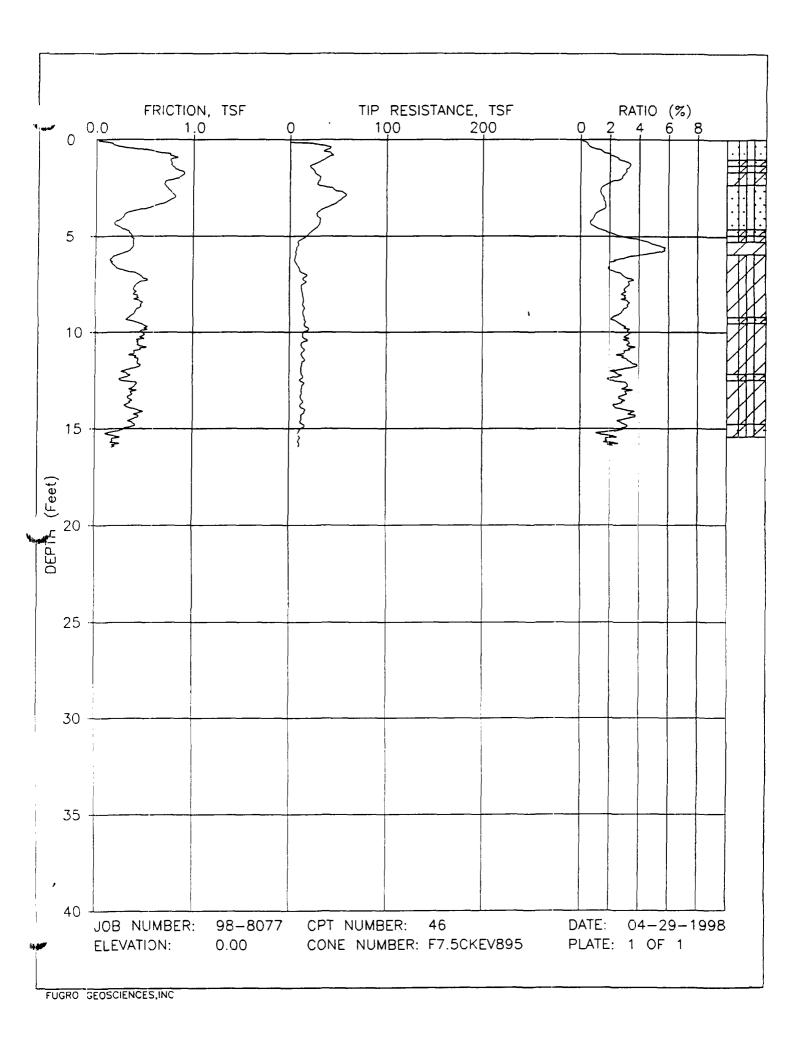


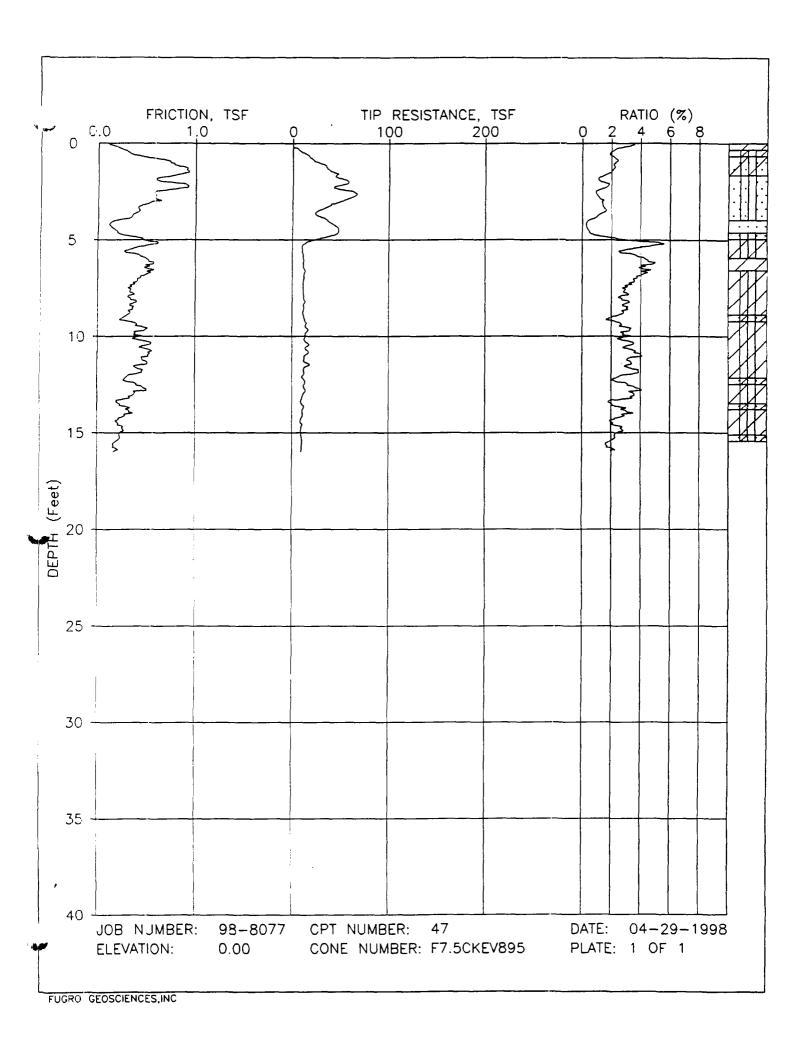


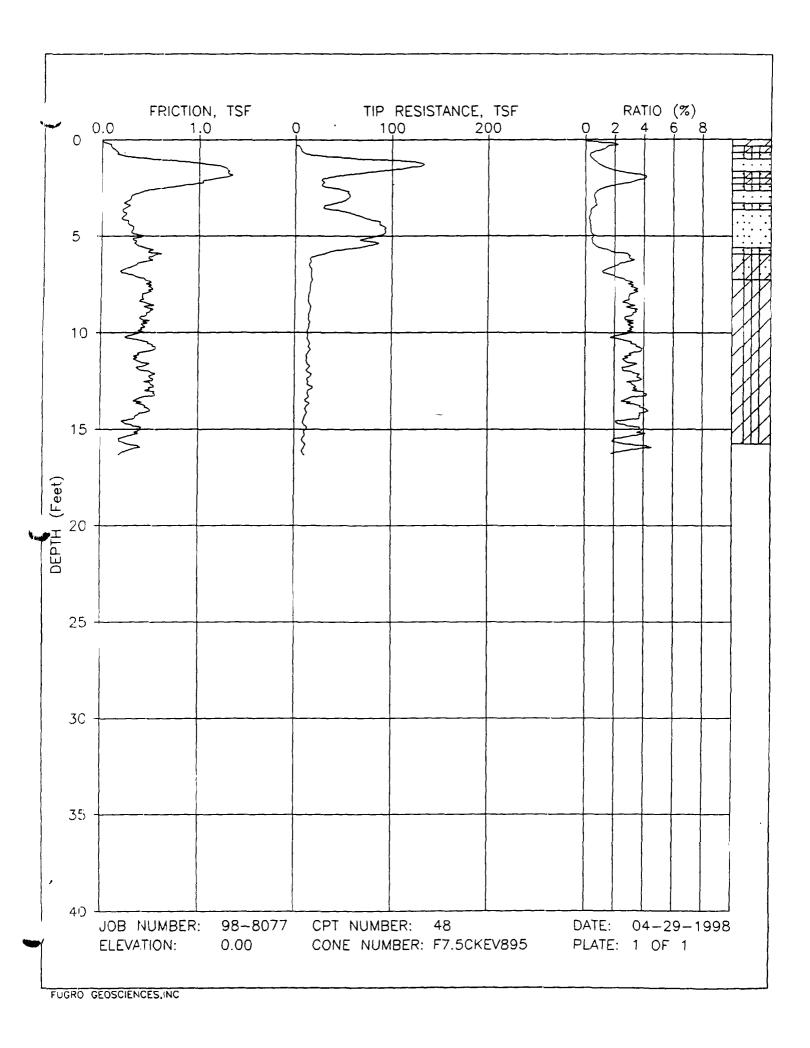


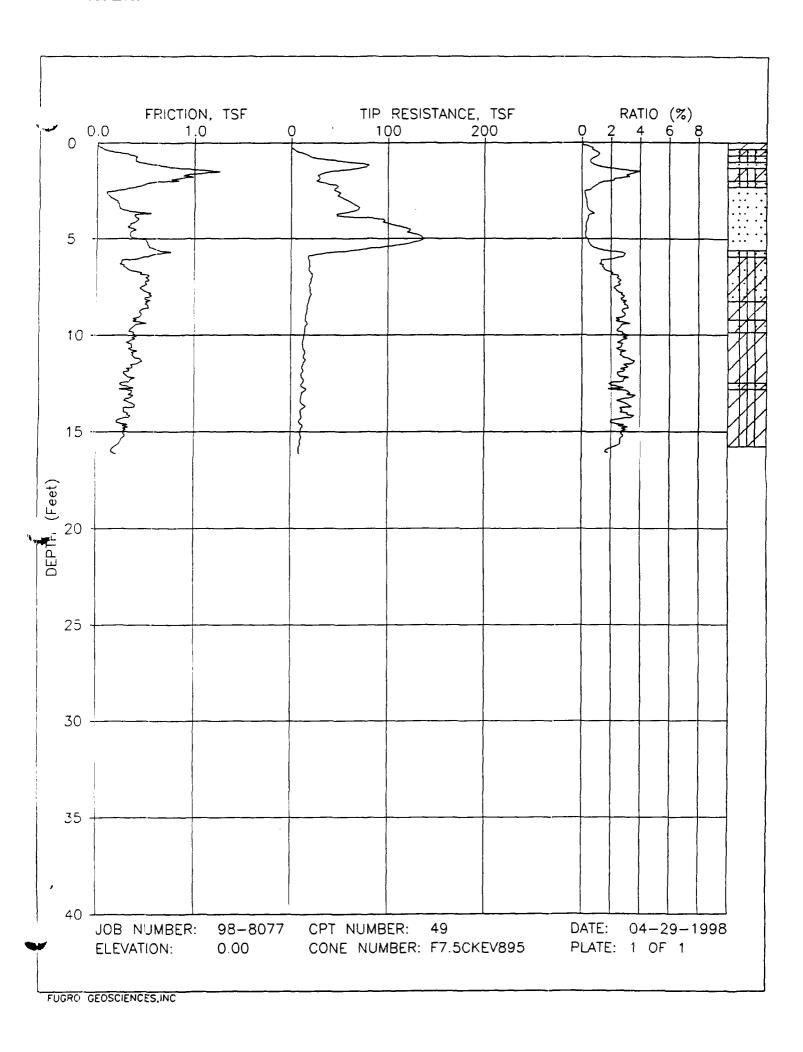


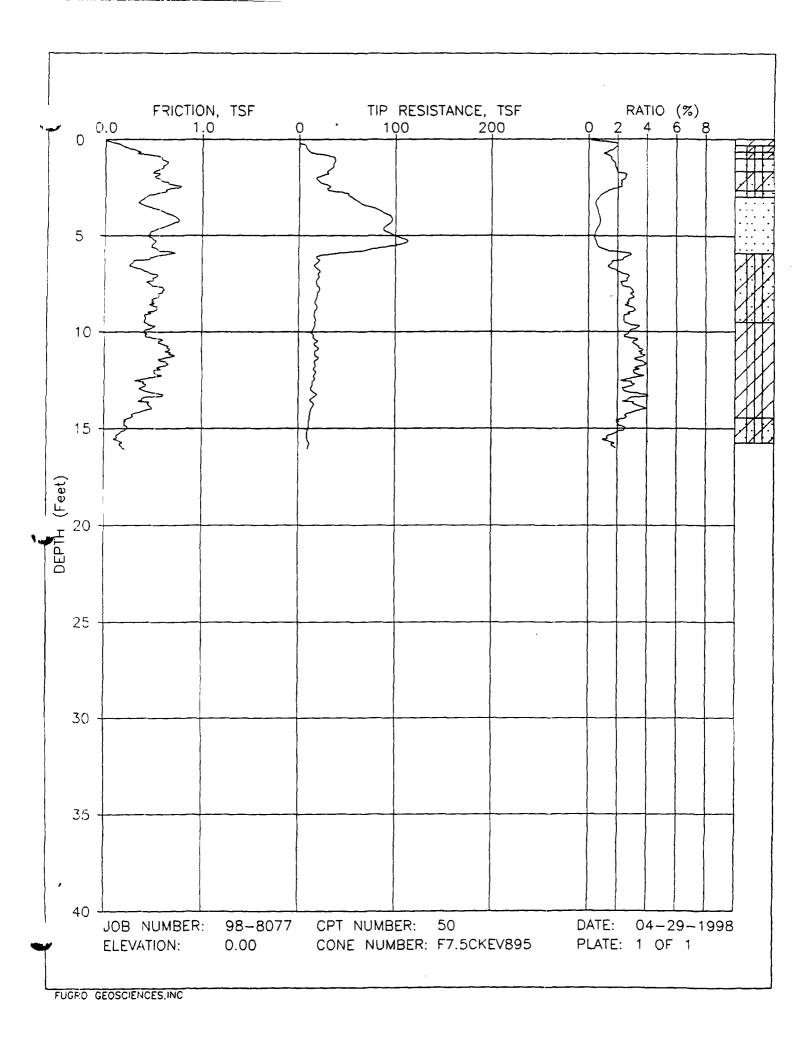


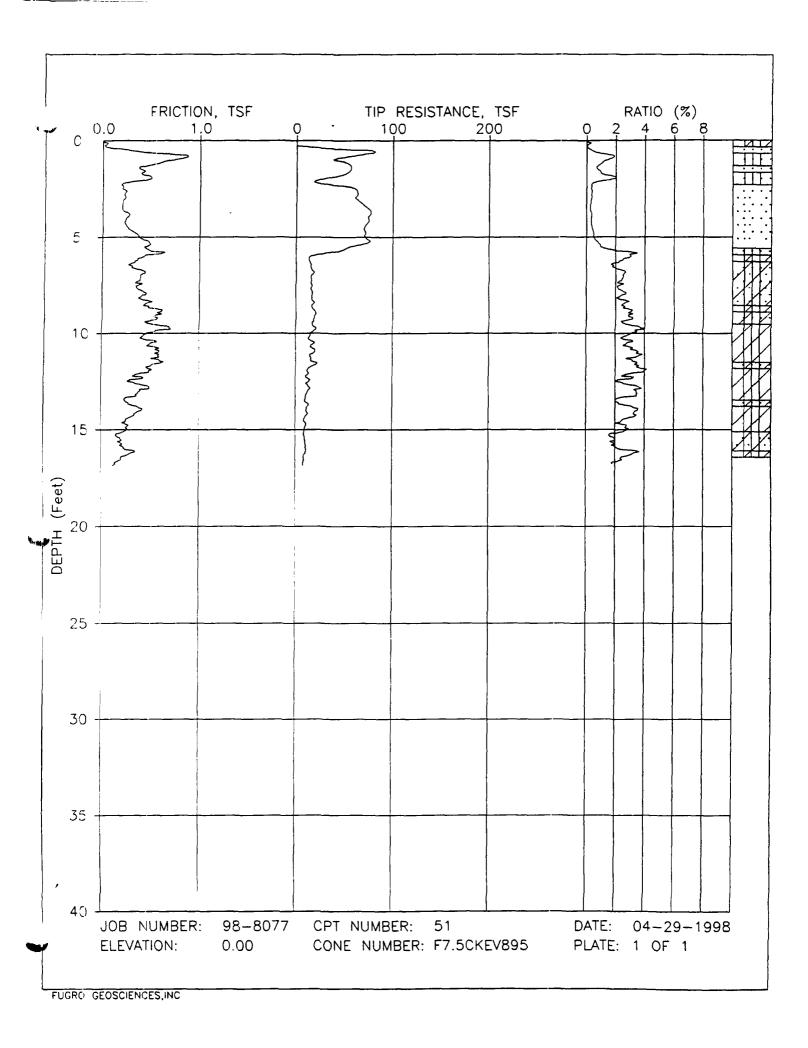


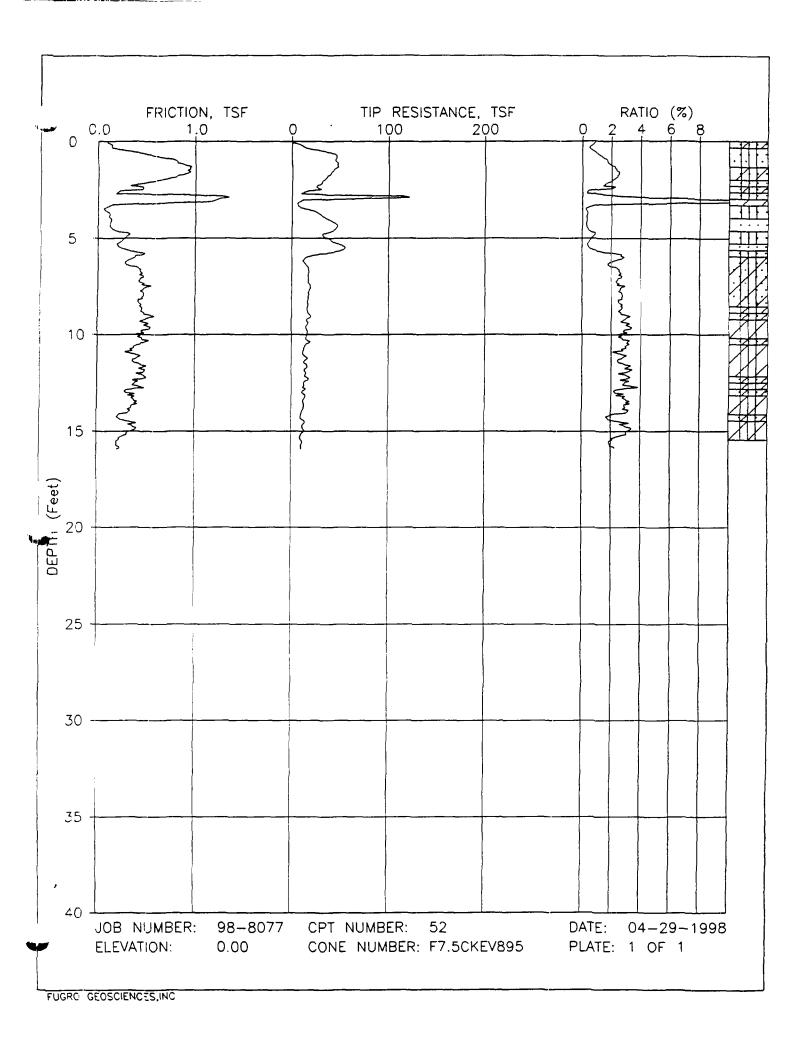


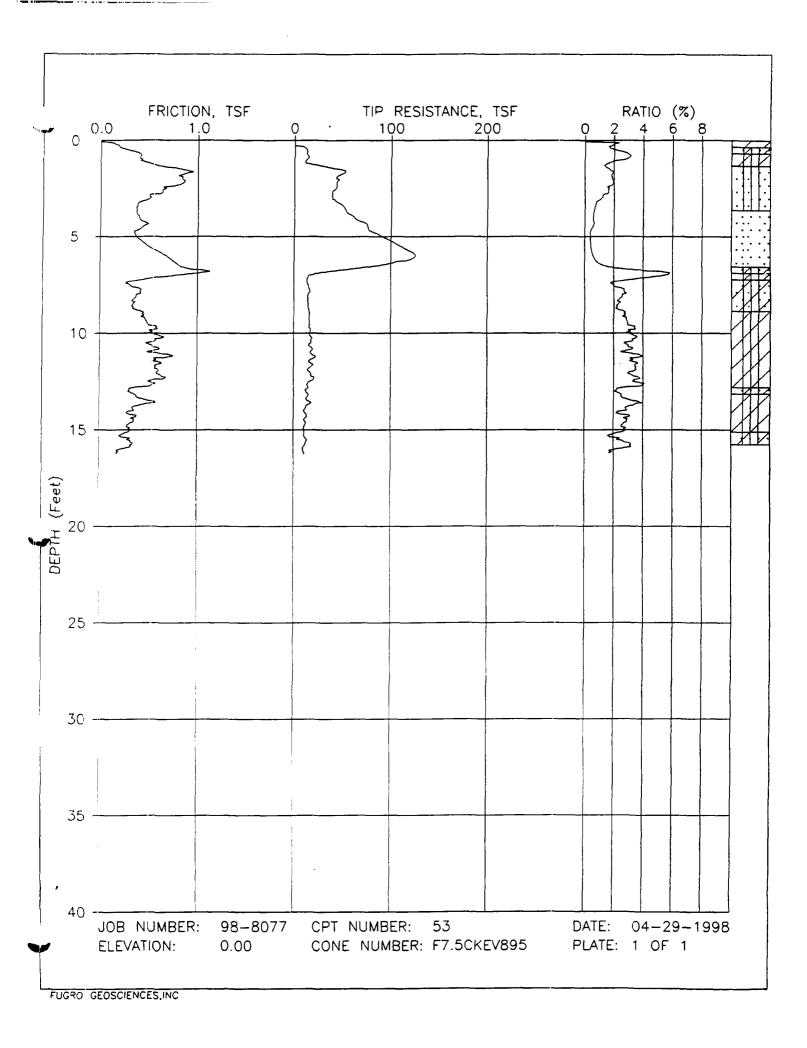


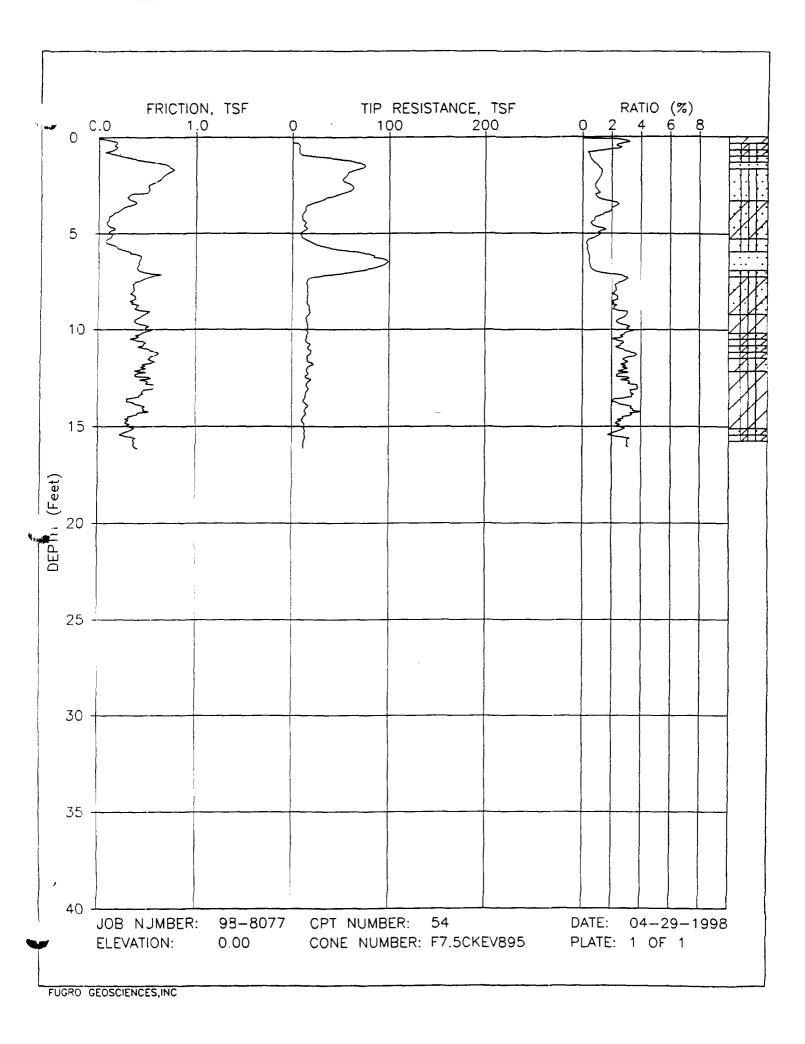


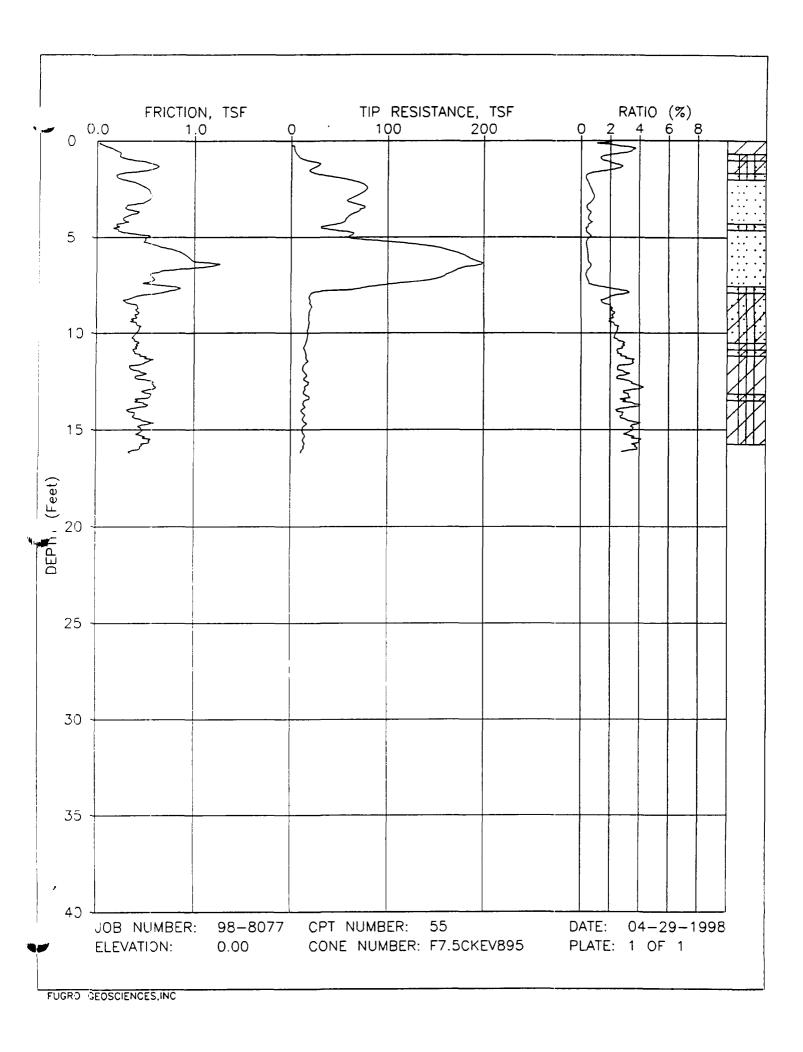


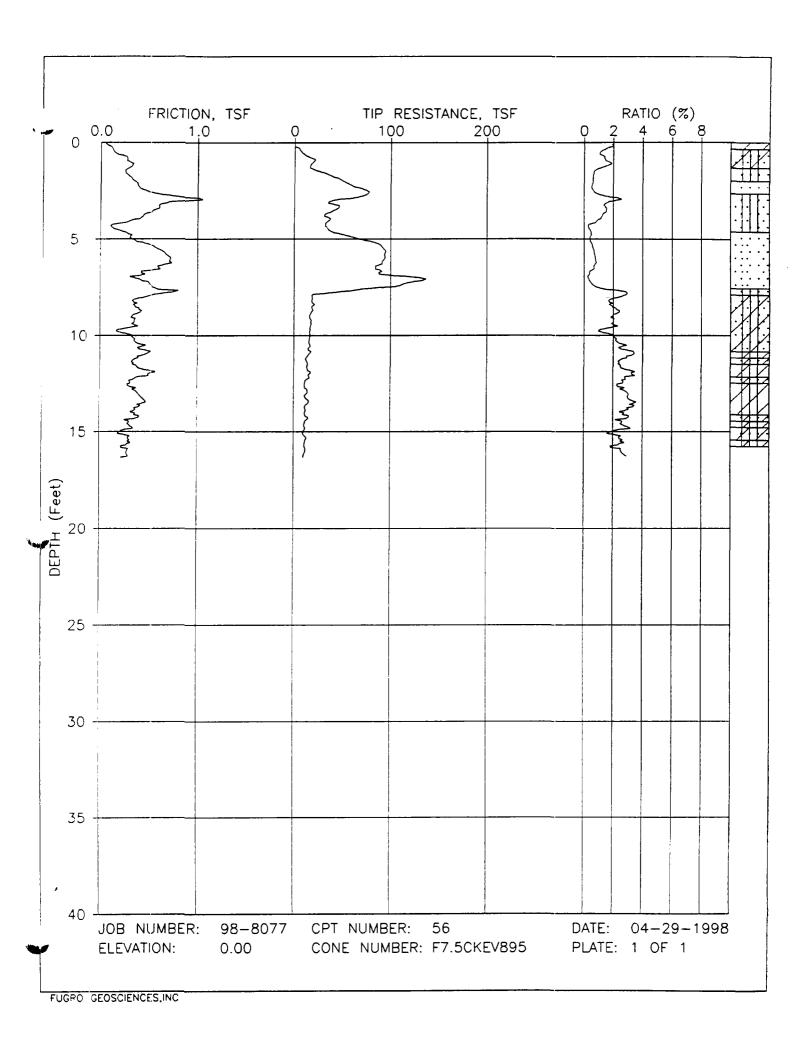


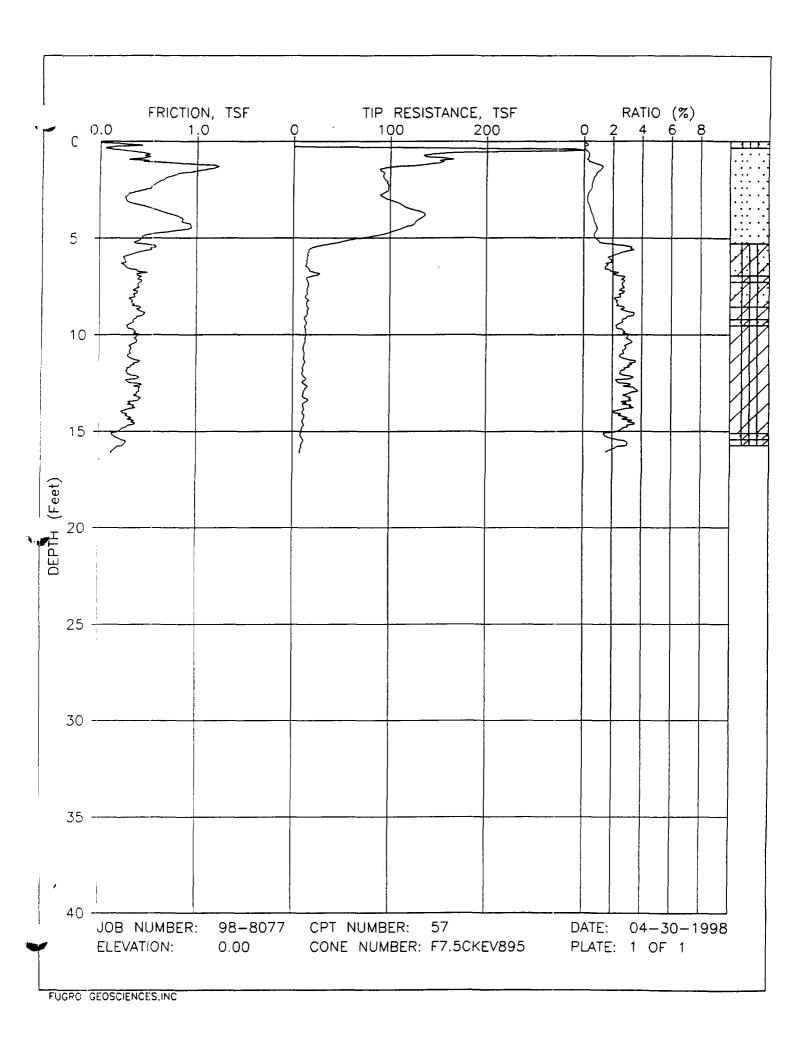


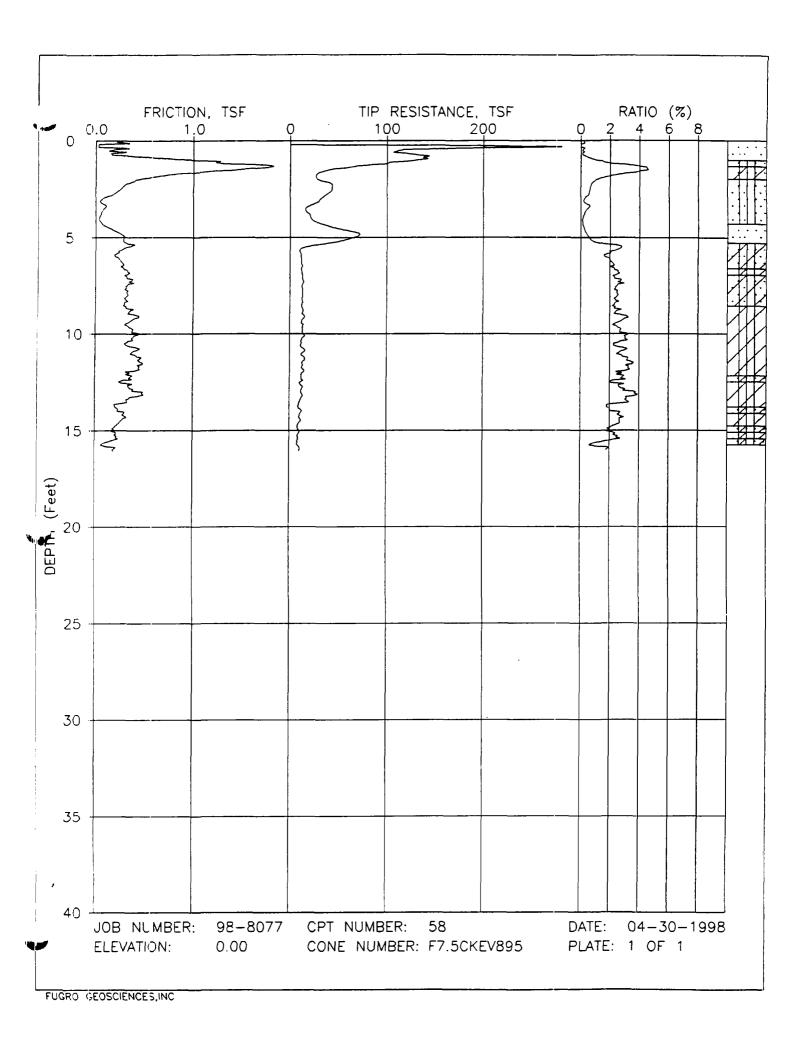


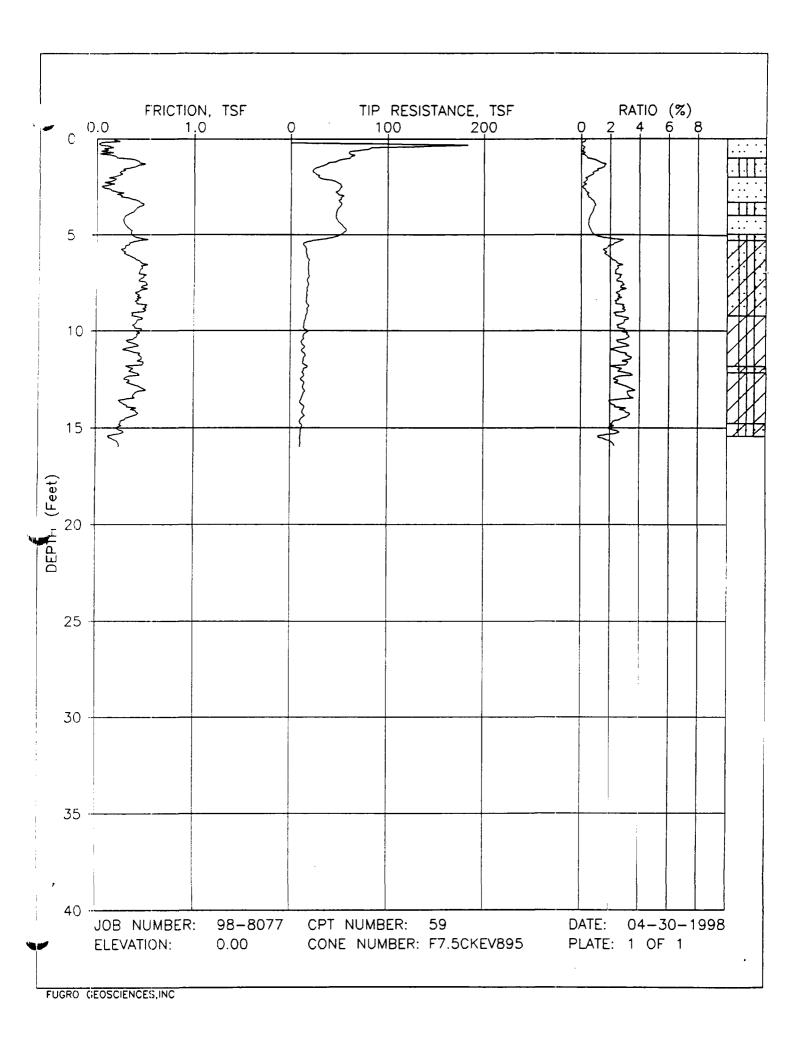


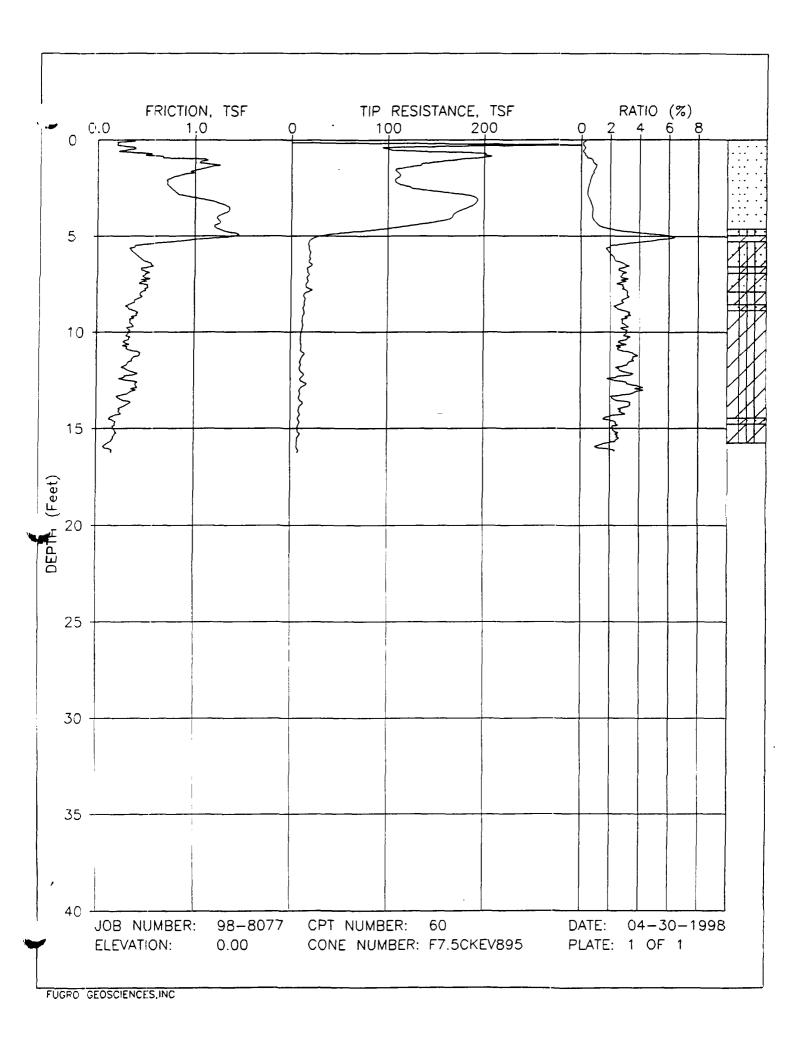


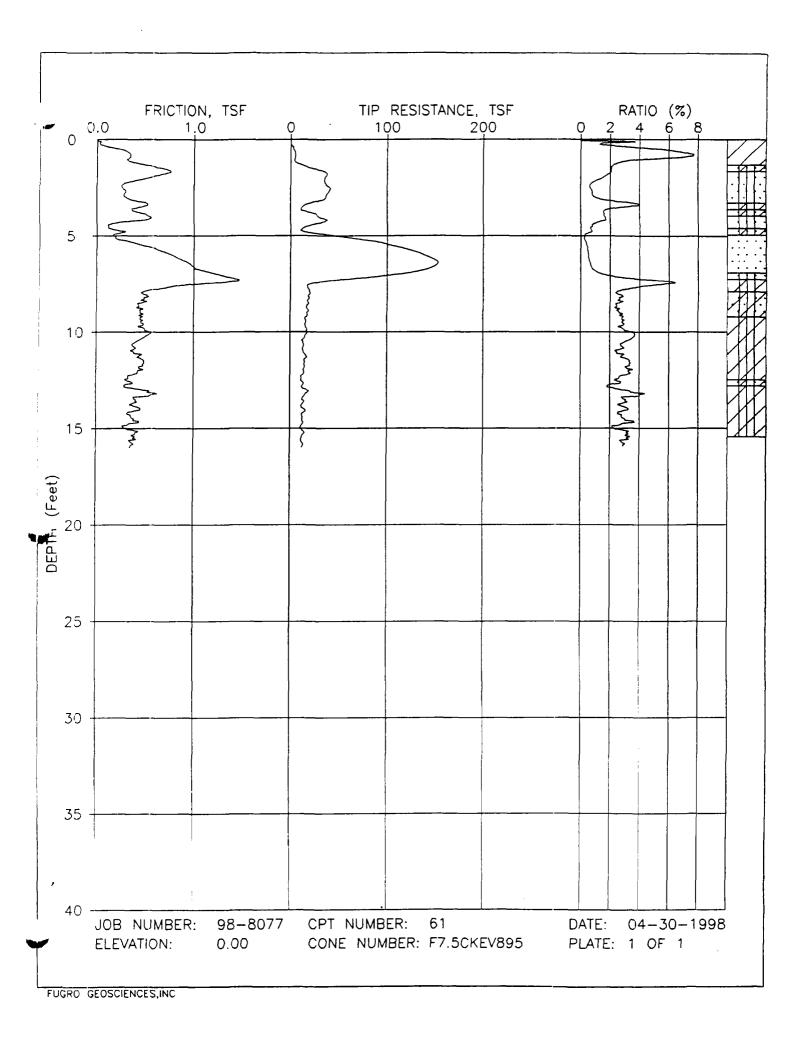


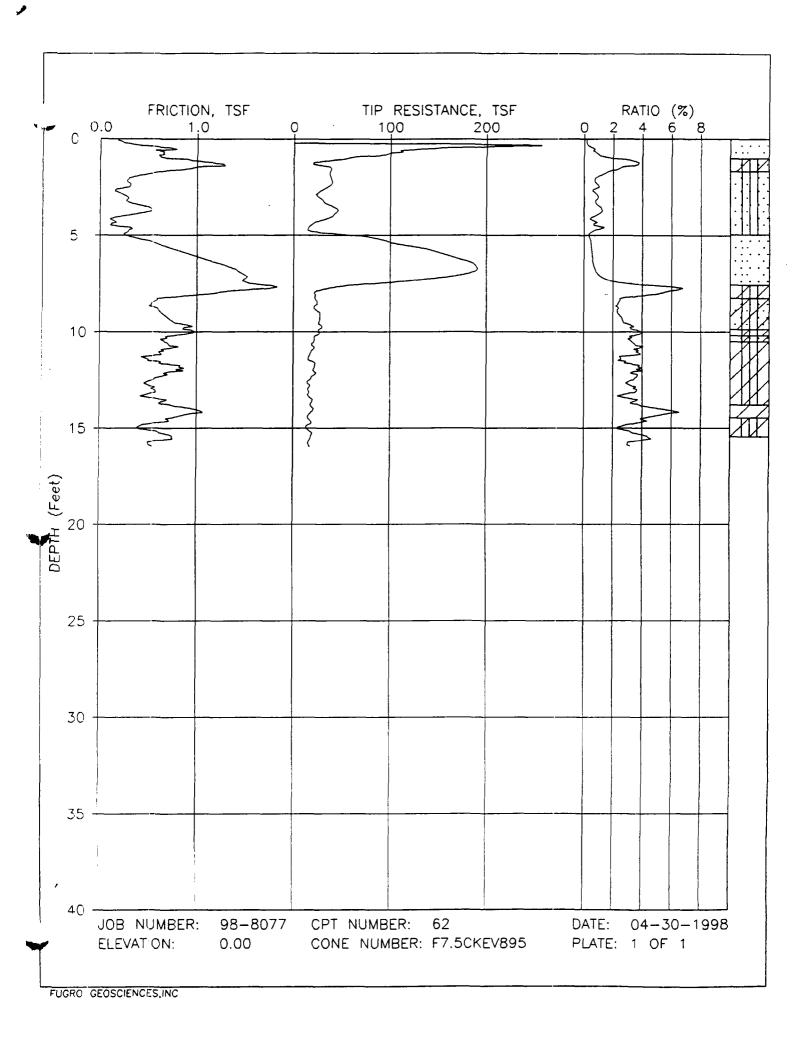


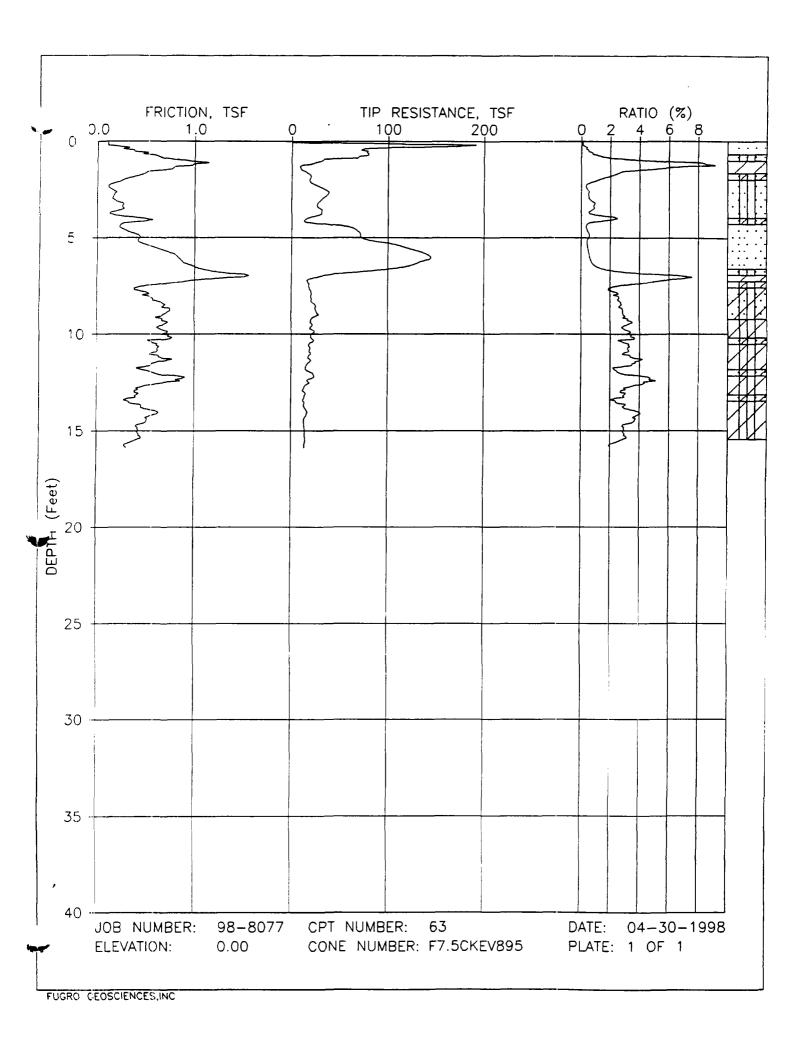


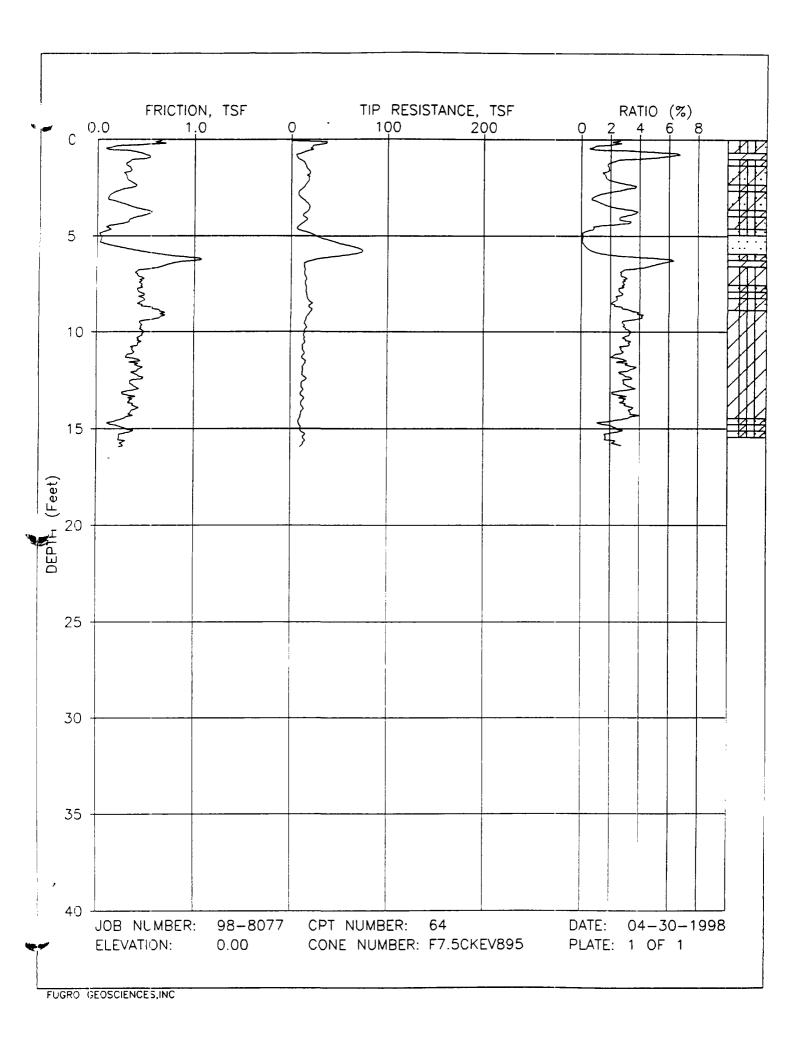


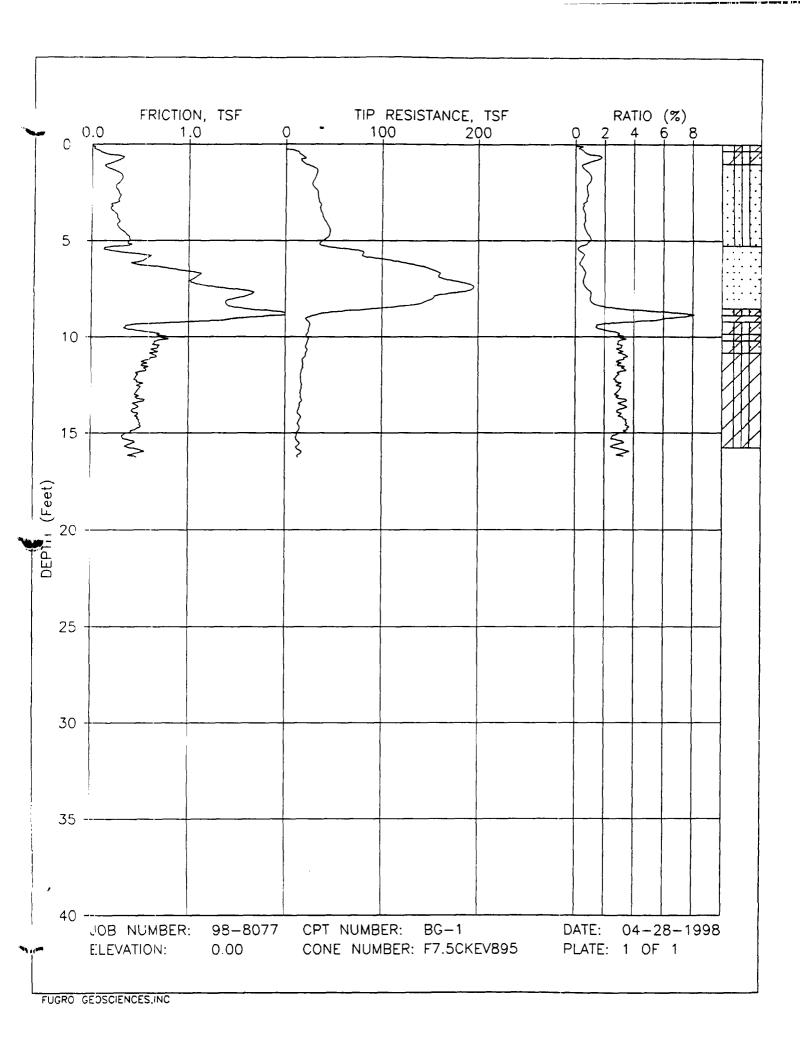












APPENDIX C

Geoprobe And Test Pit Logs

HULL & ASSOCIATES, INC. CIHO, ODEJOT

ODILL LOG	ł .	II.		SHEET NO. HOLE NUMBER
	Toledo Tie			1 of 1 SB-1
16	63448.09 / 7192	34.69 Jeff Arp		
Terra Probe	Geop	robe		BORING DIA. TOTAL DEPTH 2" 12
		GROUND ELEV. DEPTH/EL	EV. GROUND WATER 8.0	DEPTH/ELEV. TOP OF ROCK NA /
	CASING DIA/LENGT	H NOTES		1007
- T	NA	Corresponds to CP	i Boring BG-1	
(E LAYER Elev. Depth	DEPTH GRAPHIC LOG SAMPLE	density, grain size/shap composition, sorting,	pe, color, structure texture, moisture	DRILLING NOTES water levels, water return, character of drilling, etc.
NA 624.5	13354	- TOPSOIL.		
624.5 6/9.5 6/9.5 6/9.5 6/9.5 5.8	3- 3- 3- 3- 3- 4- 7- 8- 9- 10-	brown fine SAND: damp; Istaining (oxidation) & moi 3.0 ft. gray brown SILT: seam. brown fine SAND: loose; saturatedsame as above. dark gray CLAY: with silt, plastic.	heli fragments;	Sail samples PWM001- SB1- SS3-D385 collected from the 9,0-11.0 feet interval.
613.0_ 12.0	12	end of boring, 12.0 ft.		
	13-			
	DRILLER Terra Probe CORE BOXES SAMPLE O 3 BOCE tate liners NA 624.5 NA 624.5 NA 625 619.5 619	COORDINATES 1663448.09 / 7192: 1663448.09 / 7192: DRILLER Terra Probe Coordinates Geop Core Boxes Samples Casing Stickup NA Casing Dia/Lengti NA Casing Dia/Len	Toledo Tie COORDINATES 1663448.09 719234.69 Jeff Arp	DRILLER COORDINATES COOR

		ור סי) TI I 1	00	PROJEC	Ť		 	PROJECT NUMBER	SHEET	NO.	HOLE NUMBER
SITE	OLOG:	TO DE	JILL [Tole	do Tie		LOGGED BY	PWM001	1 of		SB-2
Toledo		. = = = -				99 / 7187		Jeff Arp				
BEGJN 5/3/98			RILLER Terra Pr	obe			EQUII	· · - · · · ·		BORI 2"	ING DIA	TOTAL DEPTH
3.4 / 6	COVERY (F	T./%)	CORE BOXES	S SAMPLE	S CASI NA	NG STICKU			H/ELEV. GROUND WAT E / A /	ER DEP		V. TOP OF ROCK
SAMPLE 1	TYPE			1	CASING	DIA/LENG	STH	NOTES				
4 1t. M	acro-co	I	etate line	rs	NA	T TT		Corresponds to	CPT Boring CPT-	27	1	
SAMPLE NUMBER	LENGTH/RECOV. (1eet)	BLOW COUNTS (8"-12"-8")	PID (mpq)	LAYER <i>Elev.</i> Depth	ОЕРТН	GRAPHIC LOG SAMPLE		density, grain size/ composition, sort facio	ND CLASSIFICATION shape, color, structing, texture, moistures, odor	ure e	,	LLING NOTES water levels, vater return, acter of drilling, etc.
MC-1/ SS-1	3.0/1.9	NA NA	NA	618.9_ 2.2 617.7_ 3.5_	1— 2—3—3—4—3—3—4—3—3—4—3—4—3—4—3—4—3—4—3—4—		bla co	nd & gravel. ack organic rich sei same as above; with ntent. ayey SAND	n increased sand		PWMO SS2- collec	amples OI-SB2- D385 Ited from the .5 feet ai.
		!			14							

		JI OC.	ור סו	OTI I I	00	PROJEC	T.	· · ·		F	PROJECT NUMBER	SH	HEET NO.	HOLE NUMBER
	SITE	OLOG:	IC Dr	JILL I		Tole	do Tie		LOGGED	BY	PWM001		of 1 KED BY	SB-3
_	Toledo				1		.79 / 7		.75 Jeff A					
	BEGUN 5/6/98		II	RILLER Terra Pr	ohe			ILL EQU Geopro	IIPMENT be				BORING DIA 2"	TOTAL DEPTH
		OVERY F		CORE BOXES		S CASI				D <u>E</u> PŢH/ <i>E</i>	LEV. GROUND WAT	ER I		V. TOP OF ROCK
	5.8 / 8 SAMPLE T		 -	0	2	NA	DIA/LE	NGTU	621.11 INOTES	¥ NA /	0//.i3		NA /	
		acro-cor	re w/ace	etate line		NA	, DIA/CE	.1401111		is to CF	T Boring CPT-	-39		
	SAMPLE NUMBER	LENGTH/RECOV. (feet)	(8"-12"-8")	PIO (mqq)	LAYER <i>Elev</i> . Depth	ОЕРТН	GRAPHIC LOG		density, grain	size/sha	CLASSIFICATION ape, color, struct tex:ure, maistur adar	ture		ILLING NOTES water levels, water return, acter of drilling, etc.
	MC-1/ SS-1	3.0/1.8	NA	NA NA	617.6 3.5 617.1 4.0 616.1 5.0 615.6 5.5	1— 2— 3— 4— 5— 6— 7— 8— 10— 11— 12— 13— 13—		₹	dark brown silty silghtly cohesive considerations. same as above brown/orange. CLAY. dark gray SILT: dark gray CLAY: slastic; cohesive cohesi	loose; s with silt	aturated. seams; damp; strine)	amp;	Soil s PWMO SS2- collect	amples DI- SB3- D385 ted from the .5 feet

GE	OLOG:	IC DI	RILL I	OG	PROJEC	T do Tie			PROJECT NUMBER	SHEET 1 of		OLE NUMBER
SITE					DRDINAT		-	LOGGED BY	1 111001	CHECKED		00 ,
Toledo		. ====		16	62167.		718774.	L		1000		I=0=
BEGUN 5/6/9		LETED 3/98	DRILLER Terra Pr	ohe		- 1	RILL EQ			2"	NG DIA	TOTAL DEPTH
	COVERY (F		CORE BOXE		S CASI				ELEV. GROUND WAT		TH/ELEV.	TOP OF ROCK
7.5 / 9			0	2	NA			GROUND ELEV. DEPTH/ 621.90 DEPTH/ V NR * NA	/	NA	/	_
SAMPLE	TYPE lacro-coi	re w/ac	atata lina	150	CASING NA	DIA/	LENGTH	NOTES Corresponds to 0	PDT Boring CDT_	5 7		
4 1 1			Tale inte	1 5	IVA	Ι.		Corresponds to C	or i boiling or i -	31	Т	
SAMPLE NUMBER	LENGTH/RECOV. (1eet)	BLOW COUNTS (8"-12"-8")	(mqq)	LAYER <i>Elev</i> . Depth	ОЕРТН	GRAPHIC LOG	SAMPLE	DESCRIPTION AND density, grain size/si composition, sorting facies	nape, color, struct g, tex:ure, moisturi	ure	W W	LING NOTES ater levels, ater return, octer of drilling, etc.
MC-1/ SS-1	4.0/3.5	NA	NA	<i>621.7</i>	_	•••		ASPHALT: with under la	ymen: loose grave	el.		
55**1				621.3_	1— 2—			brown fine SANO: with :	some silt; loose; da	emp.		
					3— -			same as above; beco moist; slight chemical o				
MC-2/ SS-2	4.0/4.0	AM	NA 		4— 5—			same as above; beco strong sheen.	mes coarser sand;		SS2- I collect 4.0-8.	I—SB4- D385 ed from the O feet
	j			616.4	+						interva	ıl.
				616.4 5.5				gray SILT saturated; lo	oose to slightly			
	į			<i>615.9</i> 6.0	6-	//		cohesive.	ne: damp: plastic:		i	
							``	dark gray CLAY: with file cohesive; (lacustrine).	ne, demp, plastie,			
					7_		Ħ					
					_ ′		1					
					1							
				<i>613.9</i> 8.0	8-		-	end of baring, 8.0 ft.				
					1		į					
					<u> </u>	ľ						
					9							
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					10-							
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					11—							
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	:				13-							
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	-				14							

	GE	OLOG:	IC DF	RILLI	_OG	PROJEC	T do Tie				PROJECT NUMBER PWMOO1	SHEE 1 o		HOLÉ NUMBER SB-5
	SITE				cod	ORDINAT	ES		LOGGED		1 MP1001	CHECKE		
,	Toledo BEGUN		LETED C	RILLER	16	62057	.92 / 7	18831.3 ILL EQU		rp		IBO	RING DIA	TOTAL DEPTH
	5/5/98	5/6	/98	Terra Pr			G	eoprol	be			2		9
	8.0 / 8	OVERY (F	T./%)	CORE BOXES	S SAMPLE	S CASI	NG STIC	KUP	GROUND ELEV. 1	DEPTH/A	FLEV. GROUND WAT	ER DE	PTH/ <i>ELE</i> A /	V. TOP OF ROCK
	SAMP_E T	YPE		<u> </u>		CASING	DIA/LE		NOTES					
	4 ft. M	acro-coi	Г	etate line	ers	NA	,		Correspond	le to C	PT Boring CPT-	-4		
	SAMPLE	LENGTH/RECOV. (feet)	BLOW COUNTS (8"-12"-8")	OIA (mdd)	LAYER <i>Elev.</i> Depth	ОЕРТН	GRAPHIC LOG		density, grain	size/sh	CLASSIFICATION ape, color, struct , texture, maisturi odor	ure	,	LLING NOTES water levels, vater return, acter of drilling, etc.
	MC-1/ SS-1	4.0/3.5	NA	NA	618.9 2.0	1— - - - - 2—			cohesive; roots.		ndy (CLAY: damp;			
	MC-2/ SS-2	1.0/1.0	NA	NA	2.0	3-4-		Ç	dark gray/black gravel; damp; loc	silty S .	AND: with sparse lightly cohesive.			
	MC-23/ SS-2	4.0/3.5	NA	NA		5			.same as above	, stranç	g odor and sheen.		PWMO SS2- collec	amples 01–SB5– D385 sted from the .0 feet al.
					613.9 7.0	7-		р	ark gray CLAY: lastic; sheen an oper portion of	d pradi	t seams; damp; uct in silt seams in	1		
					611.9 9.0	9-1		—— е	nd of boring, 9.	o ft.				
						11								
						12-								
	i					13-								

	01.00	דר סי) TI I I	00	PROJEC	T -			PROJECT NUMBER	SHEET		OLE NUMBER
SITE:	OLOG:	TO DE	ITLL [Toled	do Tie		LOGGED BY	PWM001	1 of		SB-6
Toledo				1		.27 / 7	18605.	06 Jeff Arp				
BEGUN 5/6/98		- 1	RILLER Terra Pr	obe			ILL EQU Seoprol			BORI 2"	NG DIA	TOTAL DEPTH 8.0
CORE RE	COVERY (F		CORE BOXE	S SAMPLE				GROUND ELEV. DEPTH	/ELEV. GROUND WATE / 617.7			TOP OF ROCK
NR / N			0	2	NA CASING	DIA/LE	NGTH	623.69 # N/	<u> </u>	NA		
	lacro-coi	re w/ace	tate line	ers	NA	T T			CPT Boring CPT-	31		
SAMPLE NUMBER	LENGTH/RECOV. (feet)	BLOW COUNTS (8"-12"-8")	PIO (mdd)	LAYER <i>Elev</i> . Depth	ОЕРТН	GRAPHIC LOG	SAMILE	density, grain size/s composition, sorti	D CLASSIFICATION shape, color, structu ng, texture, moisture s, odor	ıre	W	LING NOTES ater levels, ater return, cter of drilling, etc.
MC1/ SS-1	4.0/NR	NA	NA		-	7575		ropsoil: maist-wet.				
				622.7_ 1.0	1— 2— 3—			orown fine SAND: with lamp.	trace silt; loose;			
MC-2/ SS-2	4.0/NR	NA	NA	619-2- 4-5 618-7- 5.0	5 - 4		р s р	.same as above; wet. rown silty CLAY: with off to firm; cohesive. rown fine SAND: wetsame as above; gray				
				616.2- 615.7- 8.0-	7		d	ark gray CLAY: with s			SS2- C collect 8.0-7.6 interva Acetat stuck Ir sampler redrilled	I-SB8- 1385 ed from the 5 feet 1. e tube n macro , offset & d. Field aken @ this
					13-							

GEO	LOG]	C DR	RILL			do Tie	 		PROJECT NUMB	1	SHEET NO. HOLE NUMBER
SITE Toledo, 1	———— ОН				RDINAT 62069.	ES .74 / 718		LOGGED B Jeff Ar		CHE	ECKED BY
BEGUN 5/6/98	CO⊬PL 5/6	/98	RILLER Terra Pr			Geo	EQUIPMENT probe		·		BORING DIA. TOTAL DEP
9.8 / 98		T./%}	CORE BOXES	S SAMPLE 3	NA	NG STICKU	623.98		PTH/ <i>ELEV</i> . GROUND 7 5 / 619.0 7 NA /	WATER	DEPTH/ELEV. TOP OF ROO NA /
SAMPLE TYP 4 ft. Mac		e w/ace	tate line	!rs	CASING NA	DIA/LENG	l l		to CPT Boring CF	T-56	
SAMPLE	LENGTH/RECOV. (feet)	BLOW COUNTS (8"-12"-8")	PIO (mdd)	LAYER <i>Elev</i> . Depth	ОЕРТН	GRAPHIC LOG SAMPLE	density	y, grain si position, s	N AND CLASSIFICAT ize/shape, color, str sorting, texture, mois acies, odor	ructure	DRILLING NOTE water levels, water return, character of drillii etc.
MC-1/ 4 SS-1	4.0/4.C	NA	NA	623.5_ .5	1—	;;;; ;;;;	— dark org Ioose-sli	anic rich ghtly coh	TOPSOIL: sand & si lesive; damp.	lt;	
				620.3 3.7	2-				AND: with silt.		
MC-2/ SS-2 4	1.0/3.8	NA	NA	619.0_ 5.0	4— 5— 6—	<u></u>	gray fine	ohesive.	ine SAND : li:tle clay	; maist;	
MC-3/ SS-3	.0/3.5	NA	NA		7— 8— 9—		— Strong od — sand coa odor and	rsens wit	heen h shell fragments; sl	trang	Soil samples PWM001- SB7- SS2-D385 collected from the 7.0-9.5 feet interval.
				614.5 9.5 614.0 10.0	10-11-12-		dark gray — end of bo		ith silt; (lacustrine).) ft.		
					13-						

	GE	OLOG:	IC DF	RILL	_OG	PROJEC	ct do Tie				PROJECT NUMBER PWM001	SHEE 1 of	T NO.	HOLE NUMBER SB-8
	SITE					ORDINAT			LOGGED			CHECKE	DBY	<u></u>
,	Toledo				16	61925.				Arp		1		
	BEGUN 5/6/98	I		RILLER Terra Pr	obo			RILL EQU Geopro	JIPMENT			BO 2'	RING DI	A. TOTAL DEPTH
		COVERY (F		CORE BOXES		SICAST				DEPTH/	FIEV GROUND WAT			EV. TOP OF ROCK
	6.3 / 7		,,	0	2	NA		,-	622.38	▼ 4 / ▼ NA	ELEV. GROUND WAT 618.4 /	N	A /	
	SAMPLE T					E .	DIA/LE	ENGTH	NOTES					
	4 ft. M	acro-cor	e w/ace	etate line	rs	NA	, ,	1	Correspon	ds to C	PT Boring CPT-	-48		· · · · · · · · · · · · · · · · · · ·
	SAMPLE NUMBER	LENGTH/RECOV. (feet)	BLOW COUNTS (8"-12"-8")	PIO (mdd)	LAYER Elev. Depth	НТӨЗО	GRAPHIC LOG	SAMPLE	density, grain	size/sh	CLASSIFICATION nape, color, struct g, texture, moistur g, odor	ture		RILLING NOTES water levels, water return, eracter of drilling, etc.
	MC- / SS-1	4.0/2.3	NA	NA					dark black sand	dy SILT:	damp; loose to			
	25-1					-		}	slightly cohesiv	e, siignt	ly plastic.			
				<u> </u>	<i>621.4</i> _1.0	1					ist silty CLAY: wit slightly plastic; F]			
						3								
	MC-2/ SS-2	4.0/4.0	NA	NA	<i>618.4</i> 4.0	4					ine to medium SA l	VD :		samples 001- SB8-
,						5-		1	oose; wet; stro	ng adar	and sheen.		SS2- colle	-D385 ected from the 8.5 feet
					615.9_ 6.5	7—		l la	lark gray CLAY aminates; very acustrine.	: with sil thin fine	t; damp; plastic gray sand seams	s;	-	
1						}		10	acustrine.					
					614.4_ 8.0	8- -		е	end of boring, 8	.0 ft.				
						9-								
						10-								
					i	, - ,, -								·
						11—								
						12-								į
						13-								
						1								

GE	OLOG:	IC DF	RILL I	OG	PROJECT		PROJECT NUMBER PWM001	SHEET 1 of 1	
SITE Toleido					DRDINATE		LOGGED BY CH	ECKED	
BEGUN 5/6/98 CORE REC 7.6 / 9	COMPI 3 5/8 COVERY (F	/98	Terra Pr CORE BOXES	obe	, ,,,,	DRILL	EQUIPMENT probe P GROUND ELEV. DEPTH/ELEV. GROUND WATER \$\frac{\gamma}{\gamma} \text{ NR / } \frac{\gamma}{\gamma} \text{ NA / }	2"	NG DIA. TOTAL DEPTH 8 H/ELEV. TOP OF ROCK
SAMPLE T 4 ft. M	YPE acro-ccr	re w/ace	etate line	rs	CASING NA	DIA/LENG	TH NOTES Corresponds to CPT Boring CPT-16		
SAMPLE	LENGTH/RECOV. (teet)	BLOW COUNTS (8"-12"-8")	OId (mdd)	LAYER <i>Elev</i> . Depth	ОЕРТН	GRAPHIC LOG SAMPLE	DESCRIPTION AND CLASSIFICATION density, grain size/shape, color, structure composition, sorting, texture, moisture tacles, odor		DRILLING NOTES water levels, water return, character of drilling, etc.
MC-1/ SS-I	4.0/3.8	NA	NA		_			_	
				618.9 2.0	2-		dark brown silty CLAY: with sand light brown fine SAND: little silt; damp to moist; slightly cohesive		
MC-2/ SS-2	4.0/4.0	N A	NA	<i>615.9_</i> 5.0	5 6		gray CLAY: laminated w/ silt & fine sand seams — seams possess odor and staining; damp; firm to soft (lacustrine).		
				612.9 8.0	7 - 1 8 - 1 9 - 1		— end of boring, 8.0 ft.		Sail samples PWM001-SB9- SS2- D385 collected from the 4.5-8.0 feet interval.
					10-				

G	EOLOG	GIC D	RILL !	_OG	PROJEC	t do Tie	<u> </u>		PROJECT NUMBE	R SHEET		LE NUMBER
SITE				COC	RDINAT	ES	,	OGGED BY	1	CHECKED		
Tol:	edo, OH	PLETED	DRILLER	16	62081.		3864.89	Jeff Arp		IBORI	ING DIA.	TOTAL DEPTH
5/6	/98 5/	6/98	Terra Pr			Ge	eoprobe			2"	1	8
CORE 7 /	RECOVERY	(FT./%)	CORE BOXE	S SAMPLE	S CASII NA	NG STICK	(UP GROUND E 621.97	LEV. DEPTH	/ELEV. GROUND W	ATER DEP		OP OF ROCK
	E TYPE		1			DIA/LEN	GTH NOTES		·		,	
4 f	. Macro-c	ore w/ac	etate line	ers	NA_		Corre	sponds to	CPT Floring CPT	T-58		
SAMPLE	E	BLOW COUNTS (6"-12"-6")	DIA (mdd)	LAYER Elev. Depth	ОЕРТН	GRAPHIC LOG SAMPLE	density, compo	, grain size/s osition, sortin facie	D CLASSIFICATI Shape, color, stru ng, texture, maist s, adar	cture ure	wat	ING NOTES ter levels, er return, ter of drilling, etc.
MC- SS-		NA NA	NA	620.0_ 2.0	1		material; l	aose ta sligh	ich) SILT: with ro htly cchesive			
MC-2 SS-		NA	NA		3 4		same as	above.	(Free Product)		Soil sam PWM001- SS2- Di collecte 4.0-8.0 interval.	SB10- 385 d from the feet
				<i>616.0</i> _ 6.0	6		Dark gray (thin);	CLAY: with s	silt and sand sea	ms		
				6/4.0_ 8.0	9 10 11 12 13 13		end af bai	ring, 8.0 ft.				

GE	ol og	TC DE	RILL L	OG	PROJEC	T do Tie					PROJECT NUMBER PWMOO1		HEET N	10.	HOLE NUMBER TP-1
SITE				COC	ORDINA	res]	LOGGED		1 1111001		CKED BY	Ϋ́	11 1
Toledo BEGUN		LETED [DRILLER	16	82345		718986. RILL EQU		Jeff /	Arp		<u> </u>	BORING	G DIA	TOTAL DEPTH
5/7/98	3 5/7	/98	Heritage				Backhoe	•		r=====			PIT		7.6
NA / N	OVERY (F	T./%)	CORE BOXES	SAMPLE O	S CASI NA		CKUP (621.23	ELEV.	DEPTH/	ELEV. GROUND WAT / /	EK	NA /		. TOP OF ROCK
SAMPLE T	YPE IDE BUCI	KFT			CASING	DIA/L	ENGTH	NOTE:	3		CPT Boring CPT~				
					17/	(0)		1 00	СБРОП	00 10 0	, r Bonnig Gr 1				
SAMPLE	LENGTH/RECOV. (feet)	BLOW COUNTS (8"-12"-8")	PIO (mdd)	LAYER <i>El</i> ev. Depth	ОЕРТН	GRAPHIC LOG	SAMPLE				CLASSIFICATION nape, color, struct g, texture, moisture , odor			٠ س	LLING NOTES water levels, water return, acter of drilling, etc.
	LENG	B) B)		6/3.6_ 7.6	1	040	da	and; be	y CLAY	and oran	ige sity CLAY : wit itled with depth	h	i i	odors obser Very I enteri excav	etectable or staining ved little water ng ation ated al returned per EPA
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		PROJECT		PROJECT NUMBER	SHEET I	NO IDA	LE NUMBER
GEOLOGIC E	RILL LOG	Toledo Tie		PWMOO1	1 of 1	NO. 12	TP-2
SITE		ORDINATES	LOGGED BY		CHECKED E		
Toledo, OH	11	862237.25 / 719097	.28 Jeff Arp				
BEGUN COMPLETED	DRILLER	DRILL EQ			II	IG DIA.	TOTAL DEPTH
5/7/98 5/7/98 CORIE RECOVERY (FT./%)	Heritage CORE BOXES SAMPLE	Backho		FIFY GROUND WATE	PIT R DEPTH	1/F/FV 1	9.6 FOP OF ROCK
NA / NA	0 0	NA NA	GROUND ELEV. DEPTHA 621.00 Y NA	7	NA A		. S. SI HOUN
SAMPLE TYPE		CASING DIA/LENGTH	NOTES				
2 ft. WIDE BUCKET	 	NA	Corresponds to 0	CPT Boring CPT-	38		
SAMPLE NUMBER LENGTH/RECOV. (feet) BLOW COUNTS (6"-[2"-8")	(E) LAYER Elev. Depth	DEPTH GRAPHIC LOG SAMPLE	density, grain size/s composition, sortin	OCLASSIFICATION hape color, structu g, texture, moisture s, odor		wa wat	ING NOTES ter levels, ter return, ter of drilling, etc.
	0100		dark brown silty CLAY:	with sand			
	619.0	_!/ /	mottled brown/orange/ plastic (very weathers	gray silty CLAY: da ed lacustrine depos	amp; Ht)		
	616.0_ 5.0	5	pecames brown (water of Interface)	flowng into hole o	ut		
	ક્ષ્મું કુ	8 9	small sand seam				ant amount rentering
	611.4_ 9.8_	10-	BASE OF PIT			Excavati material to Pit pe approval	returned er EPA
		13-					

GEO	OGIC [DRILL I	_OG	PROJEC	T do Tie	•			PROJECT NUMBER PWMOO1		HEET NO.	HOLE NUMBER
SITE			CO	ORDINAT	ES	 -	LOGGE		T WHOO!		CKED BY	
Toledo, (OH COMPLETED	DRILLER	16	62074	.56 / 7		.87 Jeff UIPMENT	Arp			BORING DI	A. TOTAL DEPTH
5/7/98	5/7/98	Heritage				ackho					PIT	6.0
	/ERY (FT./%)	Y (FT./%) CORE BOXES SAMPLES CASIN			NG STIC	KUP	GROUND ELEV	DEPTH/	ELEV. GROUND WAT / /	ER		V. TOP OF ROCK
NA / NA SAMPLE TYP	E	0	0	CASING	DIA/LE	NGTH	621.51 NOTES	♥ NA	<u>/</u>		NA /	
2 ft. WID	E BUCKET		_	NA			Correspo	nds to C	PT Boring CPT-	35		
SAMPLE	LENGTH/RECOV. (feet) BLOW COUNTS (8"-12"-8")	PIO (mqq)	LAYER <i>Elev</i> . Depth	ОЕРТН	GRAPHIC LOG				CLASSIFICATION nape, color, structo g, tex:ure, moisture , odor			RILLING NOTES water levels, water return, eracter of drilling, etc.
			620.0 1.5	1			dark brown cl		T: Dry ge slity SAND :			
			618.5_ 3.0 618.0_ 3.5	3— 4—		ı	brown fine SA mattled brown to molst		slit; <u>wet</u> y CLAY : plastic; da	amp		
			<i>615.5_</i> 6.0	5— 6— 7—		E	BASE OF PIT				exca mate	etectable or staining wated itals returned t per EPA oval
				9-								
:				11-								

GEO	OLOG		RILL	OG	PROJEC	T Jo Tie				PROJECT NUMBER PWMOO1		EET NO. of 1	HOLE NUMBER
SITE				COC	RDINAT	ES		LOGGE		1		KED BY	
Toledo BEGLN		ETED	DRILLER	16	82047	.84 / 7).13 Jeff JIPMENT	Arp			BORING DI	A. TOTAL DEPTH
5/7/98	E		Heritage	!			ackho	e				PIT	5.3
	OVERY (F	(FT./%) CORE BOXES SAMPLES CASING STICKUP			KUP	GROUND ELEV.	DEPTH/	VELEV. GROUND WATE / /	ER (DEPTH/ <i>ELL</i> NA /	EV. TOP OF ROCK		
NA / N SAMPLE T			0	0	NA CASING	DIA/LE	NGTH	NOTES	<u>Y</u> NA	<i></i>		INA /	
2 ft. W.	IDE BUCK	KET		,	NA	,	,	Correspon	ds to (CPT Foring CPT-	33	···	
SAMPLE	LENGTH/RECOV. (feet)	BLOW COUNTS (6"-12"-6")	PIO (mpq)	LAYER <i>Elev</i> . Depth	ОЕРТН	GRAPHIC LOG		DESCRIPTI density, grain composition	ı size/si ı, sortin	DCLASSIFICATION hape, color, structi g, texture, maisture s, odar	ure e		RILLING NOTES water levels, water return, aracter of drilling, etc.
				620.0_	- - 1—			cohesive; damp		T: with clay; slightly	/		
				1.2	2-			mottled silty SA	KNU:				
	i		;	<i>618.5</i> 2.5	_								
	ļ		į.	618.0_ 3.0	3			dark gray (sta	ined) S/	AND: Wet			
			i	3.0	-		:	silty SAND:				PID	/FID air
	İ			617.0_ 4.0	4							read	dings range 18.3 to 9.4
	1			4.0	4		t	prown and gray	slity C	LAY: damp; plastic		bbu	
				615.7_ 5.3	5— 6—		E	BASE OF PIT				mate to P	avated erials returned ilt per EPA roval
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					PROJEC	T			-		PROJECT NUMBER	To	HEET NO		IOLE NUMBER
GE	OLOG	IC DI	RILL L	_OG		do Tie					PWMOO1		1 of 1		TP-5
SITE					ORDINA	TES			LOGGED		<u> </u>		CKED BY		
Toledo				16	361925.	58 / 7			Jeff	Arp					·
BEGUN 5/7/98	,	LETED 7/98	DRILLER Heritage			•	iill EQU Backho	JIPMENT					BORING	DIA.	TOTAL DEPTH
	COVERY		CORE BOXES		S CASI			GROUND	ELEV.	DEPTH/	ELEV. GROUND WAT	ER	1	LEV.	TOP OF ROCK
NA / N			0	0	NA			622.3	8	V NA	ELEV. GROUND WAT / /		NA /		
SAMPLE 1	TYPE IDE BUC	VET			1	DIA/LE	ENGTH	NOTE	S		PT Boring CPT-				
2 11. N	T	1	<u> </u>		NA	1 1	T	COL	езроп	ds 10 C	art Bolling Cri-	40		····	<u> </u>
SAMPLE NUMBER	LENGTH/RECOV. (feet)	BLOW COUNTS (8"-12"-8")	PID (mpq)	LAYER <i>Elev</i> . Depth	DEPTH	GRAPHIC LOG	a and a second	densit	y, grain	size/sh	CLASSIFICATION lape, color, struct g, texture, moisture , odor	ure		W Wa	LING NOTES ater levels, ater return, cter of drilling, etc.
					-		<u> </u>	ight bro	ıwn fine	SAND					
				<i>621.4</i> _1.0	1_						·····				
				1.0	-			dark bro clay; co	own to (hesive	gray mot	tled slity SAND : w	ilth			
		1			-										
					2-								ł		
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					-										
				200.4	_									lainin	g @ 3.9 to
				618.4 4.0	4		ā	ppraxin	nately 3	inch se	am (creosote rich	h)		o te	
					-										roduct into Pit Jar
			:		5—								at	soils	s and
					-		i						pr	oduc	t taken
					_								1		
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<u> </u>				615.9 6.5	7	77			M. /I o	custrine)	 				
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				614.9 1.5	1		B	IASE OF	PII				ma	icava Iteria	als returned
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GEO	OLOG	IC D	RILL L	OG	PROJEC	T do Tie	_ 		PROJECT NUMBER		EET NO. of 1	HOLE NUMBER
SITE				CO	ORDINAT	ES	710720 01	LOGGED BY	1		ED BY	<u> </u>
Toledo BEGUN		LETED	DRILLER	16	882069		718730.01	Jeff Arp		l la	ORING DIA	TOTAL DEPTH
5/7/98	5/7	7/98	Heritage			<u> </u>	Backhoe				PIT	7.5
CORE REC	COVERY IF	FT./%}	CORE BOXES	SAMPLE	S CASI	NG STIC	CKUP GROUND 622.3	ELEV. DEPTH	/ <i>ELEV</i> . GROUND WATI / /	ER D	EPTH/ <i>ELE</i> NA /	V. TOP OF ROCK
SAMPLE T	YPE				CASING	DIA/LE	NGTH NOTE	S			7	
2 ft. W	IDE BUC	1	т	ſ	NA	1 1	Cor	responds to	CPT Boring CPT-	56		
SAMPLE NUMBER	LENGTH/RECOV. (feet)	BLOW COUNTS (8"-12"-8")	(wdd)	LAYER <i>Elev</i> . Depth	ОЕРТН	GRAPHIC LOG	densit	y, grain size/s position, sortin	D CLASSIFICATION hape, color, structi ng, texture, moisture s, odor	ure		ILLING NOTES water levels, water return, iracter of drilling, etc.
				<i>621.4</i> 1.0	- - 1_		with dep	oth ———————	SAND: gades to lig	hter		
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					2-							
					3 <u> </u>							
	;			618.4 4.0	4		gray tin	e Sano : wet				
					5—							
				0/5 0	6-							nated due to
				615.9_ 6.5	, –						of wa	ssive amount ater and aminants in Pit
İ				24.0	7-			-	& Free Product			
				61 <u>4.9</u> _	8-		BASE OF	FPIT			mate to Pit appro Jar o	vated rials returned t per EPA oval f solls and uct taken
					9-							
					10-							
					11-							
					12-							
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	į				14							

APPENDIX D

Geologic Cross Sections

SDMS US EPA Region V

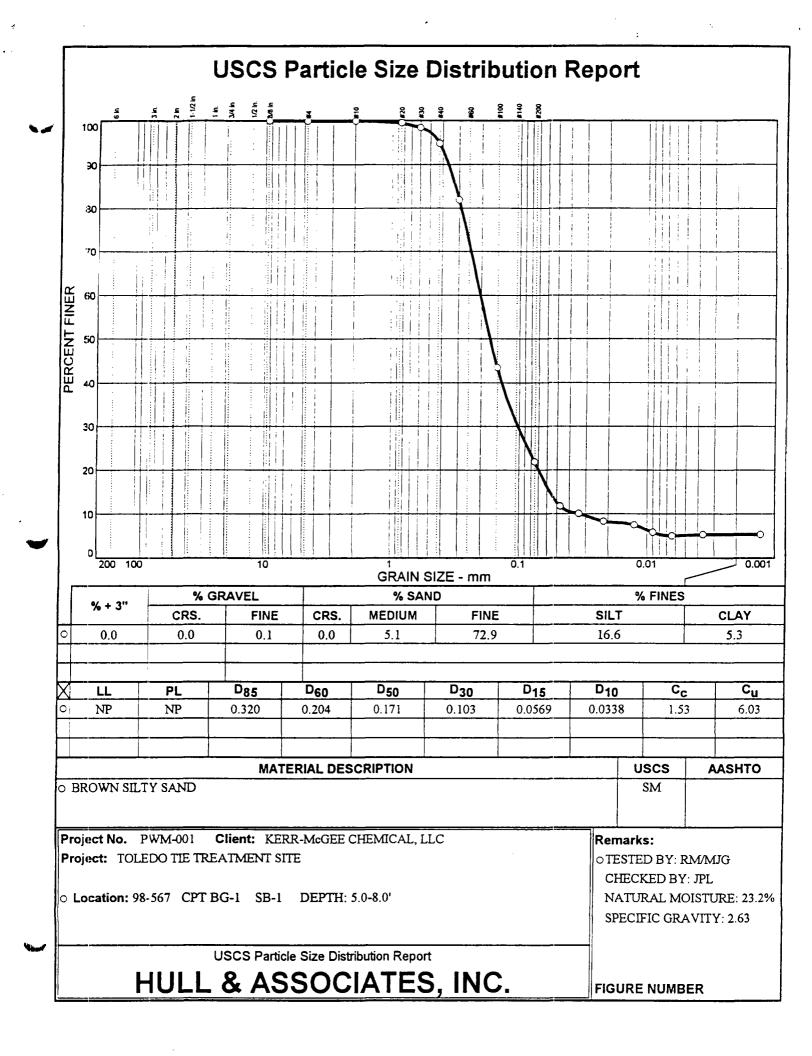
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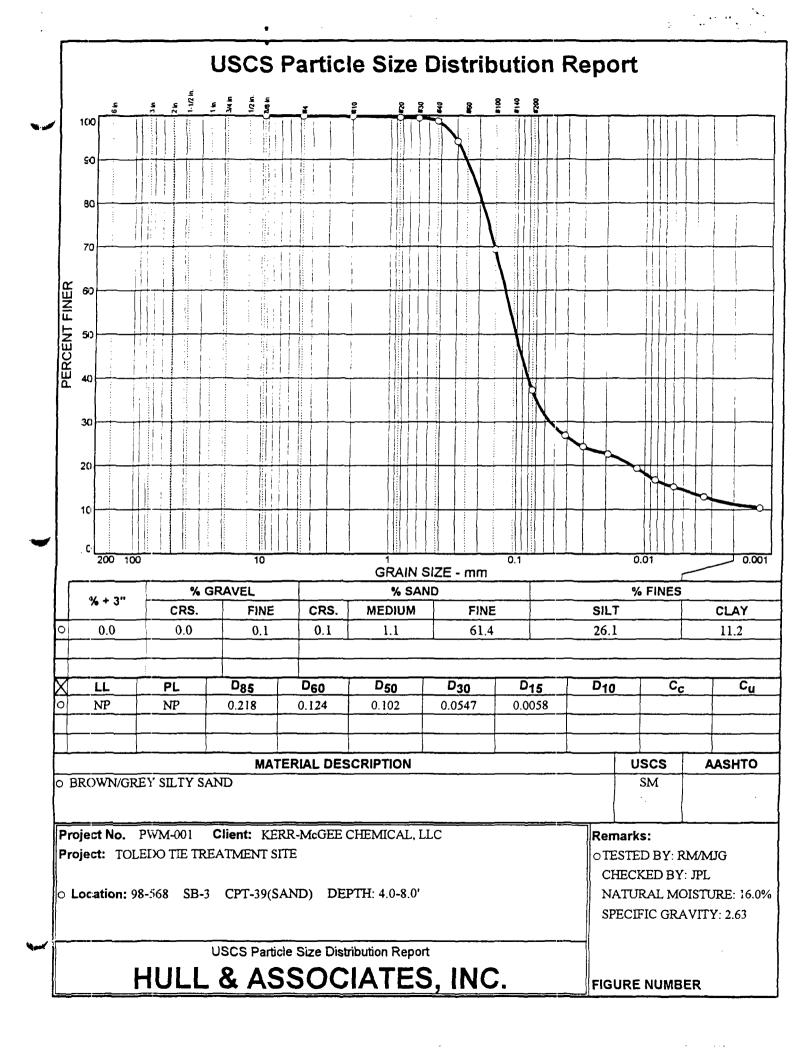
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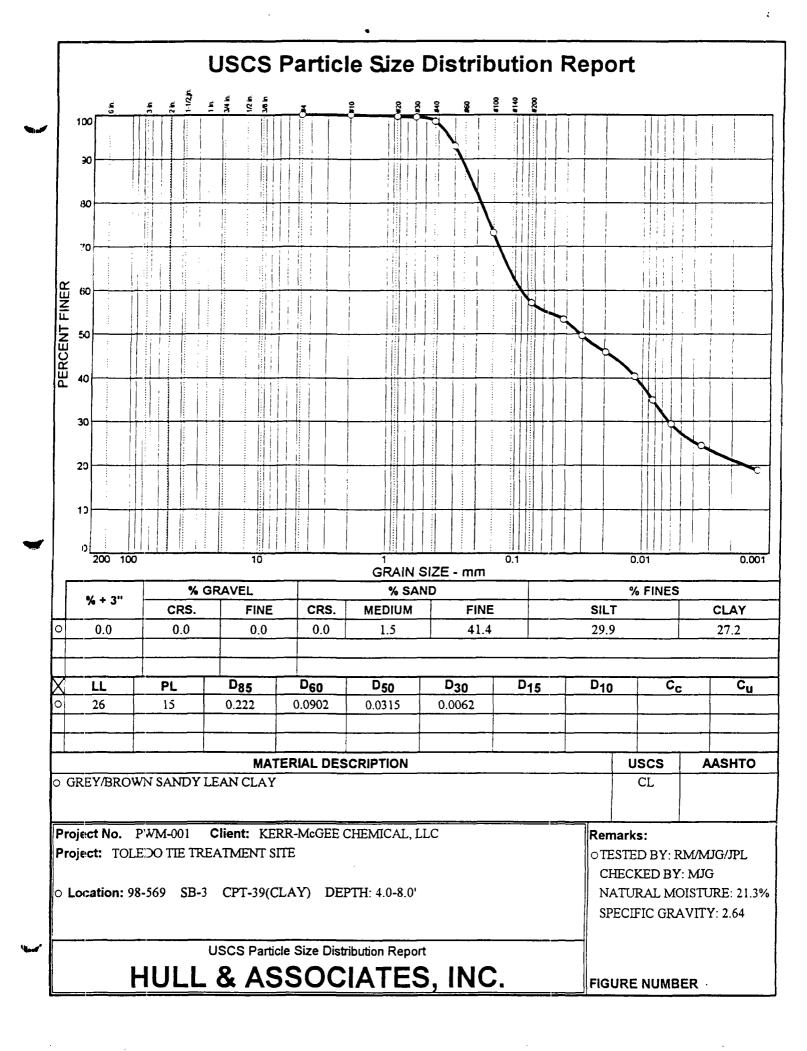
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х	Unscannable Material: Oversized X or Format. Due to certain scanning equipment capability limitations, the document page(s) is not available in SDMS. The original document is available for viewing at the Superfund Records center. Specify Type of Document(s) / Comment
	APPENDIX D – GEOLOGIC CROSS SECTIONS
	Other:
-	

APPENDIX E

Geotechnical Data







H.C. Nutting Company 4120 Airport Road Cincinnati, Ohio 45226

6/12/98smo

Huii & Associates Inc. Toledo Tie Treatment Site Proj. PWM-001 HCN W.O. # 12106.010

TABLE I

TABULATION OF CONSTANT HEAD-FIXED WALL PERMEABILITY TEST DATA

(Test performed per ASTM D-2434)

Lab No.	Boring No.	Sample No.	Depth (Ft.)	Dry Density (Lbs./Ft)	Total Head P.S.I.	Initial(I) Final(F) Natural W.C. %	(K) CM/Sec.	Material Description
4177	98-567	SB-1,BG-1	5-8	98.1	0.86	21.5(I) 21.5(F)	2.7x10-4	FINE SAND Remolded "Tight Condition"
4178	98-568	6B-3,CPT-39	4-8	106.0	5.87	16.3(I) 18.0(F)	2.4x10-6	SILTY SAND, TR ROOTS Remolded "Tight Condition"

prm6-12

H.C. NUTTING COMPANY

Robert L. House,

Vice President/Lab. Director

Hull & Associates, Inc. 3401 Glendale Avenue, Suite 300 Toledo, Ohio 43614 (419) 385-2018 (419) 385-5487 (fax)

LETTER OF TRANSMITTAL

DATE: 08/26/98	HAI Job No. PWM001
SUBJECT: Teceso -	TIE TREAMENT
Site -	

10:	MS. I	Deborah Orr					
	Unite	ed States Environmenta	l Protection Ag	gency			
	77 W	'. Jackson Boulevard (S	SE-4J)				
	Chica	ago, IL 60606					
		e sending you	Reports	_Work Order			
	_Invoi _Copy	of letter	Prints Plans	Change Order	 .		
	tem Date		Copies		Description		
	`	August 98	\	Replacement	page 27 of	29·	
				Time Cail	cal, Rancial	Plan-	
		-					
<u></u>		!	·				
	are trans signature	mitted as checked belov For review a		_For approval	_As requested	For your use	
REM.	ARKS: I	Deborah,					
Attacl	hed is a r	eplacement page for 27 o	f 29 in the repor	t for Toledo Tie we sent you	ı yesterday. Please call	if any	
questi	ons.						
					Sent	Q	
COPY	TO:		W/ENCL	OSURE			
Peter	Goetz, G	oetz Associates					
Ralph	Dollhopi	F, U. S. EPA					
					/		
					1		
				 SIGNED:	Hall?	Tax lait	
				J	Scott F./Loc	khart, P.E.	
		If e	enclosures are not as not	ed, kindly notify Hull & Associates, Inc	c. at once.		

TOLEDO TIE TREATMENT SITE TIME CRITICAL REMOVAL PLAN REVISION: 1

PAGE 27 OF 29

source or water draining from excavated soils or sediments. The City of Toledo WWTP is the

preferred receptor of potentially contaminated water from the site and negotiations are ongoing to

provide this capacity.

4.4.6 Contingency Plan

The site contingency plan will be amended as needed to address such things as on-site or off-site

spills of materials leaving the site, traffic emergencies, etc. The amended plan will be distributed to

the parties previously contacted and prior to initiating construction, reviewed with them.

4.4.7 Traffic Plan

ITC will be required to provide a traffic plan which identifies the proposed routing of trucks,

staging of equipment, materials, contaminated soils/sediments, etc. and establish a schedule of the

number and types of trucks, etc.

4.4.8 Project Schedule and Management Plan

ITC will be required to provide a project schedule which parallels to the degree practicable, the

preliminary one shown in Figure 8. Written documentation regarding cost control procedures,

project personnel, the chain of command with decision making authority defined, and regular

progress reports are to be supplied.

JULY (REVISED AUGUST)1998 PWM001,100.0063

Review of July 1988 Time Critical Work Plan

Proposed remedy:

- 1. Excavation of approximately 1250 feet of Williams Ditch sediments to a depth of two feet (up to 3.5 feet in some areas). Ditch will be rerouted during construction and the existing siphon dams will remain in place during the construction period.
- The lagoon area delineated by the investigation will be excavated to 8 feet. The existing infrasturcture (storm sewer) will be removed and replaced with a french drain. Potential migration pathways along the remaining utilities including a 4" gas line, electrical service, underground Ameritech lines, water mains and sanitary sewers, will be addressed by sealing around the pipes/trenches with geosynthetic material or bentonite seals.
- 3. Approximately 1410 feet of Frenchmens Road will be removed and replaced.
- 4. A subsurface barrier, a french drain (mentioned above), will be constructed to address residual contamination not removed. The collected storm water will be treated and released to sanitary sewer. Soil sediment will be dispose of off site or adsorption technology will be used.

Question/Comments

- It is not clear how the water collected from the french drain will be treated before discharging to the sanitary sewer.
- The basis for concluding an adequate correlation between the analytical data resulting from the borings and the geoprobe is not presented. An evaluation of the correlation between the analytical data and the CPT/LIF is not addressed at all.
- What are the action levels for the sediments in Williams Ditch and the soils in the lagoon area, they are alluded to in several places but are not listed?
- Soil boring 4 is missing from Plate 2.

Deborah Orr 20July1998

toledo/tcvkl.wpd

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MEMORANDUM

To:

Deborah Orr, Project Manager

United States Environmental Protection Agency

From: Larry Lueck, START Project Manager

Ecology & Environment, Inc.

Date: 24. July 1998

Re:

Comments on the "Time Critical Removal Plan (TCRP)

For the Toledo Tie Treatment Site Located at

ARCO Industrial Park, Toledo, Ohio," prepared by Hull & Associates, Inc. (HAI) for Kerr-McGee Chemical LLC, dated July 1998

TDD: S05-9806-012 PAN: 8N1201REXX

Ecology & Environment, Inc. (E & E) has completed review of the above referenced document. This memorandum sets forth our comments and suggestions for improvement of the TCRP.

General Comments:

- 1. The area immediately surrounding the Spartan warehouse building on the west, south, and southwest should be investigated with LIF and Geoprobe for the EE/CA; from Plate 2 of the TCRP, it appears that subsurface contamination may extend under the building and continue for an unknown distance in those directions.
- 2. Air monitoring stations and monitoring well locations are both prominently marked on Plates 1 and 2 of the TCRP but there is no discussion of either in the text.
- 3. It is perplexing that the lagoons are not distinguishable from adjacent soil on the basis of subsurface stratigraphy. Although lagoon limits are marked at the top of each cross section (Plates 3 through 5), stratigraphy is completely uninterrupted across these limits. How should that be interpreted?

Comments by sections and subsections:

page 2

1.2 Site Description

"... werehouse is currently situated over a portion of one of the suspected lagoons."

C: This could be a very important situation but it is not dealt with in the TCRP. Plate 2 shows 1-foot, 3-foot, 5-foot, and 7-foot contamination thickness contours stopping at the north side of this building, indicating that contamination must continue underneath. Pive-foot and 3-foot contamination thickness contours trend toward the building from the west but stop before reaching it. Soil sample SB-10, collected at location CPT-58 approximately 25 feet north of the building, and soil sample SB-7, collected at location CPT-56 approximately 50 feet west of the building, both show high contaminant concentrations (Table 4). The cross sections on Plates 4 and 5 also show significant contaminant signature thicknesses at these two locations, about 7 feet and 4 feet, respectively. Air photo evidence indicates that this building was constructed over one of the on-site filled lagoons known to be significant sources of subsurface contamination. This problem will have to be addressed in the EE/CA, if not in the time-critical removal.

page 4

"... municipal water supply system ..."

C: For the EE/CA, we will need to know where the municipal wells or surface water intakes are located relative to the site, and the size of drinking water population(s) they serve. It should also be verified that there is "no local use of groundwater for potable consumption."

1.3 Status of Site Removal Activities

page 5

"Field investigations to collect data on ... air at the site were conducted ..."

C: The TCRP should comment on the air monitoring methods that were used and their results, considering that other sample results are reported in detail, and should lay out specific plans for air sampling or monitoring during the time-critical removal.

2.2 Installation of CPT/LIF Borings

page 8 and section 2.2 in general

"Cross sections A-A', B-B', C-C', and D-D', which are shown on Plates 3, 4, and 5, provide an interpretation of shallow stratigraphic conditions encountered at the project area based on data obtained via installation of the CPT/LIF borings."

C: Only 10 of the CPT locations also have Geoprobe soil boring logs of the subsurface stratigraphy. This section should explain how the CPT/LIF by itself can distinguish the soil units used on Plates 3, 4, and 5, with some comment on how reliable this information is.

"..(as appropriate)..."

C: The intent of this parenthetical expression is unclear.

pages 8-9

- "... LIF signatures above background are mostly encountered in the upper sand/silt/clay deposits ..."
- C: This evaluation does not appear to be well supported by the cross sections. For example on Plate 3, cross section A-A': in CPT/LIF borings CPT-19, CPT 16 and CPT-11, contamination is shown to extend into the underlying SILT/CLAY unit for distances equivalent to half the total contamination thickness at each point. A similar situation occurs in other borings on this cross section and on cross-sections C-C' and D-D'. Six boring logs on cross section A-A', or 43%, show contamination in the lower SILT/CLAY; on cross sections C-C' and D-D', the corresponding numbers are 44% (four logs) and 17% (one log), respectively. This is important insofar as it might affect the excavation of contaminated materials.

page 10

2.3 Installation of Geoprobe Borings and Test Pits

- "...with each sample depth selected from the interval representing the LIF response above background ..."
- C: It would have been helpful to include a few analyses of samples collected from stratigraphic intervals immediately below the LIF non-detect level. We still do not know what LIF non-detect equates to in parts per million.

"In general ... was identified)."

C: This sentence is pretty unclear. Names of units like "SILT/CLAY" from the cross sections should be used to avoid confusion.

page 11

- "A review of data collected during the initial field investigation indicates that good correlation exists between the CPT/LIF borings, Geoprobe borings and test pits."
- C: This evaluation is an opinion and based on very little information. Subsurface stratigraphic detail is displayed on the cross sections of only four CPT locations for which there are also Geoprobe or test pit logs in Appendix C. Another interpretation of the comparison is that:
 - 1 the log of SB-9 is in poor agreement with the cross section of CPT-16 on Plate 3;
 - The log of SB-7 is in fair agreement with the cross section of CPT-56 on Plate 5, except for overall depth to the SILT/CLAY; the log of TP-6 is in better agreement with CPT-56;
 - 3 the log of TP-2 agrees with the cross section of CPT-38 on Plate 4; and
 - The log of SB-10 is in fair agreement with the cross section of CPT-58 on Plate 4, except for overall depth to SILT/CLAY.

page 12, first paragraph

3.0 RATIONALE FOR TECHNICAL APPROACH

- "... the proposed remedy ..."
- C: A brief up-front statement in this paragraph of what the proposed remedy is would be helpful.
- C: Somewhere between here and the end of the TCRP, there should be some ball-park estimates of cubic yardage and/or tonnage to be removed and treated or disposed of.

page 12, last sentence

- "... a direct migration pathway from these areas to the ditch was identified."
- C: There should be some discussion, probably in section 2.0, of what this pathway is. This sentence seems to be the first time it is mentioned in the TCRP.

page 14

4.1 Lagoon Excavation and Infrastructure Removal

- "... if transportation and disposal ... " "If thermal desorption ... " [underline added]
- C: It should be stated what this choice depends on and who will make the choice.

4.1.1 Excavation, Backfill, and Site Grading

- "... will be excavated to the subsurface lacustrine clay layer which is at a depth of approximately eight feet." and "... data show creosote ... rests upon a lower confining layer ..."
- C: See comment under pages 8-9, above, concerning contamination <u>in</u> this "lacustrine clay layer;" also see recommendation under page 10 that the cross section unit name "SILT/CLAY" should be used. Excavating only down to the SILT/CLAY could leave significant contamination in the ground.
- C: Sending confirmation samples to a laboratory for DNAPL analysis would seem to be essential but is not mentioned in the TCRP.

page 15

4.1.2 Utility Removal and Replacement

- '... service must be maintained to the ... warehouse ..."
- C Why? Is the building in use?

"Potential migration pathways ... seal across the utility trench."

C: Will this also be adequate for the EE/CA and the non-time-critical removal?

page 16

4 2.1 Sediment Excavation and Backfill

"... will be backfilled with either general soil fill or lined ... " [underline addec]

C: It should be stated what this choice depends on and who will make it.

C: Some discussion is needed of where the sediments will be dewatered and how.

4.2.2 Williams Ditch Rerouting

C: This section needs more explanation, with a figure that gives sufficient detail to show how this is supposed to work.

page 17

4.3.3 Operation

"... and water, once treated ..."

C: Explanation is needed of how, and where on site, contaminated water will be pretreated.

page 19

4.4.5 Dewatering/Stabilization Plan

"... the selected contractor ... "

C: There should be a brief discussion somewhere in the TCRP of what parts of the removal are to be subcontracted, how selection of subcontractor(s) will be done, and so on.

Summary of comments on the Toledo Tie Treatment Removal Action Plan

On July 15, 1998, OSC Ralph Dollhopf requested START review the Removal Action Plan submitted by the potentially responsible party, Kerr-McGee Chemical Corporation, for the Toledo Tie Treatment site. This memorandum summarizes START comments on the previously mentioned document.

Removal Action Plan

Page	Section	Comment
1	1.0	In the second paragraph, should the backup contractor be named? U.S. EPA may need to approve the backup contractor.
8	2.2	Shouldn't the last paragraph talk about maximum <u>depths</u> instead of "maximum <u>thickness</u> " of creosote signatures?
10	2.3	First paragraph, second sentence, should be reworded for clarity.
10	2.3	The first full paragraph discusses elevated parameter concentrations. SB-10 (CPT-58), located in the Spartan Chemical parking lot, exhibits the highest parameter concentrations. Looking at data from other CPT borings, it appears that the odd-shaped impoundment underneath Spartan Chemical and the impoundment underneath Frenchmens Road may be connected.
12	3.0	Bullet 2 at the bottom of the page states "The immediate sourceis identified as the two, westernmost lagoons." Proof that the impoundment located underneath the Spartan Chemical building and parking lot is not a source area needs to be provided.
14	4.1	When will a decision be made as far as off-site disposal or thermal treatment. These options should be evaluated.
14	4.1.1	Will excavation continue until the area reaches the visual extent of contamination or just to the proposed lines? Excavation of additional areas should be considered for the time-critical removal action. What will be the purpose of segregating soil? Is segregation of soil feasible, looking at how creosote has migrated to the surface in many areas of the site? Will the separate soil piles/segregation piles be sampled and sent at different levels of contamination?
15	4.1.1	Shouldn't clean backfill be used? Will a composite of proposed "native soils" be collected and analyzed to insure the soil is acceptable for backfill?
16	4.2.1	Is 2 feet deep enough for removal of upstream sediment? Are the 2 feet and 3.5 feet depths for sediment removal just guides? All sediment should be removed unless it is not contaminated. Two feet or 3.5 feet can be an estimate for disposal options/cost projections. The City of Toledo's Comprehensive Ditch Plan should be attached for review.
16	4.2.2	How will rerouting water in Williams Ditch be achieved? This should be stated in the plan for evaluation.

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<u>Page</u>	<u>Section</u>	Comment
17	4.3.3	What sampling or other information does the City of Toledo require for discharge?
19	4.4.4	Air monitoring plan action levels should be available for review before work begins on site.
Appen	dix C	
Geopro Test Pi	bbe and it Logs	PID/FID readings detected during Geoprobe soil borings and test pit excavating activities should have been indicated on the Geologic Drill Logs. TP-5 has a comment
Appen	dix E	There is no reference or discussion in the text concerning Appendix E and its relativity to the plan.
Plan S	et	Storm sewer numbers should be included on sheet 3 for the areas of the sewer to be removed.

Did you